



Designation: C 1499 – 05

Standard Test Method for Monotonic Equibiaxial Flexural Strength of Advanced Ceramics at Ambient Temperature¹

This standard is issued under the fixed designation C 1499; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This test method covers the determination of the equibiaxial strength of advanced ceramics at ambient temperature via concentric ring configurations under monotonic uniaxial loading. In addition, test specimen fabrication methods, testing modes, testing rates, allowable deflection, and data collection and reporting procedures are addressed. Two types of test specimens are considered: machined test specimens and as-fired test specimens exhibiting a limited degree of warpage. Strength as used in this test method refers to the maximum strength obtained under monotonic application of load. Monotonic loading refers to a test conducted at a constant rate in a continuous fashion, with no reversals from test initiation to final fracture.

1.2 This test method is intended primarily for use with advanced ceramics that macroscopically exhibit isotropic, homogeneous, continuous behavior. While this test method is intended for use on monolithic advanced ceramics, certain whisker- or particle-reinforced composite ceramics as well as certain discontinuous fiber-reinforced composite ceramics may also meet these macroscopic behavior assumptions. Generally, continuous fiber ceramic composites do not macroscopically exhibit isotropic, homogeneous, continuous behavior, and the application of this test method to these materials is not recommended.

1.3 Values expressed in this test method are in accordance with the International System of Units (SI) and Practice E 380.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate*

safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents

2.1 *ASTM Standards:*²

C 1145 Terminology of Advanced Ceramics

C 1239 Practice for Reporting Uniaxial Strength Data and Estimating Weibull Distribution Parameters for Advanced Ceramics

C 1259 Test Method for Dynamic Young's Modulus, Shear Modulus, and Poisson's Ratio for Advanced Ceramics by Impulse Excitation of Vibration

C 1322 Practice for Fractography and Characterization of Fracture Origins in Advanced Ceramics

E 4 Practices for Force Verification of Testing Machines

E 6 Terminology Relating to Methods of Mechanical Testing

E 83 Practice for Verification and Classification of Extensometer System

E 337 Test Method for Measuring Humidity with a Psychrometer (the Measurement of Wet- and Dry-Bulb Temperatures)

E 380 Practice for Use of International System of Units (SI) (The Modernized Metric System)

F 394 Test Method for Iron in Trace Quantities Using the 1,10-Phenanthroline Method³

3. Terminology

3.1 *Definitions*—The definitions of terms relating to biaxial testing appearing in Terminology E 6 and Terminology C 1145 may apply to the terms used in this test method. Pertinent

¹ This test method is under the jurisdiction of ASTM Committee C28 on Advanced Ceramics and is the direct responsibility of Subcommittee C28.01 on Mechanical Properties and Performance.

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Withdrawn.

definitions are listed below with the appropriate source given in parentheses. Additional terms used in conjunction with this test method are defined in the following section.

3.1.1 *advanced ceramic, n*—highly engineered, high performance predominately non-metallic, inorganic, ceramic material having specific functional attributes. **C 1145**

3.1.2 *breaking load, [F], n*—load at which fracture occurs. **E 6**

3.1.3 *equibiaxial flexural strength, [F/L₂], n*—maximum stress that a material is capable of sustaining when subjected to flexure between two concentric rings. This mode of flexure is a cupping of the circular plate caused by loading at the inner load ring and outer support ring. The equibiaxial flexural strength is calculated from the maximum-load of a biaxial test carried to rupture, the original dimensions of the test specimen, and Poisson's ratio.

3.1.4 *homogeneous, n*—condition of a material in which the relevant properties (composition, structure, density, etc.) are uniform, so that any smaller sample taken from an original body is representative of the whole. Practically, as long as the geometrical dimensions of a sample are large with respect to the size of the individual grains, crystals, components, pores, or microcracks, the sample can be considered homogeneous.

3.1.5 *modulus of elasticity, [F/L₂], n*—ratio of stress to corresponding strain below the proportional limit. **E 6**

3.1.6 *Poisson's ratio, n*—negative value of the ratio of transverse strain to the corresponding axial strain resulting from uniformly distributed axial stress below the proportional limit of the material.

4. Significance and Use

4.1 This test method may be used for material development, material comparison, quality assurance, characterization and design code or model verification.

4.2 Engineering applications of ceramics frequently involve biaxial tensile stresses. Generally, the resistance to equibiaxial flexure is the measure of the least flexural strength of a monolithic advanced ceramic. The equibiaxial flexural strength distributions of ceramics are probabilistic and can be described by a weakest link failure theory, **(1, 2)**⁴. Therefore, a sufficient number of test specimens at each testing condition is required for statistical estimation of the equibiaxial strength.

