

Specification for radio disturbance and immunity measuring apparatus and methods

Part 2-3: Methods of measurement of disturbances and immunity — Radiated disturbance measurements

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National foreword

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**Specification for radio disturbance
and immunity measuring apparatus and methods
Part 2-3: Methods of measurement of disturbances and immunity -
Radiated disturbance measurements
(CISPR 16-2-3:2006)**

Spécifications des méthodes
et des appareils de mesure
des perturbations radioélectriques
et de l'immunité aux perturbations
radioélectriques
Partie 2-3: Méthodes de mesure
des perturbations et de l'immunité -
Mesures des perturbations rayonnées
(CISPR 16-2-3:2006)

Anforderungen an Geräte
und Einrichtungen sowie Festlegung
der Verfahren zur Messung
der hochfrequenten Störaussendung
(Funkstörungen) und Störfestigkeit
Teil 2-3: Verfahren zur Messung
der hochfrequenten Störaussendung
(Funkstörungen) und Störfestigkeit -
Messung der gestrahlten Störaussendung
(CISPR 16-2-3:2006)

This European Standard was approved by CENELEC on 2006-11-01. CENELEC members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this European Standard the status of a national standard without any alteration.

Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the Central Secretariat or to any CENELEC member.

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CENELEC

European Committee for Electrotechnical Standardization
Comité Européen de Normalisation Electrotechnique
Europäisches Komitee für Elektrotechnische Normung

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Foreword

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Endorsement notice

The text of the International Standard CISPR 16-2-3:2006 was approved by CENELEC as a European Standard without any modification.

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SPECIFICATION FOR RADIO DISTURBANCE AND IMMUNITY MEASURING APPARATUS AND METHODS –

Part 2-3: Methods of measurement of disturbances and immunity – Radiated disturbance measurements

1 Scope

This part of CISPR 16 is designated a basic standard, which specifies the methods of measurement of radiated disturbance phenomena in the frequency range 9 kHz to 18 GHz.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

CISPR 13:2001, *Sound and television broadcast receivers and associated equipment – Radio disturbance characteristics – Limits and methods of measurement*

CISPR 14-1:2005, *Electromagnetic compatibility – Requirements for household appliances, electric tools and similar apparatus – Part 1: Emission*

CISPR 16-1-1:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-1: Radio disturbance and immunity measuring apparatus – Measuring apparatus*

CISPR 16-1-2:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-2: Radio disturbance and immunity measuring apparatus – Ancillary equipment – Conducted disturbances*

CISPR 16-1-4:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-4: Radio disturbance and immunity measuring apparatus – Ancillary equipment – Radiated disturbances*

CISPR 16-1-5:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-5: Radio disturbance and immunity measuring apparatus – Antenna calibration and site validation*

CISPR 16-2-1:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 2-1: Methods of measurement of disturbances and immunity – Conducted disturbance measurements*

CISPR 16-2-2:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 2-2: Methods of measurement of disturbances and immunity – Measurement of disturbance power*

CISPR 16-2-4:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 2-4: Methods of measurement of disturbances and immunity – Immunity measurements*

CISPR 16-3:2003, *Specification for radio disturbance and Immunity measuring apparatus and methods – Part 3: CISPR technical reports*
Amendment 1 (2005)

CISPR 16-4-1:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 4-1: Uncertainties, statistics and limit modelling – Uncertainties in standardized EMC tests*

CISPR 16-4-2:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 4-2: Uncertainties, statistics and limit modelling – Uncertainty in EMC measurements*

CISPR 16-4-3:2003, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 4-3: Uncertainties, statistics and limit modelling – Statistical considerations in the determination of EMC compliance of mass-produced products*

IEC 61000-4-3, *Electromagnetic compatibility (EMC) – Part 4-3: Testing and measurement techniques – Radiated, radio-frequency, electromagnetic field immunity test*

3 Terms and definitions

For the purpose of this part of CISPR 16, the definitions of IEC 60050(161) apply, as well as the following:

3.1

associated equipment

- 1) transducers (e.g. probes, networks and antennas) connected to a measuring receiver or test generator
- 2) transducers (e.g. probes, networks, antennas) which are used in the signal or disturbance transfer between an EUT and measuring equipment or a (test-) signal generator

3.2

EUT

the equipment (devices, appliances and systems) subjected to EMC (emission) compliance tests

3.3**product publication**

publication specifying EMC requirements for a product or product family, taking into account specific aspects of such a product or product family

3.4**emission limit (from a disturbing source)**

the specified maximum emission level of a source of electromagnetic disturbance

[IEV 161-03-12]

3.5**ground reference**

a connection that constitutes a defined parasitic capacitance to the surrounding of an EUT and serves as reference potential

NOTE See also IEV 161-04-36.

