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Australia



Copper, lead, zinc and nickel concentrates — Sampling

Part 1: Sampling procedures for determination of metal and moisture content



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- Australasian Institute of Mining and Metallurgy
- Australian X-ray Analytical Association
- CSIRO
- Engineers Australia
- International Copper Association Australia
- Minerals Council of Australia
- The Chamber of Minerals and Energy of Western Australia

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Copper, lead, zinc and nickel concentrates — Sampling

Part 1: Sampling procedures for determination of metal and moisture content

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Preface

This Standard was prepared by the Standards Australia Committee MN-005, Copper, Lead, Zinc and Nickel Ores and Concentrates, to supersede AS 2862.1—2008.

The objective of this document is to set out the basic methods for sampling copper, lead, zinc and nickel concentrates from moving streams and stationary lots, including stopped-belt sampling, to provide samples for chemical analysis, physical testing and determination of moisture content, in accordance with the relevant International Standards. Where the concentrates are susceptible to significant oxidation or decomposition, a common sample that is sufficiently representative, i.e. unbiased and sufficiently precise, is used for moisture determination and chemical analysis to eliminate bias (see AS 2863). Any large agglomerates (>10 mm) present in the primary sample are crushed prior to further sample processing. Sampling of concentrates in slurry form is specifically excluded from this document.

Stopped-belt sampling is the reference method for collecting concentrate samples against which mechanical and manual-sampling procedures can be compared. Sampling from moving streams is the preferred method. Both falling-stream and cross-belt samplers are described.

Sampling from stationary lots is used only where sampling from moving streams is not possible. The procedures described in this document for sampling from stationary lots only minimize some of the systematic sampling errors.

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The terms “normative” and “informative” are used in Standards to define the application of the appendices or annexes to which they apply. A “normative” appendix or annex is an integral part of a Standard, whereas an “informative” appendix or annex is only for information and guidance.

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 183, *Copper, lead, zinc and nickel ores and concentrates*.

This fourth edition cancels and replaces the third edition (ISO 12743:2018), which has been technically revised. The main changes to the previous edition are as follows:

- The minimum cutting aperture for cross-belt cutters in [8.3.2.3](#) i) has been reduced to 30 mm.
- A NOTE has been added to [15.4.10](#) indicating that ribbons with smaller dimensions can be formed depending on the mass of sample to be divided, and that the ribbon division method is particularly suitable for dividing chemical analysis samples.
- The requirements for preparation of chemical analysis samples in [16.2](#) have been expanded.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Australian Standard®

Copper, lead, zinc and nickel concentrates — Sampling

Part 1: Sampling procedures for determination of metal and moisture content

WARNING — This document can involve hazardous materials, operations and equipment. It is the responsibility of the user of this document to establish appropriate health and safety practices and to ensure compliance with any other restrictions.

1 Scope

This document sets out the basic methods for sampling copper, lead, zinc and nickel concentrates from moving streams and stationary lots, including stopped-belt sampling, to provide samples for chemical analysis, physical testing and determination of moisture content, in accordance with the relevant International Standards. Where the concentrates are susceptible to significant oxidation or decomposition, a common sample that is sufficiently representative, i.e. unbiased and sufficiently precise, is used for moisture determination and chemical analysis to eliminate bias (see ISO 10251). Any large agglomerates (>10 mm) present in the primary sample are crushed prior to further sample processing. Sampling of concentrates in slurry form is specifically excluded from this document.

Stopped-belt sampling is the reference method for collecting concentrate samples against which mechanical and manual-sampling procedures can be compared. Sampling from moving streams is the preferred method. Both falling-stream and cross-belt samplers are described.

Sampling from stationary lots is used only where sampling from moving streams is not possible. The procedures described in this document for sampling from stationary lots only minimize some of the systematic sampling errors.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 10251, *Copper, lead, zinc and nickel concentrates — Determination of mass loss of bulk material on drying*

ISO 12744, *Copper, lead, zinc and nickel concentrates — Experimental methods for checking the precision of sampling*

ISO 13292, *Copper, lead, zinc and nickel concentrates — Experimental methods for checking the bias of sampling*

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

3.1

representative sample

quantity of concentrate representing a larger mass of concentrate with both *precision* (3.29) and *bias* (3.28) within acceptable limits

3.2**lot**

quantity of concentrate to be sampled

3.3**lot sample**

quantity of concentrate representative of the *lot* ([3.2](#))

3.4**sub-lot**

subdivided parts of a *lot* ([3.2](#)) which are processed separately, each of them producing a *subsample* ([3.5](#)) which is analysed separately, for example for moisture determination

3.5**subsample**

quantity of concentrate representative of the *sub-lot* ([3.4](#))

3.6**sampling**

sequence of operations aimed at obtaining a sample representative of a *lot* ([3.2](#))

Note 1 to entry: It comprises a series of sampling stages, each stage usually comprising operations of selection and preparation.

3.7**selection**

operation by which a smaller quantity of concentrate is taken from a larger quantity of concentrate

3.8**increment**

quantity of concentrate selected by a sampling device in one operation

3.9**division**

operation of decreasing sample mass, without change of particle size, where a representative part of the sample is retained

3.10**constant-mass division**

method of *division* ([3.9](#)) in which the retained portions from individual *increments* ([3.8](#)) or *subsamples* ([3.5](#)) are of uniform mass

3.11**proportional division**

method of *division* ([3.9](#)) in which the retained portions from individual *increments* ([3.8](#)) or *subsamples* ([3.5](#)) are a constant proportion of their original mass

3.12**preparation**

nonselective operation without *division* ([3.9](#)) such as sample transfer, drying, comminution or homogenization

3.13**sample processing**

whole sequence of selection and preparation operations which transforms a *stage i sample* ([3.15](#)) into a *test sample* ([3.19](#))

3.14**comminution**

operation of reducing particle size by crushing, grinding or pulverisation

3.15**stage *i* sample**

sample obtained at the *i*th stage of the sampling scheme

3.16**moisture sample**

representative quantity of concentrate from which *test portions* (3.20) are taken for moisture determination

Note 1 to entry: Alternatively, the whole moisture sample may be dried to determine its moisture content.

