



Standard Test Method for Surface Burning Characteristics of Building Materials¹

This standard is issued under the fixed designation E 84; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (^ε) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the Department of Defense. Consult the DoD Index of Specifications and Standards for the specific year of issue which has been adopted by the Department of Defense.

^{ε1} NOTE—Editorial changes were made in Sections 5, 6, and 9 in July 1998.

1. Scope

1.1 This fire-test-response standard for the comparative surface burning behavior of building materials is applicable to exposed surfaces such as walls and ceilings. The test is conducted with the specimen in the ceiling position with the surface to be evaluated exposed face down to the ignition source. The material, product, or assembly shall be capable of being mounted in the test position during the test. Thus, the specimen shall either be self-supporting by its own structural quality, held in place by added supports along the test surface, or secured from the back side.

1.2 The purpose of this test method is to determine the relative burning behavior of the material by observing the flame spread along the specimen. Flame spread and smoke developed index are reported. However, there is not necessarily a relationship between these two measurements.

1.3 The use of supporting materials on the underside of the test specimen may lower the flame spread index from that which might be obtained if the specimen could be tested without such support, and the test results do not necessarily relate to indices obtained by testing materials without such support.

1.4 This test method may not be appropriate for obtaining comparative surface burning behavior of some cellular plastic materials.

1.5 Testing of materials that melt, drip, or delaminate to such a degree that the continuity of the flame front is destroyed, results in low flame spread indices that do not relate directly to indices obtained by testing materials that remain in place.

1.6 The values stated in inch-pound units are to be regarded as the standard.

1.7 The text of this standard references notes and footnotes that provide explanatory information. These notes and footnotes, excluding those in tables and figures, shall not be considered as requirements of the standard.

1.8 *This standard is used to measure and describe the response of materials, products, or assemblies to heat and flame under controlled conditions, but does not by itself incorporate all factors required for fire-hazard or fire-risk assessment of the materials, products, or assemblies under actual fire conditions.*

1.9 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:

- A 390 Specification for Zinc-Coated (Galvanized) Steel Poultry Fence Fabric (Hexagonal and Straight Line)²
- D 4442 Test Methods for Direct Moisture Content Measurement of Wood and Wood-Base Materials³
- D 4444 Test Methods for Use and Calibration of Hand-Held Moisture Meters³
- E 69 Test Method for Combustible Properties of Treated Wood by the Fire-Tube Apparatus³
- E 160 Test Method for Combustible Properties of Treated Wood by the Crib Test⁴
- E 162 Test Method for Surface Flammability of Materials Using a Radiant Heat Energy Source⁵
- E 176 Terminology of Fire Standards⁵
- E 286 Test Method for Surface Flammability of Building Materials Using an 8-ft (2.44-m) Tunnel Furnace⁶

3. Terminology

3.1 *Definitions*—For definitions of terms used in this test method refer to Terminology E 176. The term flame spread index from Terminology E 176 is of particular interest to this standard and is defined in 3.1.1.1.

3.1.1 *flame spread index, n*—a number or classification indicating a comparative measure derived from observations made during the progress of the boundary of a zone of flame under defined test conditions.

3.2 Definitions of Terms Specific to This Standard:

3.2.1 *smoke developed index, n*—a number or classification indicating a comparative measure derived from smoke obscuration data collected during the test for surface burning characteristics.

3.2.2 *surface flame spread, n*—the propagation of a flame away from the source of ignition across the surface of the specimen.

¹ This test method is under the jurisdiction of ASTM Committee E-5 on Fire Standards and is the direct responsibility of Subcommittee E05.22 on Surface Burning.

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² Annual Book of ASTM Standards, Vol 01.06.

³ Annual Book of ASTM Standards, Vol 04.10.

⁴ Discontinued; see 1993 Annual Book of ASTM Standards, Vol 04.09.

⁵ Annual Book of ASTM Standards, Vol 04.07.

