



Designation: E1816 – 07

Standard Practice for Ultrasonic Testing Using Electromagnetic Acoustic Transducer (EMAT) Techniques¹

This standard is issued under the fixed designation E1816; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This practice covers procedures for the use of electromagnetic acoustic transducers (EMATs) for specific ultrasonic examination applications. Recommendations are given for specific applications for using EMAT techniques to detect flaws through both surface and volumetric examinations as well as to measure thickness.

1.2 These procedures recommend technical details and guidelines for the reliable and reproducible ultrasonic detection of flaws and thickness measurements using electromagnetic acoustic transducers for both the pulsing and receiving of ultrasonic waves. The EMAT techniques described herein can be used as a basis for assessing the serviceability of various components nondestructively, as well as for process control in manufacturing.

1.3 These procedures cover noncontact techniques for coupling ultrasonic energy into materials through the use of electromagnetic fields. Surface, Lamb, longitudinal, and shear wave modes are discussed.

1.4 These procedures are intended to describe specific EMAT applications. These procedures are intended for applications in which the user has determined that the use of EMAT techniques can offer substantial benefits over conventional piezoelectric search units. It is not intended that EMAT techniques should be used in applications in which conventional techniques and applications offer superior benefits (refer to Guide E1774).

1.5 These procedures are applicable to any material in which acoustic waves can be introduced electromagnetically. This includes any material that is either electrically conductive or ferromagnetic.

1.6 The procedures outlined in this practice address proven EMAT techniques for specific applications; they do not purport to address the only variation or all variations of EMAT

techniques to address the given applications. Latitude in application techniques is offered where options are considered appropriate.

1.7 The values stated in inch-pound units are to be regarded as the standard. The values given in parentheses are for information only.

1.8 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

E114 Practice for Ultrasonic Pulse-Echo Straight-Beam Contact Testing

E494 Practice for Measuring Ultrasonic Velocity in Materials

E587 Practice for Ultrasonic Angle-Beam Contact Testing

E797 Practice for Measuring Thickness by Manual Ultrasonic Pulse-Echo Contact Method

E1316 Terminology for Nondestructive Examinations

E1774 Guide for Electromagnetic Acoustic Transducers (EMATs)

2.2 ASNT Standards:³

SNT-TC-1A Recommended Practice for Personnel Qualifications and Certification in Nondestructive Testing

ANSI/ASNT CP-189 Standard for Qualification and Certification of Nondestructive Testing Personnel

2.3 Military Standard:

MIL-STD-410 Nondestructive Testing Personnel Qualification and Certification⁴

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Available from American Society for Nondestructive Testing (ASNT), P.O. Box 28518, 1711 Arlingate Ln., Columbus, OH 43228-0518, <http://www.asnt.org>.

⁴ Available from Standardization Documents Order Desk, DODSSP, Bldg. 4, Section D, 700 Robbins Ave., Philadelphia, PA 19111-5098, <http://www.dodssp.daps.mil>.

¹ This practice is under the jurisdiction of ASTM Committee E07 on Nondestructive Testing and is the direct responsibility of Subcommittee E07.06 on Ultrasonic Method.

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3. Terminology

3.1 *Definitions*—Related terminology is defined in Terminology E1316.

3.2 *Definitions of Terms Specific to This Standard:*

3.2.1 *bulk wave*—an ultrasonic wave, either longitudinal or shear mode, used in nondestructive testing to interrogate the volume of a material.

3.2.2 *electromagnetic acoustic transducer (EMAT)*—an electromagnetic device for converting electrical energy into acoustical energy in the presence of a magnetic field.

3.2.3 *lift-off effect*—refer to Terminology E1316, Section C.

3.2.4 *Lorentz forces*—forces applied to electric currents when placed in a magnetic field. Lorentz forces are perpendicular to both the direction of the magnetic field and the current direction. Lorentz forces are the forces responsible behind the principle of electric motors.

3.2.5 *magnetostrictive forces*—forces arising from magnetic domain wall movements within a magnetic material during magnetization.