3.17**laboratory sample**

sample that is processed so that it can be sent to the laboratory and used for further processing and selection of one or more *test samples* (3.19) for analysis

3.18**common sample**

representative quantity of concentrate which is dried to determine its mass loss and subsequently used for further processing and selection of one or more *test samples* (3.19) for chemical analysis

3.19**test sample**

representative quantity of concentrate obtained from a *laboratory sample* (3.17) when additional preparation, such as drying or hygroscopic moisture determination, is needed prior to the selection of one or more *test portions* (3.20)

3.20**test portion**

representative quantity of concentrate taken from a *moisture sample* (3.16), a *laboratory sample* (3.17) or a *test sample* (3.19) which is submitted to moisture determination or analysis in its entirety

3.21**systematic sampling**

selection of *increments* (3.8) in which the concentrate being sampled is divided into equal strata and the first *increment* (3.8) is taken at random within the first stratum, the interval between subsequent *increments* (3.8) being equal to the stratum size

3.22**stratified random sampling**

selection of *increments* (3.8) in which the concentrate being sampled is divided into equal strata, each *increment* (3.8) being taken at random within each stratum

3.23**agglomerate**

cluster of particles that are held together by chemical or physical phenomena

3.24**nominal top size**

aperture size of a test sieve that retains 5 % of the mass of concentrate

3.25**moisture determination**

quantitative measurement of the mass loss of the moisture *test portion* (3.20) under the conditions of drying specified in ISO 10251

3.26**chemical analysis**

quantitative determination of the required chemical constituents of the analysis *test portion* (3.20)

3.27**error**

difference between the true value and the value obtained for an individual measurement in any quantitative measurement

3.28**bias**

statistically significant difference between the mean of the test results and an accepted reference value

Note 1 to entry: See also ISO 13292.

3.29**precision**

closeness of agreement between independent test results obtained under stipulated conditions

Note 1 to entry: See also ISO 12744.

3.30**interleaved samples**

samples constituted by placing consecutive primary *increments* (3.8) alternately into two separate sample containers

4 Sampling theory

4.1 General

The basic rule for a correct sampling method is that all possible increments from the concentrate stream or stratum shall have the same probability of being selected and appearing in the sample. Any deviation from this basic requirement can result in a bias. An incorrect sampling scheme cannot be relied on to provide representative samples.

Sampling should preferably be carried out on a systematic basis, either on a mass basis (see 7.2) or on a time basis (see 7.3), but only where it can be shown that no systematic error (or bias) could be introduced due to any periodic variation in quality or quantity that may coincide with, or approximate to, any multiples of the proposed sampling interval. In such cases, it is recommended that stratified random sampling within fixed time or mass intervals be carried out (see 7.4).

The methods for sampling, including sample processing, depend on the final choice of the sampling scheme and on the steps necessary to minimize possible systematic errors. The aim is always to reduce the total variance to an acceptable level, while at the same time eliminating any significant biases, for example minimizing degradation of samples used for determination of size distribution.

Moisture samples shall be processed as soon as possible and test portions shall be weighed immediately. If this is not possible, samples shall be stored in impervious airtight containers with a minimum of free air space to minimize any change in moisture content but should be prepared without delay.

4.2 Total variance

The general aim of a sampling scheme is to provide one or several test portions, sufficiently representative of a lot, for determination of the quality characteristics of the lot. The total variance of the final result, denoted by s_T^2 , consists of the variance of sampling (including sample processing) plus the variance of analysis (e.g. chemical analysis, moisture determination, determination of particle size distribution) and is given by [Formula \(1\)](#):

$$s_T^2 = s_S^2 + s_A^2 \quad (1)$$

where

s_S^2 is the sampling variance (including sample processing);

s_A^2 is the analytical variance.

In [Formula \(1\)](#), the sampling variance includes the variances due to all sampling (and sample processing) steps, except selection of the test portion. The variance due to selection of the test portion is included in the analytical variance, s_A^2 , which shall be determined in accordance with ISO 12744, because it is difficult to determine separately the “true” analytical variance.

Often replicate analyses of quality characteristics are carried out, which reduces the total variance. In this case, if r replicate analyses are made, the total variance is given by [Formula \(2\)](#):

$$s_T^2 = s_S^2 + \frac{s_A^2}{r} \quad (2)$$

The estimation or measurement of the total variance can be carried out in several ways, depending on the purpose of the exercise. In many respects, the different approaches are complementary.

The first method, which was developed by Gy,^[3,4] is to break up the sampling variance into its components for each sampling stage, and shall be carried out as specified in [Annex A](#). The total variance is then given by [Formula \(3\)](#):

$$s_T^2 = s_{S_1}^2 + \dots + s_{S_i}^2 + \dots + s_{S_{u-1}}^2 + \frac{s_A^2}{r} \quad (3)$$

where

$s_{S_1}^2$ is the sampling variance for stage 1, i.e. the primary sampling variance;

$s_{S_i}^2$ is the sampling variance for stage i ;

$s_{S_{u-1}}^2$ is the sampling variance for stage $u - 1$, the second last stage;

u is the number of sampling stages, stage u corresponding to selection of the test portion.

This is referred to as the “sampling stage” method (see [4.3](#)) and provides very detailed information on the variance components, which is particularly useful for designing and assessing sampling schemes. However, to obtain maximum benefit it is necessary to collect data at each sampling stage.

The second method, called the “simplified” method (see [4.4](#)), is to break up the total variance into primary sampling, sample processing and analytical variances only. In this case, the total variance is given by [Formula \(4\)](#):

$$s_T^2 = s_{S_1}^2 + s_P^2 + \frac{s_A^2}{r} \quad (4)$$

where

$s_{S_1}^2$ is the primary sampling variance;

s_P^2 is the variance due to all subsequent sampling steps, i.e. sample processing, except selection of the test portion;

s_A^2 is the analytical variance, including selection of the test portion [at stage u in [Formula \(3\)](#)].

The primary sampling variance is identical to the sampling variance for stage 1 in [Formula \(3\)](#), while s_P^2 is equal to the total sampling variance for the remaining sampling stages, except for selection of the

test portion which is included in the analytical variance. The relative magnitudes of the variance components in [Formula \(4\)](#) indicate where additional effort is required to reduce the total variance. However, it is not possible to separate the variances of the separate sample-processing stages. This method is suitable for estimating the total variance for new sampling schemes based on the same sample-processing procedures, where the numbers of primary increments, sample processings and analyses are varied.