⁶ Discontinued; see 1991 Annual Book of ASTM Standards, Vol 04.02.

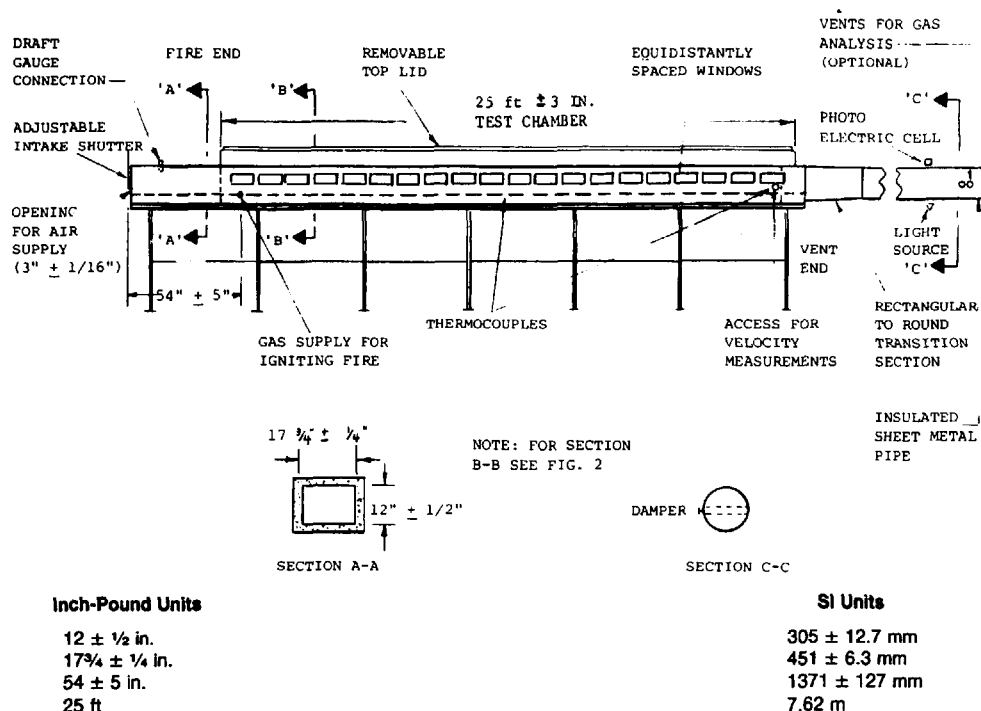


FIG. 1 Test Furnace, Showing Some Critical Dimensions (Not a Construction Drawing)

4. Significance and Use

4.1 This test method is intended to provide only comparative measurements of surface flame spread and smoke density measurements with that of select grade red oak and inorganic reinforced cement board⁷ surfaces under the specific fire exposure conditions described herein.

4.2 This test method exposes a nominal 24-ft (7.32-m) long by 20-in. (508-mm) wide specimen to a controlled air flow and flaming fire exposure adjusted to spread the flame along the entire length of the select grade red oak specimen in 5 1/2 min.

4.3 This test method does not provide for the following:

4.3.1 Measurement of heat transmission through the tested surface.

4.3.2 The effect of aggravated flame spread behavior of an assembly resulting from the proximity of combustible walls and ceilings.

4.3.3 Classifying or defining a material as noncombustible, by means of a flame spread index by itself.

5. Apparatus

5.1 *Fire Test Chamber*—See Figs. 1 and 2.