4.3 Equibiaxial strength tests provide information on the strength and deformation of materials under multiple tensile stresses. Multiaxial stress states are required to effectively evaluate failure theories applicable to component design, and to efficiently sample surfaces that may exhibit anisotropic flaw distributions. Equibiaxial tests also minimize the effects of test specimen edge preparation as compared to uniaxial tests because the generated stresses are lowest at the test specimen edges.

4.4 The test results of equibiaxial test specimens fabricated to standardized dimensions from a particular material and/or selected portions of a component may not totally represent the

strength properties in the entire, full-size component or its in-service behavior in different environments.

4.5 For quality control purposes, results derived from standardized equibiaxial test specimens may be considered indicative of the response of the bulk material from which they were taken for any given primary processing conditions and post-processing heat treatments or exposures.

5. Interferences

5.1 Test environment (vacuum, inert gas, ambient air, etc.) including moisture content (for example, relative humidity) may have an influence on the measured equibiaxial strength. Testing to evaluate the maximum strength potential of a material can be conducted in inert environments and/or at sufficiently rapid testing rates so as to minimize any environmental effects. Conversely, testing can be conducted in environments, test modes and test rates representative of service conditions to evaluate material performance under use conditions.

5.2 Fabrication of test specimens can introduce dimensional variations that may have pronounced effects on the measured equibiaxial mechanical properties and behavior (for example, shape and level of the resulting stress-strain curve, equibiaxial strength, failure location, etc.). Surface preparation can also lead to the introduction of residual stresses and final machining steps might or might not negate machining damage introduced during the initial machining. Therefore, as universal or standardized methods of surface preparation do not exist, the test specimen fabrication history should be reported. In addition, the nature of fabrication used for certain advanced ceramic components may require testing of specimens with surfaces in the as-fabricated condition (that is, it may not be possible, desired or required to machine some of the test specimen surfaces directly in contact with the test fixture). For very rough or wavy as-fabricated surfaces, perturbations in the stress state due to non-symmetric cross-sections as well as variations in the cross-sectional dimensions may also interfere with the equibiaxial strength measurement. Finally, close geometric tolerances, particularly in regard to flatness of test specimen surfaces in contact with the test fixture components are critical requirements for successful equibiaxial tests. In some cases it may be appropriate to use other test methods (for example, Test Method **F 394**).

5.3 Contact and frictional stresses in equibiaxial tests can introduce localized failure not representative of the equibiaxial strength under ideal loading conditions. These effects may result in either over or under estimates of the actual strength **(1, 3)**.

5.4 Fractures that consistently initiate near or just outside the load-ring may be due to factors such as friction or contact stresses introduced by the load fixtures, or via misalignment of the test specimen rings. Such fractures will normally constitute invalid tests (see **Note 14**). Splitting of the test specimen along a diameter that expresses the characteristic size may result from poor test specimen preparation (for example, severe grinding or very poor edge preparation), excessive tangential stresses at the test specimen edges, or a very weak material. Such fractures will constitute invalid tests if failure occurred from the edge.

⁴ The boldface numbers in parentheses refer to the list of references at the end of this standard.

5.5 Deflections greater than one-quarter of the test specimen thickness can result in nonlinear behavior and stresses not accounted for by simple plate theory.

5.6 Warpage of the test specimen can result in nonuniform loading and contact stresses that result in incorrect estimates of the test specimen's actual equibiaxial strength. The test specimen shall meet the flatness requirements (see 8.2 and 8.3) or be specifically noted as warped and considered as a censored test.

6. Apparatus

6.1 *Testing Machines*—Machines used for equibiaxial testing shall conform to the requirements of Practices E 4. The load cells used in determining equibiaxial strength shall be accurate within $\pm 1\%$ at any load within the selected load range of the testing machine as defined in Practice E 4. Check that the expected breaking load for the desired test specimen geometry and test material is within the capacity of the test machine and load cell. Advanced ceramic equibiaxial test specimens require greater loads to fracture than those usually encountered in uniaxial flexure of test specimens with similar cross sectional dimensions.

6.2 *Loading Fixtures for Concentric Ring Testing*—An assembly drawing of a fixture and a test specimen is shown in Fig. 1, and the geometries of the load and support rings are given in Fig. 2.

6.2.1 *Loading Rods and Platens*—Surfaces of the support platen shall be flat and parallel to 0.05 mm. The face of the load rod in contact with the support platen shall be flat to 0.025 mm. In addition, the two loading rods shall be parallel to 0.05 mm per 25 mm length and concentric to 0.25 mm when installed in the test machine.