3.2.6 *meander coil*—an EMAT coil consisting of periodic, winding, nonintersecting, and usually evenly spaced conductors.

3.2.7 *pancake (spiral) coil*—an EMAT coil consisting of spirally wound, usually evenly spaced conductors.

4. Summary of Practice

4.1 *Surface Examination:*

4.1.1 The generation of Rayleigh or surface waves in the material to be examined allows for sensitivity to surface flaws and discontinuities. Flaws can be detected by reflections of acoustic waves from the discontinuity interfaces or by acoustic wave attenuation in traversing across the surface of the component. Either pulse-echo or pitch-catch ultrasonic techniques can be used.

4.1.2 Fig. 1 shows a typical EMAT setup for the transduction of Rayleigh or Lamb waves. As shown, an external magnetic induction B is applied parallel to the surface of an electrically conductive or ferromagnetic material. A meander coil is used. The coil is oriented in the same plane as the surface of the material and is excited by an electrical radio frequency (RF) pulse. A surface current is produced in the material by transformer action. The surface current, in the presence of the magnetic field, experiences Lorentz forces that

produce oscillating stress waves perpendicular to the surface of the material to produce surface acoustic waves. Basic EMAT designs generate bidirectional surface waves. Specialized designs can be used to generate unidirectional waves, as with conventional ultrasonic examination.

4.1.3 Surface flaws or discontinuities lead to reflections or attenuation of the surface waves. Upon approach to the receiver EMAT, the reflected or attenuated ultrasonic waves produce oscillations within the conductor in the presence of the magnetic field and thus produce a voltage induction in the coil, allowing for detection.

4.2 *Volumetric Examination:*

4.2.1 Sensitivity to flaws or discontinuities within a part requires the use of bulk acoustic wave modes to interrogate the volume of the material. As with surface examinations, reliance on the reflection or attenuation of acoustic waves from discontinuity interfaces forms the basis for the detection of flaws.

4.2.2 Depending on the particular application, either longitudinal or shear wave modes may be desirable. While straight beam applications using pulse-echo techniques are the most straightforward, angle beam pitch-catch techniques could be desirable, depending on such factors as expected flaw location and orientation.

4.2.3 Fig. 2 shows one typical EMAT setup for the transduction of bulk waves. As shown, an external magnetic induction B is applied normal to the surface of an electrically conductive or ferromagnetic material. A spiral EMAT coil is used for this example. The coil is positioned in a plane parallel to the surface of the material and is excited by an electrical current pulse. A surface current is produced in the material by transformer action. The surface current, in the presence of the magnetic field, experiences Lorentz forces that produce oscillating stress waves originating in the surface of the material. Radially polarized shear waves are generated for this example. Depending on the design characteristics of the magnetic field, the excitation of either radially polarized or planar-polarized shear waves, propagating normal to the surface, can be introduced. Longitudinal wave modes can also be generated and used effectively in non-ferromagnetic materials. Longitudinal wave generation in ferromagnetic materials is impractical due to unacceptably low coupling efficiency. Mode-converted longitudinal waves can be used effectively. Paragraph 7.2 and