5.1.1 The fire test chamber shall consist of a horizontal duct having an inside width of 17 3/4 ± 1/4 in. (451 ± 6.3 mm) measured at ledge location along side walls and 17 5/8 ± 3/8 in. (448 ± 10 mm) at all other points; a depth of 12 ± 1/2 in. (305 ± 13 mm) measured from the bottom of the test chamber to the ledge of the inner walls on which the specimen is supported (including the 1/8-in. (3.2-mm) thickness of woven

fiberglass⁸ gasketing tape); and a length of 25 ft (7.62 m). The sides and base of the duct shall be lined with an insulating masonry material as illustrated in Fig. 2, consisting of A. P. Green, G-26⁹ refractory fire brick. One side shall be provided with double observation windows¹⁰ with the inside pane flush mounted (See Fig. 2). Exposed inside glass shall be 2 3/4 ± 3/8 by 11 + 1, -2 in. (70 ± 10 by 279 + 25 - 50 mm). The centerline of the exposed area of the inside glass shall be in the upper half of the furnace wall, with the upper edge not less than 2.5 in. (63 mm) below the furnace ledge. The window shall be located such that not less than 12 in. (305 mm) of the specimen width can be observed. Multiple windows shall be located along the tunnel so that the entire length of the test sample is observable from outside the fire chamber. The windows shall be pressure tight in accordance with 7.2 and 7.2.1.

5.1.2 The ledges shall be fabricated of structural materials¹¹ capable of withstanding the abuse of continuous testing, level with respect to the length and width of the chamber and each other, and maintained in a state of repair commensurate with the frequency, volume, and severity of testing occurring at any time.

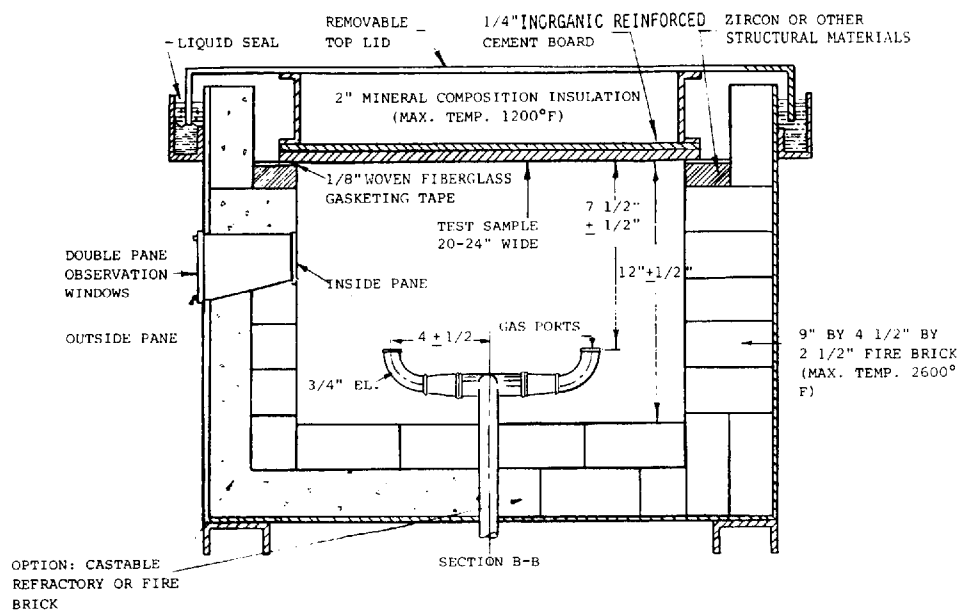
⁸ The sole source of supply of the apparatus known to the committee at this time is McMaster-Carr, P.O. Box 54960, Los Angeles, CA 90054. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

⁹ The sole source of supply of the apparatus known to the committee at this time is A. P. Green Refractories, Green Blvd., Mexico, MO 65265. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

¹⁰ Heat-resistant glass. High-silica, 100 % silica glass, nominal 1/4 in. thick, has been found suitable for the interior pane; borosilicate glass, nominal 1/4 in. thick, has been found suitable for the exterior pane.

¹¹ High-temperature furnace refractory. Zirconium silicate has been found suitable for this purpose.

⁷ The sole source of supply of the apparatus known to the committee at this time is CEM-FIL Corp., 120 Spence Lane, Nashville, TN 37210. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.