Finally, the total variance s_T^2 can be estimated experimentally by collecting interpenetrating duplicate samples (see [4.5](#)). This is called the “interleaved sample” method and gives valuable information on the total variance actually achieved for a given sampling scheme with no extra effort, provided facilities are available for collecting duplicate samples (Merks[5]). It gives no information on variance components, but the total variance can be compared with the analytical variance to ascertain whether the sampling scheme used was optimized or not. It is therefore of limited use for designing sampling schemes, but it can be used to monitor whether a sampling scheme is in control.

4.3 Sampling-stage method of estimating sampling and total variance

The sampling variance for stage i is given by [Formula \(5\)](#) (see [Annex A](#)):

$$s_{S_i}^2 = \frac{s_{b_i}^2}{n_i} \quad (5)$$

where

$s_{b_i}^2$ is the variance between increments for stage i ;

n_i is the number of increments for stage i .

The variance between increments for stage i , $s_{b_i}^2$, can be estimated using [Formula \(6\)](#):

$$s_{b_i}^2 = \frac{\sum_{j=1}^n (x_j - \bar{x})^2}{n_i - 1} - s_{PA}^2 \quad (6)$$

where

x_j is the test result for increment j ;

$\bar{x}$ is the mean test result for all increments;

s_{PA}^2 is the variance of subsequent sample processing and analysis.

The variance of subsequent sample processing and analysis of each increment, s_{PA}^2 , has been taken into account in [Formula \(6\)](#) to obtain an unbiased estimate of $s_{b_i}^2$.

NOTE Care is needed in subtracting variances. The difference is significant only when the F ratio of the variances being subtracted is statistically significant.

Remembering that the variance due to selection of the test portion is included in the analytical variance s_A^2 , the total sampling variance is given by [Formula \(7\)](#):

$$s_S^2 = \sum_{i=1}^{u-1} \frac{s_{b_i}^2}{n_i} \quad (7)$$

Combining [Formulae \(2\)](#) and [\(7\)](#) provides the total variance s_T^2 , which is given by [Formula \(8\)](#):

$$s_T^2 = \sum_{i=1}^{u-1} \frac{s_{b_i}^2}{n_i} + \frac{s_A^2}{r} \quad (8)$$

For a three-stage sampling scheme (including selection of the test portion), [Formula \(8\)](#) reduces to [Formula \(9\)](#):

$$s_T^2 = \frac{s_{b_1}^2}{n_1} + \frac{s_{b_2}^2}{n_2} + \frac{s_A^2}{r} \quad (9)$$

The best way of reducing the value of s_T^2 to an acceptable level is to reduce the largest terms in [Formula \(8\)](#) first. Clearly $s_{b_i}^2 / n_i$ for a given sampling stage can be reduced by increasing the number of increments n_i or reducing $s_{b_i}^2$ by homogenizing the concentrate prior to sampling. The last term can be reduced by reducing the particle size prior to selection of the test portion or performing replicate analyses. Selecting the optimum number of increments n_i for each sampling stage may require several iterations to obtain the required total variance s_T^2 .

EXAMPLE Consider a four-stage sampling scheme for determining the metal content of a copper concentrate containing 31,2 % Cu. Assume that the concentrate is being conveyed at 500 t/h on a conveyor belt, that the lot size is 500 t, and that the following parameters have been determined using [Formula \(6\)](#) where appropriate:

$$s_{b_1} = 0,3 \% \text{ Cu}$$

$$s_{b_2} = 0,2 \% \text{ Cu}$$

$$s_{b_3} = 0,1 \% \text{ Cu}$$

$$s_A = 0,05 \% \text{ Cu}$$

NOTE Many measurements might be required to obtain good estimates of s_{b_1} , s_{b_2} , s_{b_3} and s_A .

Stage 1

Assume that the primary cutter takes increments of 12 kg mass at 2 min intervals. Thus:

$$n_1 = 30$$

Primary sample mass = 360 kg

[Formula \(5\)](#) gives:

$$s_{S_1}^2 = (0,3)^2 / 30 = 0,003$$

Stage 2

The primary increments are collected in a hopper and then fed to the secondary cutter at a rate of 360 kg/h. Secondary increments of 0,01 kg are taken at 30 s intervals. Thus:

$$n_2 = 120$$

Divided sample mass = 1,2 kg

$$s_{S_2}^2 = (0,2)^2/120 = 0,000\ 333$$

Stage 3

The 1,2 kg sample is transported to the sample-processing laboratory and fed through a rotary sample divider with a sample-collection canister divided into eight equal sectors rotating at 30 rev/min (0,5 s⁻¹). Sample division takes 2 min. Thus:

$$n_3 = 60$$

Divided sample mass = 150 g

$$s_{S_3}^2 = (0,1)^2/60 = 0,000\ 167$$

Stage 4

Dry the sample and then pulverize it to 150 µm. Select a 1 g test portion by taking 10 increments of 0,1 g with a spatula and conduct a single analysis. Thus:

$$s_A = 0,05\ \% \text{ Cu}$$

The total variance is given by:

$$\begin{aligned} s_T^2 &= s_{S_1}^2 + s_{S_2}^2 + s_{S_3}^2 + s_A^2 \\ &= 0,003\ 0 + 0,000\ 333 + 0,000\ 167 + 0,002\ 5 \\ &= 0,006 \end{aligned}$$

Hence:

$$s_T = 0,077\ \% \text{ Cu}$$

In this example, the largest components of variance are due to primary sampling and analysis. Consequently, the total variance can be reduced by increasing the number of primary increments and conducting replicate analyses.

An example of the application of the sampling-stage method of estimating total variance to sampling from grabs is given in [Annex B](#).

4.4 Simplified method of estimating sampling and total variance

While it is not possible to partition, i.e. separate, the variances of the individual sample-processing stages, the simplified method is suitable for estimating the total variance for new sampling schemes based on the same sample-processing procedures, where the numbers of primary increments, sample processings and analyses are varied.

Using [Formula \(5\)](#), the primary sampling variance $s_{S_1}^2$ is given by [Formula \(10\)](#):

$$s_{S_1}^2 = \frac{s_{b_1}^2}{n_1} \quad (10)$$

where

n_1 is the number of primary increments;

$s_{b_1}^2$ is the variance between primary increments determined using [Formula \(6\)](#).