3.6**(electromagnetic) emission**

the phenomenon by which electromagnetic energy emanates from a source

[IEV 161-01-08]

3.7**coaxial cable**

a cable containing one or more coaxial lines, typically used for a matched connection of associated equipment to the measuring equipment or (test-)signal generator providing a specified characteristic impedance and a specified maximum allowable cable transfer impedance

3.8**measuring receiver**

a receiver for the measurement of disturbances with different detectors

NOTE The receiver is specified according to CISPR 16-1-1.

3.9**test configuration**

gives the specified measurement arrangement of the EUT in which an emission level is measured

NOTE The emission level is measured as required by IEV 161-03-11, IEV 161-03-12, IEV 161-03-14 and IEV 161-03-15, definitions of emission level.

3.10**weighting (quasi-peak detection)**

the repetition-rate dependent conversion of the peak-detected pulse voltages to an indication corresponding to the psychophysical annoyance of pulsive disturbances (acoustically or visually) according to the weighting characteristics, or alternatively gives the specified manner in which an emission level or an immunity level is evaluated

NOTE 1 The weighting characteristics are specified in CISPR 16-1-1.

NOTE 2 The emission level or immunity level is evaluated as required by IEC 60050(161) definitions of level (see IEV 161-03-01, IEV 161-03-11 and IEV 161-03-14).

3.11

continuous disturbance

RF disturbance with a duration of more than 200 ms at the IF-output of a measuring receiver, which causes a deflection on the meter of a measuring receiver in quasi-peak detection mode which does not decrease immediately

[IEV 161-02-11, modified]

NOTE The measuring receiver is specified in CISPR 16-1-1.

3.12

discontinuous disturbance

for counted clicks, disturbance with a duration of less than 200 ms at the IF-output of a measuring receiver, which causes a transient deflection on the meter of a measuring receiver in quasi-peak detection mode

NOTE 1 For impulsive disturbance, see IEV 161-02-08.

NOTE 2 The measuring receiver is specified in CISPR 16-1-1.

3.13

measurement time

T_m

the effective, coherent time for a measurement result at a single frequency (in some areas also called dwell time)

- for the peak detector, the effective time to detect the maximum of the signal envelope,
- for the quasi-peak detector, the effective time to measure the maximum of the weighted envelope
- for the average detector, the effective time to average the signal envelope
- for the r.m.s. detector, the effective time to determine the r.m.s. of the signal envelope

3.14

sweep

a continuous frequency variation over a given frequency span

3.15

scan

a continuous or stepped frequency variation over a given frequency span

3.16

sweep or scan time

T_s

the time between start and stop frequencies of a sweep or scan

3.17

span

Δf

difference between stop and start frequencies of a sweep or scan

3.18

sweep or scan rate

the frequency span divided by the sweep or scan time

3.19**number of sweeps per time unit (e.g. per second)**

$$\frac{n_s}{1/(\text{sweep time} + \text{retrace time})}$$

3.20**observation time** T_o

the sum of measurement times T_m on a certain frequency in case of multiple sweeps. If n is the number of sweeps or scans, then $T_o = n \times T_m$

3.21**total observation time** T_{tot}

the effective time for an overview of the spectrum (either single or multiple sweeps). If c is the number of channels within a scan or sweep, then $T_{tot} = c \times n \times T_m$

4 Types of disturbance to be measured

This clause describes the classification of different types of disturbance and the detectors appropriate for their measurement.

4.1 Types of disturbance

For physical and psychophysical reasons, dependent on the spectral distribution, measuring receiver bandwidth, the duration, rate of occurrence, and degree of annoyance during the assessment and measurement of radio disturbance, distinction is made between the following types of disturbance:

- a) *narrowband continuous disturbance*, i.e. disturbance on discrete frequencies as, for example, the fundamentals and harmonics generated with the intentional application of RF energy with ISM equipment, constituting a frequency spectrum consisting only of individual spectral lines whose separation is greater than the bandwidth of the measuring receiver so that during the measurement only one line falls into the bandwidth in contrast to b);
- b) *broadband continuous disturbance*, which normally is unintentionally produced by the repeated impulses of, for example, commutator motors, and which have a repetition frequency which is lower than the bandwidth of the measuring receiver so that during the measurement more than one spectral line falls into the bandwidth; and
- c) *broadband discontinuous disturbance* is also generated unintentionally by mechanical or electronic switching procedures, for example by thermostats or programme controls with a repetition rate lower than 1 Hz (click-rate less than 30/min).