Inch-Pound Units	SI Units	Inch-Pound Units	SI Units
1/4 in.	6.3 mm	20 in.	508 mm
2 in.	51 mm	9 by 4 1/2 by 2 1/2 in.	230 by 115 by 65 mm
4 ± 1/2 in.	102 ± 13 mm	1200°F	649°C
7 1/2 ± 1/2 in.	191 ± 13 mm	2600°F	1427°C
12 ± 1/2 in.	305 ± 13 mm		

FIG. 2 Test Furnace Showing Some Critical Dimensions (Section "B-B" is not a Construction Drawing)

5.1.3 To provide air turbulence for proper combustion, turbulence baffling shall be provided by positioning six A. P. Green, G-26⁹ refractory fire bricks (long dimension vertical, 4 1/2-in. (114-mm) dimension along the wall) along the side walls of the chamber at distances of 7, 12, and 20 ± 1/2 ft (2.1, 3.7, and 6.1 ± 0.2 m) on the window side and 4 1/2, 9 1/2, and 16 ± 1/2 ft (1.3, 2.9, and 4.9 ± 0.2 m) on the opposite side.

5.1.4 The lid shall consist of a removable noncombustible metal and mineral composite structure as shown in Fig. 2 and of a size necessary to cover completely the fire test chamber and the test samples. The lid shall be maintained in an unwarping and flat condition. When in place, the lid shall be completely sealed to prevent air leakage into the fire test chamber during the test.

5.1.4.1 The lid shall be insulated with nominal 2 in. (51 mm) thick mineral composition material¹² having physical characteristics comparable to the following:

Maximum effective use temperature of at least:	1200°F (650°C)
Bulk density	21 lb/ft ³ (336 kg/m ³)
Thermal conductivity at 300 to 700°F (149 to 371°C)	0.50 to 0.71 Btu·in./h·°F (0.072 to 0.102 W/m·K)
K _{ρC} product: ⁴	1 to 4 $\frac{\text{btu}^2 \cdot \text{in.}}{\text{ft}^3 \cdot \text{h} \cdot ^\circ\text{F}^2} \left(1 \times 10^4 \right)$ to 4 × 10 ⁴ $\frac{\text{W}^2 \cdot \text{S}}{\text{m}^4 \cdot \text{K}^2}$

⁴ K_{ρC} is equal to the thermal conductivity times the density times the specific heat.

¹² The sole source of supply of the apparatus known to the committee at this time is A. P. Green Refractories, Green Blvd., Mexico, Mo 65265. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

5.1.4.2 The entire lid assembly shall be protected with flat sections of high-density (nominal 110 lb/ft³ or 1761 kg/m³) 1/4-in. (6.3-mm) inorganic reinforced cement board,⁷ maintained in an unwarping and uncracked condition through continued replacement. The protective board is to be secured to the furnace lid or placed on the back side of the test specimen.

5.1.5 One end of the test chamber, designated as the fire end, shall be provided with two gas burners delivering flames upward against the surface of the test sample. The burners shall be spaced 12 in. (305 mm) from the fire end of the test chamber, and 7 1/2 ± 1/2 in. (190 ± 13 mm) below the under surface of the test sample. The air intake shutter shall be located 54 ± 5 in. (1372 ± 127 mm) upstream of the burner, as measured from the burner centerline to the outside surface of the shutter. Gas to the burners shall be provided through a single inlet pipe, distributed to each port burner through a tee-section. The outlet shall be a 3/4-in. elbow. The plane of the port shall be parallel to the furnace floor, such that the gas is directed upward toward the specimen. Each port shall be positioned with its centerline 4 ± 1/2 in. (102 ± 13 mm) on each side of the centerline of the furnace so that the flame is evenly distributed over the width of the exposed specimen surface (see Fig. 2). The controls used to assure constant flow of gas to the burners during period of use shall consist of a pressure regulator, a gas meter calibrated to read in increments of not more than 0.1 ft³ (2.8 L), a manometer to indicate gas pressure in inches of water, a quick-acting gas shut-off valve, a gas metering valve, and an orifice plate in combination with a water manometer to assist in maintaining uniform gas flow conditions. An air intake fitted with a vertically sliding shutter extending the entire width of the test chamber shall be provided at the fire end of the furnace.

shall be positioned so as to provide an air inlet port $3 \pm \frac{1}{16}$ in. (76 ± 2 mm) high measured from the floor level of the test chamber at the air intake point.