The primary sampling variance can be reduced by increasing the number of primary increments n_1 .

The sample-processing variance s_p^2 and analytical variance s_A^2 shall be determined experimentally by duplicate sample processing and determination of quality characteristics in accordance with ISO 12744. The analytical variance s_A^2 can also be obtained by carrying out duplicate analyses on test samples.

Multiple sample processings and analyses are often carried out to reduce the total variance. In this case, combining [Formulae \(4\)](#) and [\(10\)](#) gives [Formulae \(11\)](#), [\(12\)](#) and [\(13\)](#).

- a) Where a single sample is constituted for the lot and r replicate analyses are carried out on the test sample:

$$s_T^2 = \frac{s_{b_1}^2}{n_1} + s_p^2 + \frac{s_A^2}{r} \quad (11)$$

- b) Where the lot is divided into k sub-lots, a subsample is constituted for each sub-lot, and r replicate analyses are carried out on each resultant test sample:

$$s_T^2 = \frac{s_{b_1}^2}{n_1} + \frac{s_p^2}{k} + \frac{s_A^2}{rk} \quad (12)$$

- c) Where sample processing and analysis is carried out on each increment taken from the lot and r replicate analyses are carried out:

$$s_T^2 = \frac{s_{b_1}^2 + s_p^2 + \frac{s_A^2}{r}}{n_1} \quad (13)$$

EXAMPLE Assume that 50 primary increments are taken from a zinc concentrate lot that has been divided into two sub-lots. The resultant two subsamples are processed separately and analysed in duplicate. Assume that the primary increment, sample processing and analytical standard deviations have been determined experimentally as follows:

$$s_{b_1} = 0,3 \% \text{ Zn}$$

$$s_p = 0,1 \% \text{ Zn}$$

$$s_A = 0,05 \% \text{ Zn}$$

Using [Formula \(12\)](#), the total variance is given by:

$$\begin{aligned} s_T^2 &= (0,3)^2/50 + (0,1)^2/2 + (0,05)^2/(2 \times 2) \\ &= 0,001\ 8 + 0,005\ 0 + 0,000\ 625 \\ &= 0,007\ 43 \end{aligned}$$

Hence:

$$s_T = 0,086 \% \text{ Zn}$$

In this example, the major component of variance is sample processing. This component can be reduced by dividing the lot into a larger number of sub-lots and constituting a subsample for each sub-lot.

4.5 Interleaved sample method of measuring total variance

The total variance s_T^2 achieved for a given sampling operation can be estimated experimentally by collecting interleaved duplicate samples as shown in [Figure 1](#). If the number of primary increments for routine sampling is n_1 , then $2n_1$ primary increments are taken from each lot and the odd- and even-numbered increments are separately combined to give samples A and B for the lot. Samples A and B are then separately submitted to sample processing and analysis. This procedure is repeated until sampling has been completed. The total variance for a single lot is then given by [Formula \(14\)](#):

$$s_T^2 = \frac{\pi}{4} \left[\frac{\sum_{i=1}^N |x_{A_i} - x_{B_i}|}{N} \right]^2 \quad (14)$$

where

x_{A_i} and x_{B_i} are the analyses for each pair of samples A_i and B_i ;

N is the number of lots (in the range 10 to 20);

$\frac{\pi}{4}$ is a statistical factor relating range to variance for a pair of measurements.

Alternatively, if the precision is being checked as part of routine sampling, n primary increments may be taken from each lot and two interleaved samples constituted, each comprising $n/2$ primary increments. However, the overall variance thus obtained is overestimated and the sampling variance component has to be divided by two to obtain the overall variance for lot samples comprising n primary increments (see ISO 12744).