6.2.2 *Loading Fixture and Ring Geometry*—Ideally, the bases of the load and support fixtures should have the same

outer diameter as the test specimen for ease of alignment. Parallelism and flatness of faces as well as concentricity of the load and support rings shall be as given in Fig. 2. The ratio of the load ring diameter, D_L , to that of the support ring, D_S , shall be $0.2 \leq D_L/D_S \leq 0.5$. For test materials exhibiting low elastic modulus ($E < 100$ GPa) and high strength ($\sigma_f > 1$ GPa) it is recommended that the ratio of the load ring diameter to that of the support ring be $D_L/D_S = 0.2$. The sizes of the load and support rings depend on the dimensions and the properties of the ceramic material to be tested. The rings are sized to the thickness, diameter, strength, and elastic modulus of the ceramic test specimens (see Section 8). For test specimens made from typical substrates ($h \approx 0.5$ mm), a support ring diameter as small as 12 mm may be required. For test specimens to be used for model verification, it is recommended that the test specimen support diameter be at least 35 mm. The tip radius, r , of the cross sections of the load and support rings should be $h/2 \leq r \leq 3h/2$.

6.2.3 *Load and Support Ring Materials*—For machined test specimens (see Section 8) the load and support fixtures shall be made of hardened steel of $HR_C > 40$. For as-fabricated test specimens, the load/support rings shall be made of steel or acetyl polymer.

6.2.4 *Compliant Layer and Friction Elimination*—The brittle nature of advanced ceramics and the sensitivity to misalignment, contact stresses and friction may require a compliant interface between the load/support rings and the test specimen, especially if the test specimen is not flat. Line or point contact stresses and frictional stresses can lead to crack initiation and fracture of the test specimen at stresses other than the actual equibiaxial strength.

6.2.4.1 *Machined Test Specimens*—For test specimens machined according to the tolerance in Fig. 3, a compliant layer is not necessary. However, friction needs to be eliminated. Place a sheet of carbon foil (~ 0.13 mm thick) or Teflon tape (~ 0.07 mm thick) between the compressive and tensile surfaces of the test specimen and the load and support rings.

NOTE 1—Thicker layers of carbon foil or Teflon tape may be used, particularly for very strong plates. However, excessively thick layers will redistribute the contact region and may affect results. The thicknesses listed above have been used successfully. Guidance regarding the use of thick layers cannot be given currently; some judgement may be required.

Alternatively, an appropriate lubricant (anti-seizing compound or Teflon oil) may be used to minimize friction. The lubricant should be placed only on the load and support rings so that effects of the test environment are not significantly altered. To aid fractographic examination, place a single strip of adhesive tape with a width of D_L or greater on the compressive face of the test specimen. Do not use multiple strips of tape, or a strip of tape with width less than D_L , as this may result in nonuniform loading.

6.2.4.2 *As-Fabricated Test Specimens*—If steel load and support rings are used to test as-fabricated test specimens (for example, as-fired ceramics and glass test specimens), minimize the effects of test specimen-ring misalignment by placing a sheet of rubber or silicone (shore hardness of 60 ± 5) of approximately one-half the test specimen thickness between the test specimen and the support ring. To aid fracture