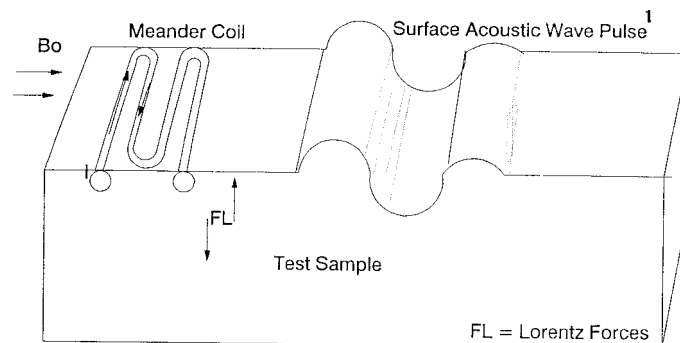


FIG. 1 Typical EMAT Configuration for Rayleigh or Lamb Wave Generation

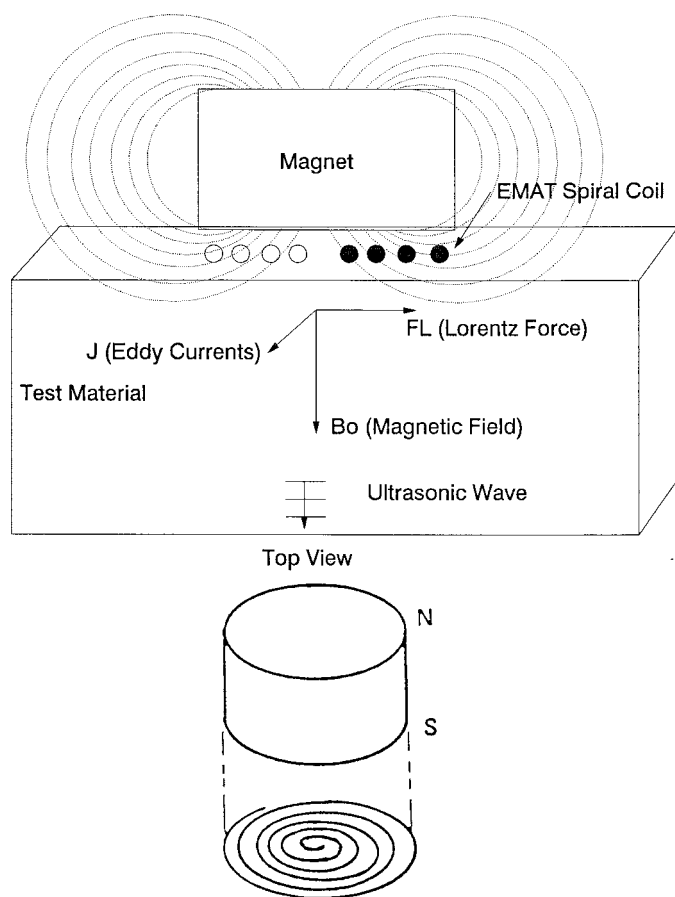


FIG. 2 Typical EMAT Configuration for Bulk Wave Generation

the subparagraphs of 7.2 give a more in-depth discussion of the various EMAT/magnet configurations for producing various bulk wave modes.

4.3 Thickness Gaging:

4.3.1 Determining the thickness of a material by ultrasonic means is a matter of coupling an ultrasonic wave into the material, allowing the sound wave to propagate through the material, reflect from the backwall boundary interface of the material, and propagate back to the front surface. The thickness of the material can be calculated by measuring the transit time of the ultrasonic wave, and through knowledge of the ultrasonic wave velocity. Thickness measurements can also be extrapolated for a given material through standardizations of transit time as a function of thickness as derived from a standardization block (see Practice E797 and 7.3.1).

4.3.2 The ultrasonic velocity of the material under examination is a function of the physical properties of the material, namely, stiffness and density. It is usually assumed to be constant for a given class of materials. Approximate velocity values are available in tabular format from numerous sources, including the ASNT *Nondestructive Testing Handbook*.⁵ Velocity values can also be determined empirically (see Practice E494).

⁵ *Nondestructive Testing Handbook*, 2nd ed., Vol 7, *Ultrasonic Testing*, A. S. Birks, R. E. Green, and P. McIntire, eds., American Society for Nondestructive Testing, Columbus, OH, 1991.

4.3.3 Determination of the transit time of an acoustic wave through a material requires the use of bulk acoustic wave modes. While longitudinal waves can be used, it is often desirable to use shear waves since their slower propagation velocities lend themselves to more accurate measurements of thin materials. While straight beam applications using pulse-echo techniques are the most straightforward and popular, angle beam pitch-catch techniques could be desirable, especially in applications in which fast scan rates are needed or high resolution is desired for thin material. The generation of bulk waves by means of the EMAT technique is discussed in 4.2.3 and depicted in Fig. 2.