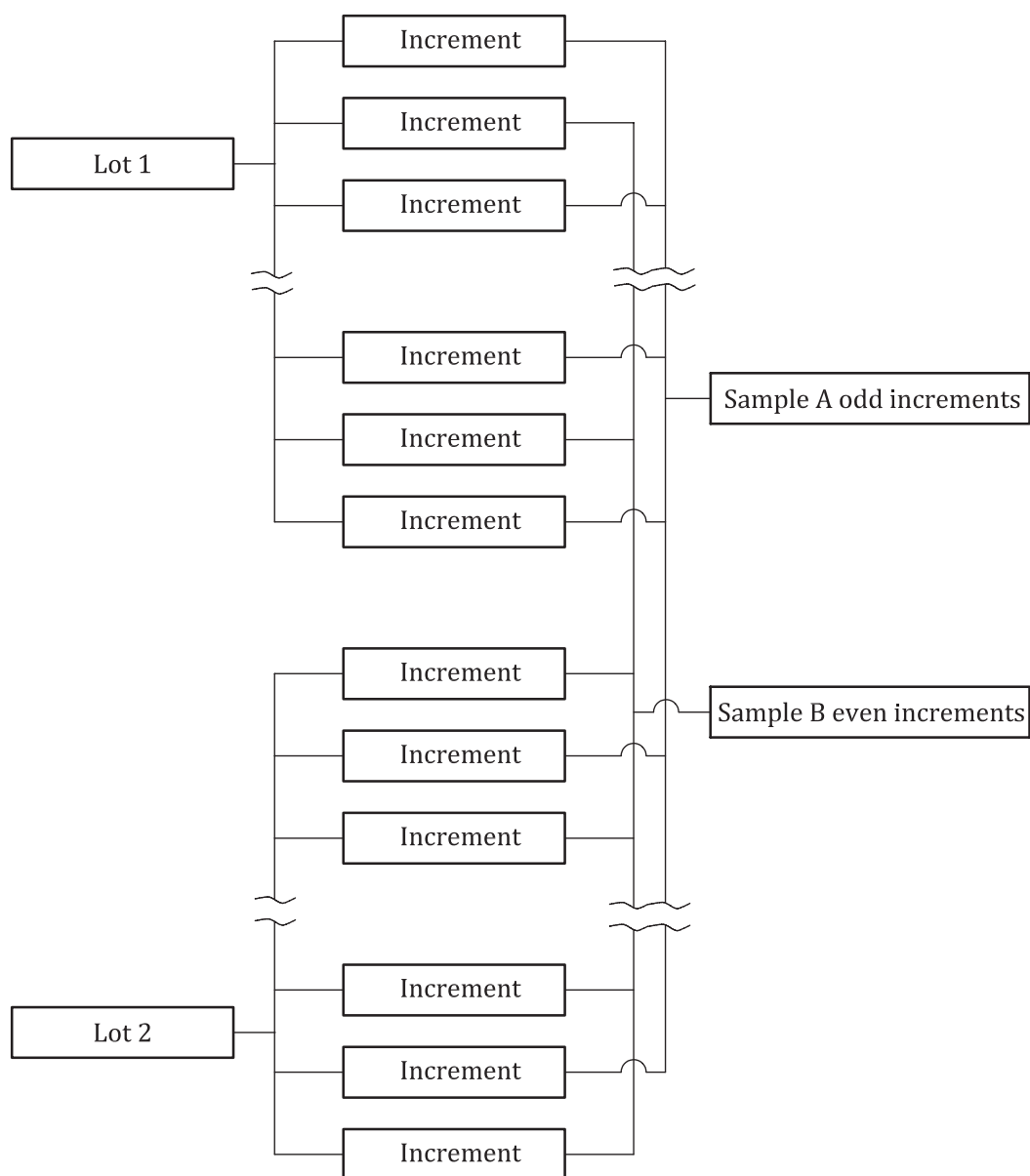


Figure 1 — Example of a plan for interleaved duplicate sampling

EXAMPLE The analyses of interleaved samples taken from 10 lots of copper concentrate are given in [Table 1](#).

Table 1 — Analyses of interleaved samples taken from copper concentrate

Lot	Odd samples (A) Cu %	Even samples (B) Cu %	Absolute difference Cu %
1	30,37	30,34	0,03
2	30,47	30,46	0,01
3	29,99	30,01	0,02
4	29,97	29,98	0,01
5	30,12	30,18	0,06
6	30,02	30,05	0,03
7	30,32	30,35	0,03
8	30,18	30,17	0,01
9	30,31	30,27	0,04
10	30,28	30,25	0,03
Sum of absolute differences			0,27

[Formula \(14\)](#) gives:

$$s_T^2 = \left(\frac{\pi}{4}\right) (0,27/10)^2$$

$$= 0,000\ 573$$

Hence:

$$s_T = 0,024\ \% \text{ Cu}$$

5 Establishing a sampling scheme

The procedure for establishing a sampling scheme is as follows.

- Identify the quality characteristics to be measured and specify the mass of the lot or sub-lot and the desired total variance s_T^2 . Typical values of s_T are given in [Table 2](#).
- Ascertain the nominal top size of the concentrate.
- Specify the cutter aperture, or the dimensions of the manual-sampling implement, according to the nominal top size of the concentrate.
- Ascertain the analytical variance s_A^2 . Typical values of s_A are given in [Table 2](#).
- Determine the variance between primary increments $s_{b_1}^2$ and the sample-processing variance s_p^2 if the simplified method is used (see [4.4](#)), or the variance between increments $s_{b_1}^2$ for each proposed stage if the sampling-stage method is used (see [4.3](#)). [Table 3](#) gives typical values of s_{b_1} for the first sampling stage.
- If the simplified method is used, use [Formula \(11\)](#), [\(12\)](#) or [\(13\)](#) to select the number of primary increments, sample processings and replicate analyses, so that the total variance s_T^2 does not exceed the desired value specified in step a).

Alternatively, if the sampling-stage method is used, use [Formula \(8\)](#) to select the number of increments n_i required at each sampling stage and the number of replicate analyses so that the total variance s_T^2 does not exceed the value selected in step a).

- g) Determine the sampling intervals at each stage, in tonnes for mass-basis systematic sampling (see 7.2) and stratified random sampling within fixed mass intervals (see 7.4), or in minutes for time-basis systematic sampling (see 7.3) and stratified random sampling within fixed time intervals (see 7.4).
- h) Take increments at the intervals determined in step g) for each stage during the whole period of handling the lot.
- i) Either combine the primary increments into lot samples or subsamples for analysis or analyse each primary increment separately. Examples of suitable sampling schemes are given in Figures 2 to 4, but the scheme shown in Figure 2 and Figure 4 is not suitable for preparing chemical analysis samples used to analyse for volatile elements, such as mercury.

The lot is often divided into sub-lots from which subsamples are prepared and analysed separately to reduce the total variance, as outlined in 4.4. Subsamples may also be prepared to provide progressive information on the quality of the lot, or to reduce possible changes in the moisture content of samples.

Table 2 — Typical target values of the required total and analytical standard deviations for determination of metal and moisture content

Characteristic	Parameter	Content range/standard deviation		
Cu	Range	< 30 %	30 % to 50 %	
	s_T	0,05 %	0,1 %	
	s_A	0,03 %	0,03 %	
Pb, Zn	Range	< 30 %	30 % to 50 %	> 50 %
	s_T	0,1 %	0,2 %	0,3 %
	s_A	0,07 %	0,07 %	0,15 %
Ni	Range	< 10 %	10 % to 30 %	
	s_T	0,1 %	0,2 %	
	s_A	0,05 %	0,1 %	
Ag	Range	< 500 g/t	500 g/t to 1 000 g/t	> 1 000 g/t
	s_T	10 g/t	2 % of concentrate	2 % of concentrate
	s_A	7 g/t	15 g/t	20 g/t
Au	Range	< 5 g/t	5 g/t to 15 g/t	> 15 g/t
	s_T	0,5 g/t	0,5 g/t	2 % of concentrate
	s_A	0,15 g/t	0,2 g/t	0,4 g/t
Moisture	Range	< 20 %		
	s_T	0,3 %		
	s_A	0,07 %		

NOTE s_T can be reduced if required by performing replicate analyses.

Table 3 — Examples of standard deviations between primary increments

Constituent	Standard deviation between primary increments (s_{bi})
Cu in copper concentrate	0,1 % to 0,5 % Cu
Pb and Zn in lead and zinc concentrates	0,1 % to 2,0 % Pb/Zn
Ni in nickel concentrates	0,1 % to 0,5 % Ni
Ag in copper, lead and zinc concentrates	1 g/t to 5 g/t Ag

Table 3 (continued)

Constituent	Standard deviation between primary increments (s_{bi})
Au in copper, lead and zinc concentrates	0,5 g/t to 2,0 g/t Au
Moisture in copper, lead and zinc concentrates	0,2 % to 0,7 %
NOTE The standard deviation between primary increments for mass fraction of silver is applicable to Ag < 500 g/t only.	