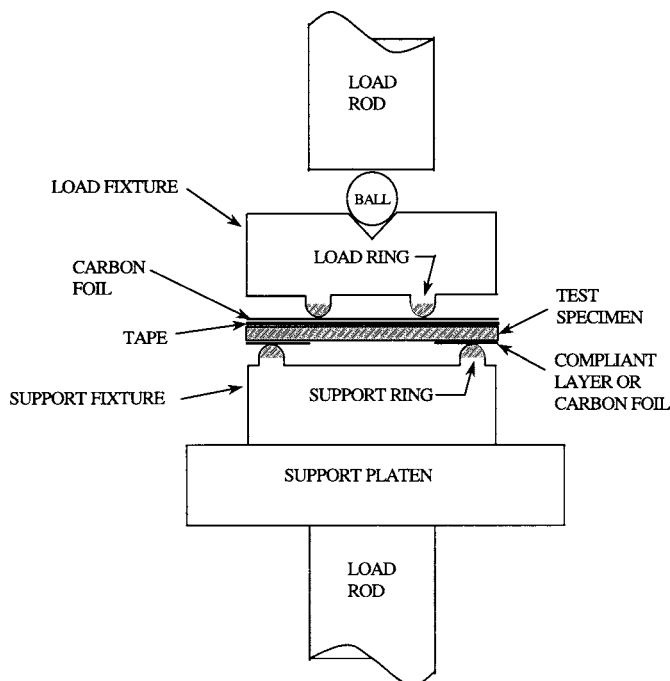
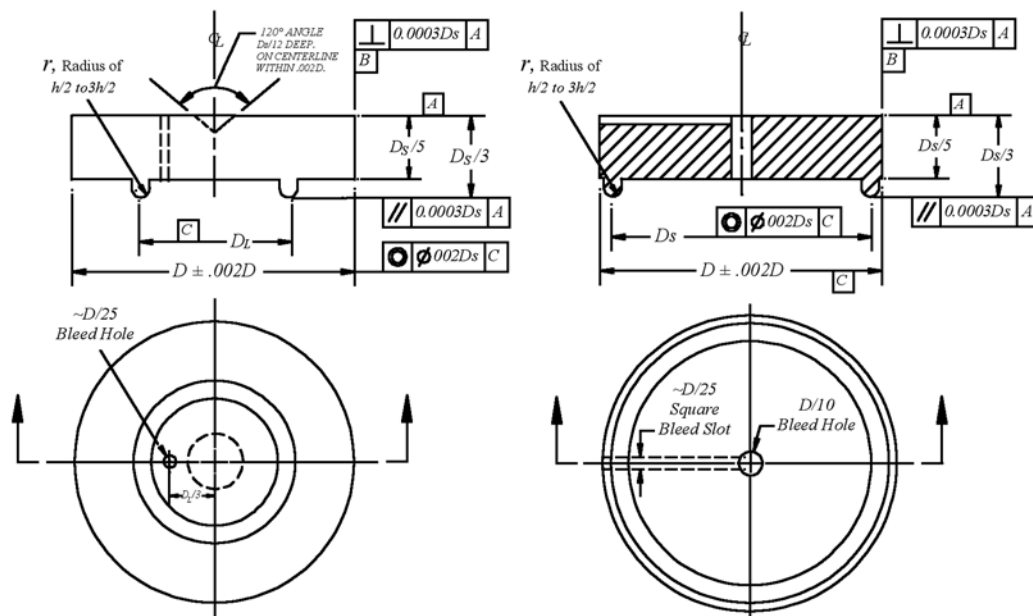
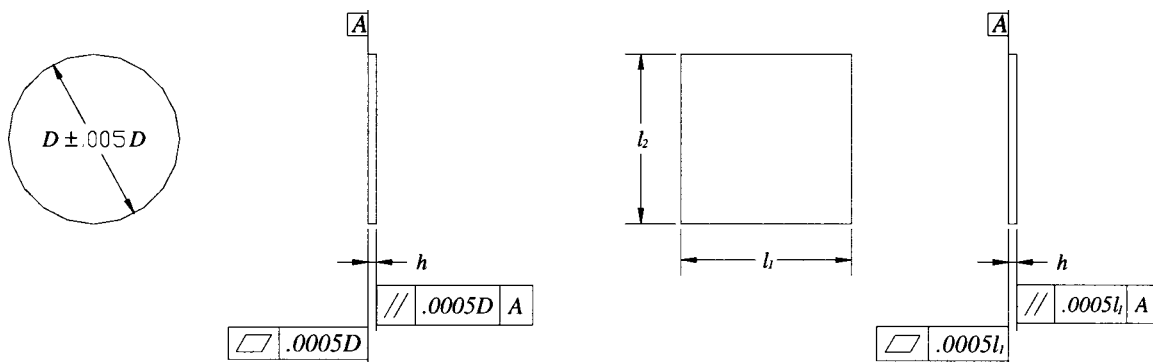


FIG. 1 Section View of Basic Fixturing and Test Specimen for Equibiaxial Testing



NOTE—0.4 to 0.8 μm surface finish. Harden to 40 Rc or greater.

FIG. 2 Load and Support Fixture Designs for Equibiaxial Testing



Round Test Specimen

FIG. 3 Recommended Equibiaxial Test Specimen Geometry (h and D or l_1 and l_2 are Determined from Eq 1-3).

examination, place a single strip of adhesive tape with a width of D_L or greater on the compressive face of the test specimen. Do not use multiple strips of tape, or a strip of tape with width less than D_L , as this may result in nonuniform loading. To minimize the effects of friction at the load ring interface, place a sheet of carbon foil or TFE-fluorocarbon tape between the compressive surface of the test specimen and the load-ring. Alternatively, an appropriate lubricant (anti-seizing compound or TFE-fluorocarbon oil) may be used to minimize friction at the load ring. If acetyl polymer load rings are used, a compliant layer is not required. Minimize the effects of friction at the load ring interface, by placing a sheet of carbon foil or TFE-fluorocarbon tape between the compressive and tensile surfaces of the test specimen and the load and support rings. Alterna-

tively, an appropriate lubricant (anti-seizing compound or TFE-fluorocarbon oil) may be used to minimize friction at the load ring.

NOTE 2—As-fabricated test specimens that meet the flatness requirements in Fig. 3 may be tested as described in 6.2.4.1. A compliant layer is not necessary.

NOTE 3—The use of acetyl polymer load rings can result in sufficiently low friction (4) so that no layer is required. If the friction coefficient is less than 0.05, then the friction reduction layer may be eliminated.

6.3 Alignment—The load ring and support ring shall be aligned concentrically to 0.5 % of the support ring diameter. The test specimen shall be concentric with the load and support rings to 2 % of the support ring diameter.