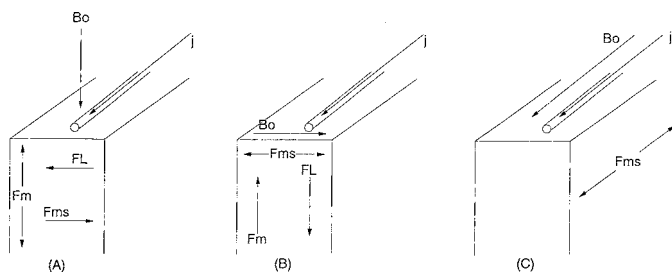
5. Significance and Use

5.1 Since EMAT techniques are noncontacting, they should be considered for ultrasonic examinations in which applications involve automation, high-speed examinations, moving objects, applications in remote or hazardous locations, and applications to objects at elevated temperatures or objects with rough surfaces. This practice describes procedures for using EMAT techniques as associated with the ultrasonic method to detect flaws for both surface and volumetric examinations as well as to measure thickness.

5.2 The uniqueness of the electromagnetic acoustic transducer technique for ultrasonic examination basically lies in the generation and reception of the ultrasonic waves. Otherwise, conventional ultrasonic techniques and methodologies generally apply.

5.3 An EMAT generates and receives acoustic waves in a material by electromagnetic means; electrically conductive or ferromagnetic materials can be examined. In its simplest form, an EMAT as a generator of ultrasonic waves is basically a coil of wire, excited by an alternating current, and placed in a uniform magnetic field near the surface of a material. For conductive materials, eddy currents are induced as a result of the alternating current. Due to the magnetic field, these eddy currents experience Lorentz forces that in turn are transmitted to the solid by collisions with the lattice or other microscopic processes. These forces are alternating at the frequency of the driving current and act as a source of ultrasonic waves. If the material is ferromagnetic, additional coupling mechanisms play a part in the generation of ultrasonic waves. Interactions between the dynamic magnetic field generated by the alternating currents and the magnetization associated with the material offer a source of coupling, as do the associated magnetostrictive influences. Reciprocal processes exist whereby all of these mechanisms lead to detection. Fig. 3 depicts the mechanisms (forces), along with associated direction, for electromagnetic ultrasound generation.

5.4 The EMAT can be used to generate all ultrasonic modes of vibration. As with conventional ultrasonic techniques, material types, probable flaw locations, and flaw orientations determine the selection of beam directions and modes of vibration. The use of EMATs and selection of the proper wave mode presuppose a knowledge of the geometry of the object; the probable location, size, orientation, and reflectivity of the expected flaws; the allowable range of EMAT lift-off; and the laws of physics governing the propagation of acoustic waves.



NOTE 1— j = current in a single conductor, B_o = magnetization from external magnet, F_m = magnetic force (ferromagnetic material), F_{ms} = magnetostrictive force (ferromagnetic material), and F_L = Lorentz force (conductive material).

FIG. 3 Mechanisms of Electromagnetic Ultrasound Generation

5.5 The EMAT techniques show benefits and advantages over conventional piezoelectric ultrasonic techniques in special applications in which flexibility in the type of wave mode generation is desired. The EMATs are highly efficient in generating surface waves. The EMATs lend themselves to horizontally polarized shear wave (SH) generation more easily than do conventional ultrasonic search units. This is important since SH shear waves produce no mode conversions at interfaces and their angle of introduction can be varied from 0 to 90° simply by sweeping through various frequency RF generation. The EMATs can also be configured to produce Lamb wave modes whose use can provide the full circumferential examination of tubular products or volumetric examination of thin plate material. The EMATs also lend themselves easily to the repeatability of sensor fabrication, and hence the associated sensor response is highly reproducible.

6. Basis of Application

6.1 *Personnel Qualification*—Nondestructive testing (NDT) personnel shall be qualified in accordance with a nationally recognized NDT personnel qualification practice or standard such as ANSI/ASNT CP-189, SNT-TC-1A, MIL-STD-410, or a similar document. The practice or standard used and its applicable revision shall be specified in the contractual agreement between the using parties.