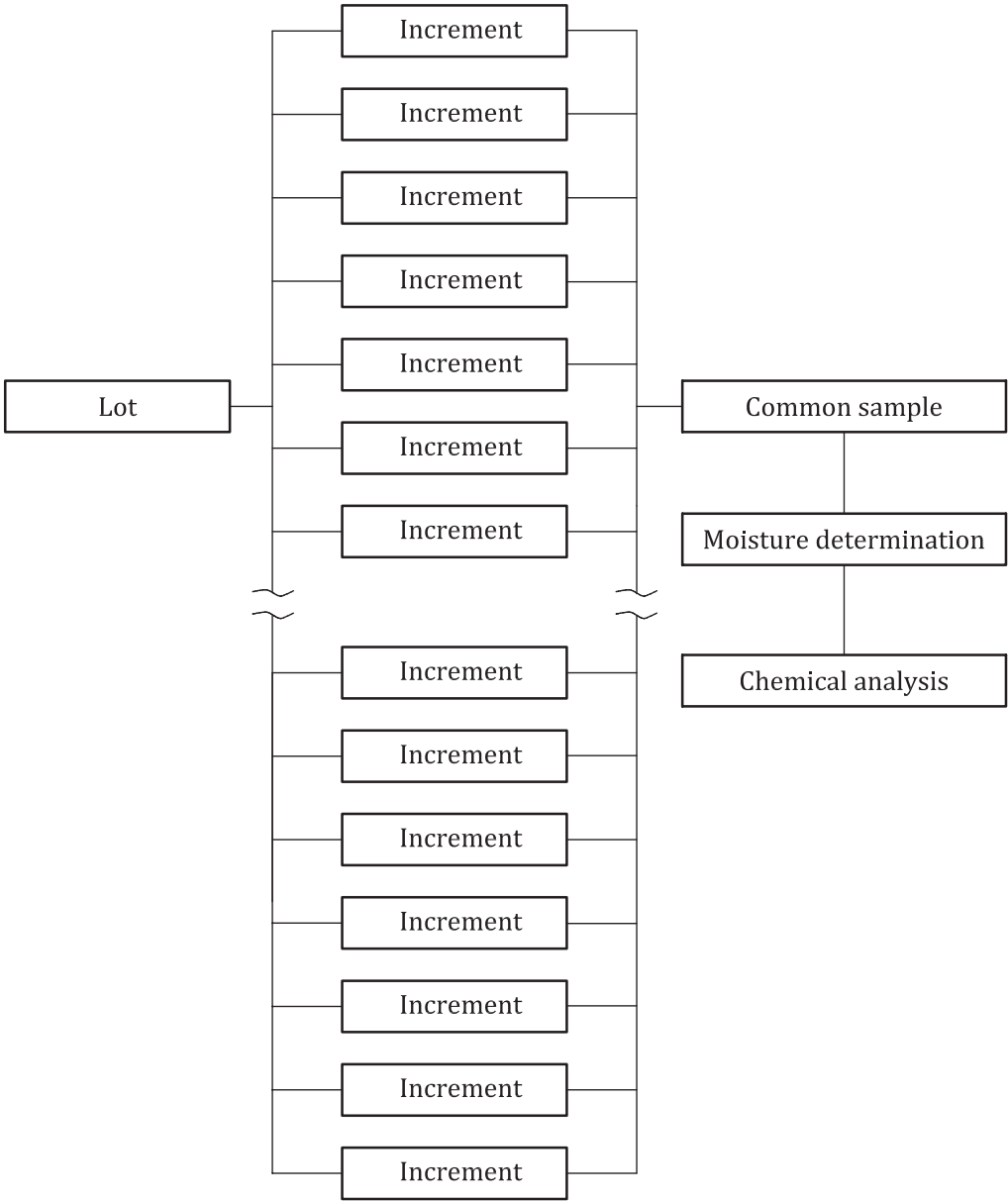
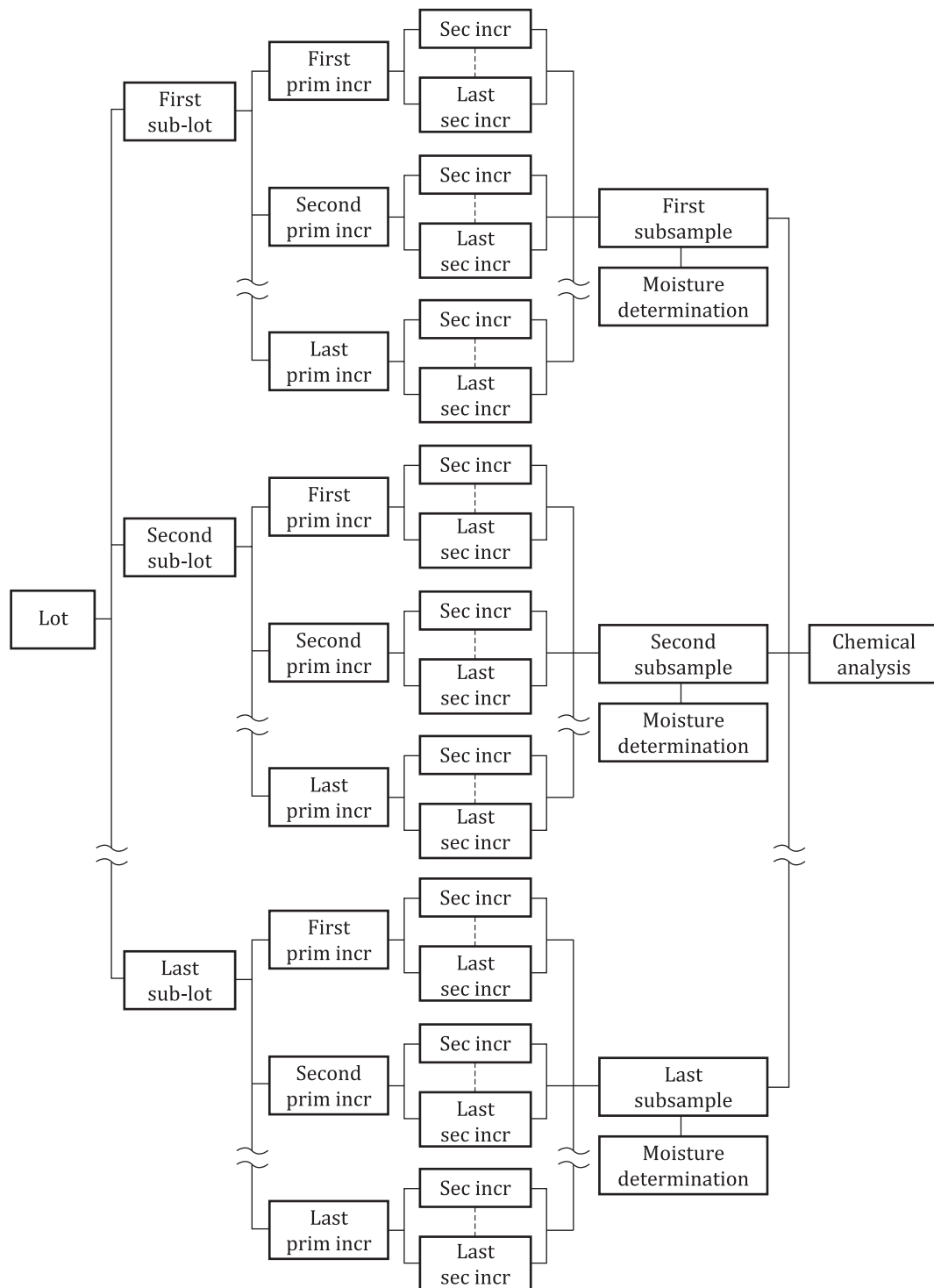