5.1.6 The other end of the test chamber, designated as the "vent end," shall be fitted with a gradual rectangular-to-round transition piece, not less than 20 in. (508 mm) in length, with a cross-sectional area of not less than 200 in.² (1290 cm²) at any point. The transition piece shall in turn be fitted to a 16-in. (406-mm) diameter flue pipe. The movement of air shall be by an induced draft system having a total draft capacity of at least 0.15-in. (3.8-mm) water column with the sample in place, the shutter at the fire end open the normal $3 \pm \frac{1}{16}$ in. (76 ± 2 mm), and the damper in the wide open position. A draft gage tap to indicate static pressure shall be inserted through the top at the midwidth of the tunnel, 1 ± 0.5 in. (25 ± 12 mm) below the ceiling, 15 ± 0.5 in. (381 ± 12 mm) downstream from the inlet shutter.

5.1.7 Photometer System:

5.1.7.1 A photometer system consisting of a lamp¹³ and photocell¹⁴ shall be mounted on a horizontal section of the 16-in. (406-mm) diameter vent pipe at a point where it will be preceded by a straight run of pipe (at least 12 diameters or 16 ft (4.88 m) and not more than 30 diameters or 40 ft (12.19 m)) from the vent end of the chamber, and with the light beam directed upward along the vertical axis of the vent pipe. The vent pipe shall be insulated with at least 2 in. (51 mm) of high-temperature mineral composition material, from the vent end of the chamber to the photometer location. The photoelectric cell of which the output is directly proportional to the amount of light received shall be mounted over the light source and connected to a recording device having a minimum operating chart width of 5 in. (127 mm) with an accuracy within $\pm 1\%$ of full scale, for indicating changes in the attenuation of incident light by the passing smoke, particulate, and other effluent. The distance between the light source lens and the photocell lens shall be 36 ± 4 in. (914 ± 102 mm). The cylindrical light beam shall pass through 3-in. (76-mm) diameter openings at the top and bottom of the 16-in. diameter duct, with the resultant light beam centered on the photocell.

5.1.7.2 Linearity of the photometer system shall be verified periodically by interrupting the light beam with calibrated neutral density filters. The filters shall cover the full range of the recording instrument. Transmittance values measured by the photometer, using neutral density filters, shall be within $\pm 3\%$ of the calibrated value for each filter.

5.1.8 Draft Regulating Device:

5.1.8.1 An automatically controlled damper to regulate the draft pressure shall be installed in the vent pipe downstream of the smoke-indicating attachment. The damper

shall be provided with a manual override.

5.1.8.2 Other manual or automatic draft regulation devices, or both, are allowed to be incorporated to help maintain fan characterization and air-flow control throughout test periods.

5.1.9 Thermocouples:

5.1.9.1 A No. 18 Awg (1.02-mm) thermocouple, with $\frac{3}{8} \pm \frac{1}{8}$ in. (9.5 ± 3.2 mm) of the junction exposed in the air, shall be inserted through the floor of the test chamber so that the tip is $1 \pm \frac{1}{32}$ in. (25.4 ± 0.8 mm) below the top surface of the gasketing tape and $23 \pm \frac{1}{2}$ in. (7.0 ± 13 mm) from the centerline of the burner ports at the center of its width.