6.2 *Procedures and Techniques*—The procedures and techniques to be used shall be as described in this practice unless otherwise specified. Specific techniques may be specified in the contractual agreement.

6.3 *Reporting Criteria and Acceptance Criteria*—Reporting criteria for the examination results shall be in accordance with Section 11 unless otherwise specified. Acceptance criteria shall be specified in the contractual agreement.

6.4 *Reexamination of Repaired and Re-Worked Items*—The reexamination of repaired and reworked items is not addressed in this practice and, if required, shall be specified in the contractual agreement.

7. Apparatus

7.1 Surface Examinations:

7.1.1 Base Material Applications:

7.1.1.1 *EMAT Coil Design*—Fig. 4 shows a typical meander EMAT coil design for Rayleigh wave transduction. The mode of operation can be either pulse-echo or pitch-catch.

7.1.1.2 *Coil Excitation*—A high-power, specialized RF generator is necessary to provide excitation to the coil in the form of a toneburst of several cycles.

7.1.1.3 *Magnetization*—Fig. 5 shows a typical electromagnet configuration for producing an external magnetic induction for the meander coil. A pulsed magnetic induction is produced parallel to the examination surface for the particular design shown. An accompanying magnet pulser and power supply unit are needed to supply the current pulse to the pulsed magnet. It should be noted that magnetization could be supplied from a permanent magnet or from a dc magnet with power supply.

7.1.1.4 *Instrumentation*—The following is a description of a typical instrumentation package for data acquisition and analysis of the EMAT signals. The signal processing and data acquisition electronics should consist of a receiver section to provide for adjustable gain and filtering for the EMAT signals. Conventional ultrasonic instruments can be used for this purpose. The user has several options to capture and analyze the EMAT signals. A personal computer housing any of several commercially available analog-to-digital converter boards with associated dedicated ultrasonics software provides for an effective configuration. However, as with conventional ultrasonics, configurations as simple as analog output to oscilloscope can provide for acceptable results. In either case, pulser/receiver synchronization circuitry will be necessary to provide adequate triggering for signal acquisition.

7.1.1.5 *Reference Standard*—A reference standard for verification of the system standardization should be prepared from a component of the same material, thickness, surface finish, and nominal heat treatment as the material to be examined. The material should be free of discontinuities or other abnormal conditions other than those reference reflectors exemplifying the necessary sensitivity. Flaw dimensions of length, depth,

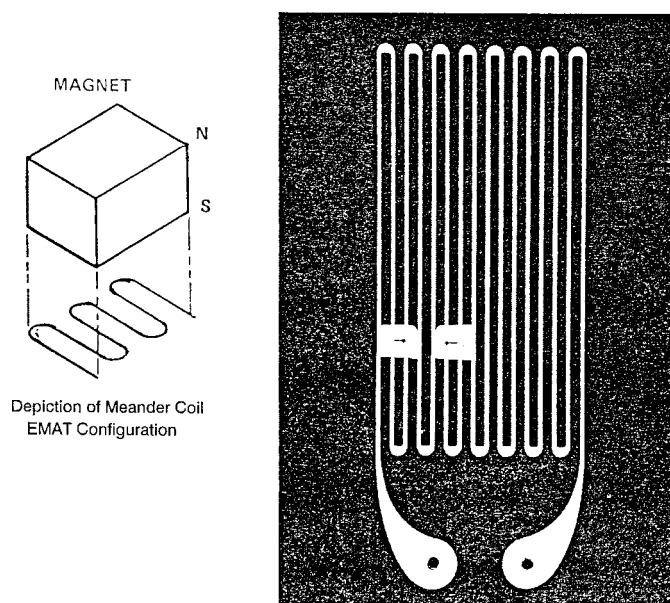


FIG. 4 Typical EMAT Meander Coil for Rayleigh Wave Generation