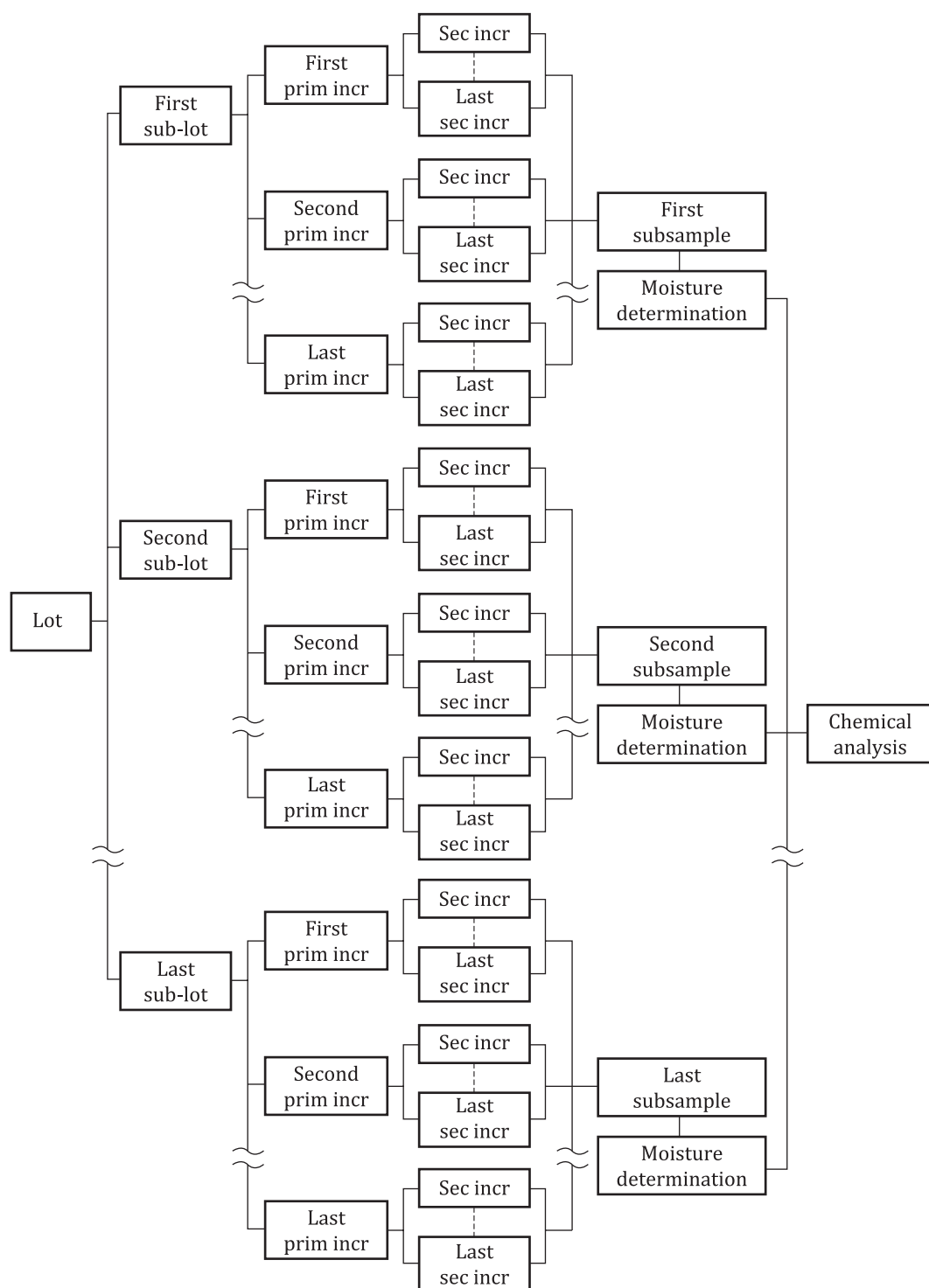
Figure 2 — Example of a sampling scheme in which a common sample is constituted for the lot for moisture determination and subsequent chemical analysis

**Key**

prim incr primary increment
 sec incr secondary increment

NOTE Mixing, comminution and division steps have been omitted for simplicity. This scheme is suitable for concentrates that are susceptible to oxidation or decomposition.

Figure 3 — Example of a sampling scheme in which the lot is divided into sub-lots for moisture determination and a separate lot sample is constituted for chemical analysis

**Key**

prim incr primary increment
 sec incr secondary increment

NOTE Mixing, comminution and division steps have been omitted for simplicity. This scheme is suitable for concentrates that are susceptible to oxidation or decomposition.