5.1.9.2 A No. 18 Awg (1.02-mm) thermocouple embedded $\frac{1}{8}$ in. (3.2 mm) below the floor surface of the test chamber shall be mounted in refractory or portland cement, carefully dried to avoid cracking, at distances of $13 \pm \frac{1}{2}$ in. (3.96 ± 13 mm) and $23 \frac{1}{4} \pm \frac{1}{2}$ in. (7.09 ± 13 mm) from the centerline of the burner ports.

5.1.9.3 The room in which the test chamber is located shall have provision for a free inflow of air during the test to maintain the room at atmospheric pressure during the entire test run.

6. Test Specimens

6.1 The test specimen shall be at least 2 in. (51 mm) wider (nominally $20 \frac{1}{4} \pm \frac{3}{4}$ in. (514 ± 19 mm)) than the interior width of the tunnel. The length of the specimen shall be a total of $24 \pm \frac{1}{2}$ in. (7.32 ± 13 mm) and shall be butted against the vent end of the fire test chamber. The specimen consists of a continuous, unbroken length, or of sections joined end-to-end. Specimens shall be truly representative of the materials for which test results are desired. Properties adequate for identification of the materials or ingredients, or both, of which the test specimen is made shall be recorded.

6.2 The upstream end of the fire test chamber shall be filled with a $14 \pm \frac{1}{8}$ -in. (356 ± 3 mm) length of uncoated 16-gauge (0.053 to 0.060 in.) steel sheet placed on the specimen mounting ledge in front of and under the leading edge of the specimen.

6.3 The test specimen shall be conditioned to a constant weight at a temperature of $73.4 \pm 5^\circ\text{F}$ ($23 \pm 2.8^\circ\text{C}$) and at a relative humidity of $50 \pm 5\%$.

7. Calibration

7.1 Place a $\frac{1}{4}$ -in. (6.3-mm) inorganic reinforced cement board on the ledge of the furnace chamber, then place the removable lid of the test chamber in position.

7.2 With the $\frac{1}{4}$ -in. (6.3-mm) inorganic reinforced cement board in position on top of the ledge of the furnace chamber and with the removable lid in place, establish a draft to produce a 0.15-in. (3.8-mm) water-column reading on the draft manometer, with the fire-end shutter open $3 \pm \frac{1}{16}$ in. (76 ± 1.6 mm), by manually setting the damper as a characterization of fan performance. Then close and seal the fire-end shutter, without changing the damper position. The manometer reading shall increase to at least 0.375 in. (9.53 mm), indicating that no excessive air leakage exists.

7.2.1 In addition, conduct a supplemental leakage test periodically with the tunnel sealed from the inlet end to beyond the photometer system, by placing a smoke bomb in the chamber. Ignite the bomb and pressurize the chamber to

¹³ The sole source of supply of the apparatus known to the committee at this time is 12-V sealed beam, clear lens, auto spot lamp, No. 4405, from General Electric, Nela Park, OH. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

¹⁴ The sole source of supply of the apparatus known to the committee at this time is No. 856BB from Weston Instruments, Wauconda, IL. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