Figure 4 — Example of a sampling scheme in which the lot is divided into sub-lots for moisture determination, and the dried moisture subsamples are subsequently combined into a single lot sample for chemical analysis

6 Mass of increment

6.1 General

To avoid bias, it is essential that increments are extracted in such a manner that all possible increments from the concentrate stream have the same probability of being selected and becoming part of the final sample for analysis, irrespective of the size, mass or density of individual particles in the stream. This determines the increment mass required to obtain an unbiased sample.

However, there is also a practical minimum increment mass that should always be exceeded to minimize the effect of handling on the characteristics of the increment as it passes through the sampling system. This is particularly important for moisture content, where moisture loss (or gain) has to be minimized. The minimum mass needs to be specified for each concentrate type and each sampling device.

6.2 Mass of increment for falling-stream samplers

To avoid bias, the mass of increment at any sampling stage taken by a mechanical or manual cutter type sampler from the concentrate stream at the discharge end of a moving conveyor is determined by the minimum cutter aperture as specified in [8.3.2.2](#), the maximum cutter speed, as specified in [8.3.3.2](#), and the flow rate of the concentrate stream, and therefore is given by [Formula \(15\)](#):

$$m_I = \frac{GA}{3,6 v_c} \quad (15)$$

where

m_I is the mass of increment, in kilograms;

G is the flow rate of the concentrate stream, in tonnes per hour;

A is the cutter aperture, in metres (see [8.3.2.2](#));

v_c is the cutter speed, in metres per second (see [8.3.3.2](#)).

6.3 Mass of increment for cross-belt samplers

The mass of increment taken by a cross-belt cutter from a moving stream to avoid bias is determined by the minimum cutter aperture as specified in [8.3.2.3](#), the speed of the concentrate stream (i.e. the belt speed) and the flow rate of the concentrate stream, and therefore is given by [Formula \(16\)](#):

$$m_I = \frac{GA}{3,6 v_B} \quad (16)$$

where

A is the cutter aperture, in metres (see [8.3.2.3](#));

v_B is the speed of the concentrate stream, in metres per second.

6.4 Mass of increment for manual sampling from stationary lots

6.4.1 Primary increments

The minimum mass of primary increment taken by a manual-sampling implement from a stationary lot shall be 0,25 kg. However, if the nominal top size exceeds 16 mm due to the presence of agglomerates,

the mass shall be increased in accordance with [Formula \(17\)](#) based on a sampling implement of minimum dimensions $3d \times 3d \times 3d$:

$$m_{\text{Imin}} = 27 \rho d^3 \times 10^{-6} \quad (17)$$

where

m_{Imin} is the minimum mass of increment, in kilograms;

ρ is the bulk density of the concentrate, in tonnes per cubic metre;

d is the nominal top size of the agglomerates, in millimetres.

6.4.2 Mass of secondary and subsequent increments

The minimum mass of secondary and subsequent increments taken by a manual-sampling implement shall be 10 g. However, if the nominal top size is 5 mm or greater due to the presence of agglomerates, the mass shall be increased in accordance with [Formula \(17\)](#).

6.5 Mass of increment for stopped-belt reference sampling

The mass of increment taken from a stopped belt for reference sampling is determined by the minimum length of the sampling frame as specified in [Clause 10](#), the speed of the concentrate stream (i.e. the belt speed) and the flow rate of the concentrate stream, and therefore is given by [Formula \(18\)](#):

$$m_{\text{I}} = \frac{GW}{3,6v_{\text{B}}} \quad (18)$$

where W is the length of the sampling frame, in metres (see [Clause 10](#)).

7 Methods of sampling from concentrate streams

7.1 General

Mechanical and manual sampling of concentrate streams may be carried out on either a mass-basis or a time-basis. This needs to be decided before designing a sampling system and before sampling commences.

7.2 Mass-basis systematic sampling

7.2.1 General

Mass-basis sampling involves the following steps:

- a) Distributing the required number of primary increments on a uniform tonnage basis throughout the lot to be sampled.
- b) Taking increments of almost uniform mass from each tonnage interval.

NOTE Sample masses are considered to be almost uniform if the coefficient of variation of the masses is 20 % or less. If increments are not of almost uniform mass, constant-mass division is required, so that the mass of sample reporting to the lot sample or subsample is almost uniform.

7.2.2 Sampling interval

The interval between primary increments for mass-basis sampling shall be determined from [Formula \(19\)](#):

$$\Delta m \leq \frac{m_L}{n_1} \quad (19)$$

where

Δm is the mass interval between primary increments, in tonnes;

m_L is the mass of the lot, in tonnes;

n_1 is the number of primary increments determined in accordance with [Clause 5](#).

The mass interval between primary increments should be rounded down to the nearest tonne, to ensure that the number of primary increments taken will be larger than the minimum number required.

7.2.3 Sample cutter

The following cutters may be used for taking primary increments:

- a falling-stream cutter whose cutting speed is constant during the course of handling the entire lot;
- a falling-stream cutter whose cutting speed is constant while cutting the stream but can be regulated, primary increment by primary increment, corresponding to the flow rate of the concentrate on the conveyor belt;
- a cross-belt cutter.

7.2.4 Taking of primary increments

Each primary increment shall preferably be taken by a single traverse of the sampling device, so that a full cross-section of the concentrate stream is taken. However, in manual-sampling cases where it is not possible to obtain a complete cross-section in one operation, increments may be taken systematically across the concentrate stream so that, when they are combined, they represent the full cross-section of the stream (see [9.7](#)).

The first primary increment shall be taken at a random mass, less than the mass interval Δm determined in [7.2.2](#). Thereafter, the required number of primary increments shall be taken at fixed mass intervals of Δm , and this interval shall not be changed during the entire course of sampling the lot.

If the planned number of primary increments has been taken and handling has not been completed, additional primary increments shall be taken at the same mass interval until the handling operation is completed.

7.2.5 Constitution of subsamples and lot samples

If the coefficient of variation of primary increment masses is 20 % or less, primary increments may be combined into subsamples or a lot sample, either as taken or after having been processed individually to a particular stage. Subsamples shall preferably comprise equal numbers of consecutive primary increments.

However, if the coefficient of variation of primary increment masses exceeds 20 %, either:

- each primary increment shall be subjected separately to division (according to the rules of division) and determination of its quality characteristics; or