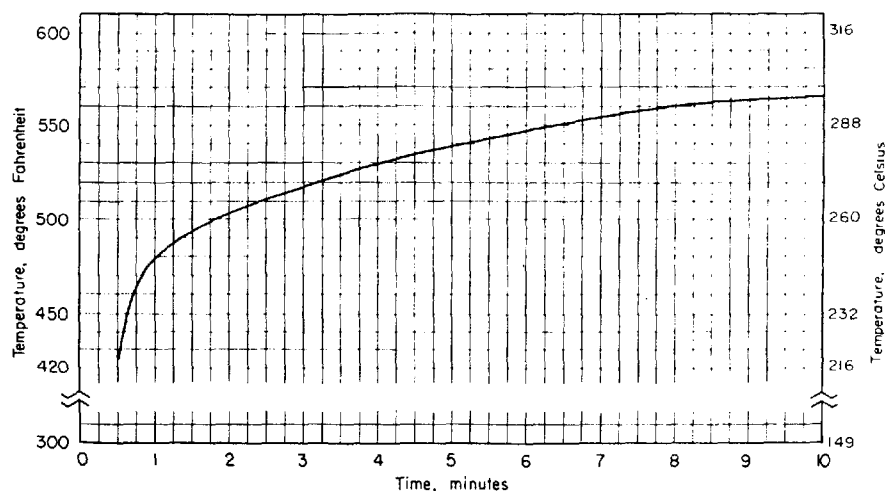


FIG. 3 Representative Time-Temperature Curve for Preheat Temperature

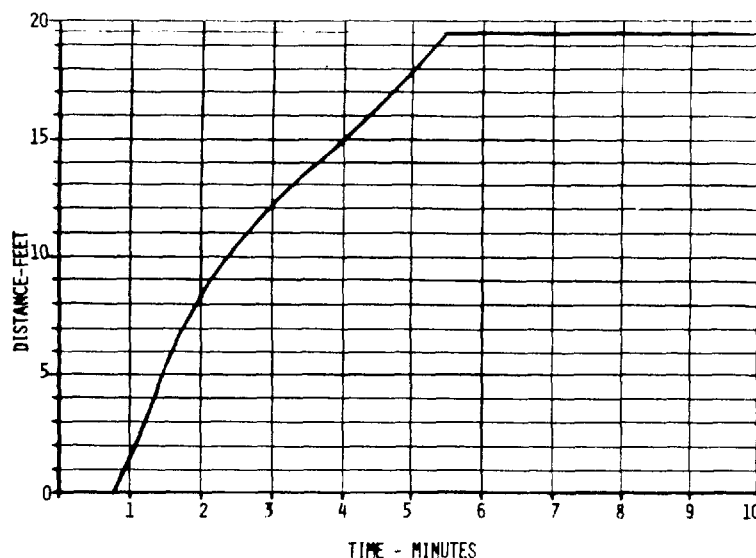


FIG. 4 Representative Time-Distance Curve for Flame Spread of Red Oak

0.375 ± 0.125 in. (9.53 ± 3.18 mm) water column. Seal all points of leakage observed in the form of escaping smoke particles.

7.3 Establish a draft reading within the range 0.055 to 0.100 in. (1.40 to 2.54 mm) water column. The required draft gage reading will be maintained throughout the test by the automatically controlled damper. Record the air velocity at seven points, 23 ft from the centerline of the burner ports, 6 ± ¼ in. (168 ± 7 mm) below the plane of the specimen mounting ledge. Determine these seven points by dividing the width of the tunnel into seven equal sections and recording the velocity at the geometrical center of each section. During the measurement of velocity, remove the turbulence bricks (see 4.3) and the exposed 23-ft thermocouple and place 24-in. (670-mm) long straightening vanes between 16 and 18 ft (4.88 and 5.49 m) from the burner. The straightening vanes shall divide the furnace cross section into nine uniform sections. Determine the velocity with furnace air temperature at 73.4 ± 5°F (23 ± 2.8°C), using a velocity transducer. The velocity, determined as the arithmetic av-

erage of the seven readings, shall be 240 ± 5 ft (73.2 ± 1.5 m)/min.

7.3.1 The following alternative to the velocity transducer equipment and method of determining the tunnel air velocity has been found suitable: A 4 in. diameter rotary vane anemometer¹⁵ is attached to the steel stand and placed in the tunnel 22.5 ft downstream of the burners. Three trials shall be conducted and their values averaged. The average is rounded to the nearest unit. The centerline of the vane anemometer shall be aligned with the vertical centerline of the tunnel by placing it on the steel stand. Trial 1 is run with the vane edge 1 in. from the non-window wall; Trial 2 is with the center axis at the tunnel center point; and Trial 3 is run with the vane edge 1 in. from the window wall.

¹⁵ The sole source of supply of the apparatus known to the committee at this time is Davis Instruments model A-4, B.B., Davis Instruments, Baltimore, MD. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.