The frequency spectra of b) and c) are characterized by having a continuous spectrum in the case of individual (single) impulses and a discontinuous spectrum in case of repeated impulses, both spectra being characterized by having a frequency range which is wider than the bandwidth of the measuring receiver specified in CISPR 16-1-1.

4.2 Detector functions

Depending on the types of disturbance, measurements may be carried out using a measuring receiver with:

- a) an average detector generally used in the measurement of narrowband disturbance and signals, and particularly to discriminate between narrowband and broadband disturbance;
- b) a quasi-peak detector provided for the weighted measurement of broadband disturbance for the assessment of audio annoyance to a radio listener, but also usable for narrowband disturbance;
- c) a peak detector which may be used for either broadband or narrowband disturbance measurement.

Measuring receivers incorporating these detectors are specified in CISPR 16-1-1.

5 Connection of measuring equipment

This subclause describes the connection of measuring equipment, measuring receivers and associated equipment such as artificial networks, voltage and current probes, absorbing clamps and antennas.

5.1 Connection of associated equipment

The connecting cable between the measuring receiver and the associated equipment shall be shielded and its characteristic impedance shall be matched to the input impedance of the measuring receiver.

The output of the associated equipment shall be terminated with the prescribed impedance.

5.2 Connections to RF reference ground

The artificial mains network (AMN) shall be connected to the reference ground by a low RF impedance, e.g. by direct bonding of the case of the AMN to the reference ground or reference wall of a shielded room, or with a low impedance conductor as short and as wide as practical (maximum length to width ratio is 3:1).

Terminal voltage measurements shall be referenced only to the reference ground. Ground loops (common impedance coupling) shall be avoided. This should also be observed for measuring apparatus (e.g. measuring receivers and connected associated equipment, such as oscilloscopes, analyzers, recorders, etc.) fitted with a protective earth conductor (PE) of Protection Class I equipment. If the PE connection of the measuring apparatus and the PE connection of the power mains to the reference ground do not have RF isolation from the reference ground, the necessary RF isolation shall be provided by means such as RF chokes and isolation transformers, or if applicable, by powering the measuring apparatus from batteries, so that the RF connection of the measuring apparatus to the reference ground is made via only one route.

For the treatment of PE connection of the EUT to the reference ground, see Clause A.4 of CISPR 16-2-1:2003.

Stationary test configurations do not require a connection with the protective earth conductor if the reference ground is connected directly and meets the safety requirements for protective earth conductors (PE connections).

5.3 Connection between the EUT and the artificial mains network

General guidelines for the selection of grounded and non-grounded connections of the EUT to the AMN are discussed in Annex A of CISPR 16-2-1.

6 General measurement requirements and conditions

Radio disturbance measurements shall be:

- a) reproducible, i.e. independent of the measurement location and environmental conditions, especially ambient noise;
- b) free from interactions, i.e. the connection of the EUT to the measuring equipment shall neither influence the function of the EUT nor the accuracy of the measurement equipment.

These requirements may be met by observing the following conditions:

- c) existence of a sufficient signal-to-noise ratio at the desired measurement level, e.g. the level of the relevant disturbance limit;
- d) having a defined measuring set-up, termination and operating conditions of the EUT;
- e) having a sufficiently high impedance of the probe at the measuring point, in the case of voltage probe measurements;
- f) when using a spectrum analyzer or scanning receiver due considerations shall be given to its particular operating and calibration requirements.

6.1 Disturbance not produced by the equipment under test

The measurement signal-to-noise ratio with respect to ambient noise shall meet the following requirements. Should the spurious noise level exceed the required level, it shall be recorded in the test report.

6.1.1 Compliance testing

A test site shall permit emissions from the EUT to be distinguished from ambient noise. The ambient noise level should preferably be 20 dB, but at least be 6 dB below the desired measurement level. For the 6 dB condition, the apparent disturbance level from the EUT is increased by up to 3,5 dB. The suitability of the site for required ambient level may be determined by measuring the ambient noise level with the test unit in place but not operating.

In the case of compliance measurement according to a limit, the ambient noise level is permitted to exceed the preferred –6 dB level provided that the level of both ambient noise and source emanation combined does not exceed the specified limit. The EUT is then considered to meet the limit. Other actions can also be taken; for example, reduce the bandwidth for narrowband signals and/or move the antenna closer to the EUT.

NOTE If both the ambient field strength and field strength of ambient and EUT are measured separately, it may be possible to provide an estimate of the EUT field strength to a quantifiable level of uncertainty. Reference is made in this respect in Annex C of CISPR 11.

6.2 Measurement of continuous disturbance

6.2.1 Narrowband continuous disturbance

The measuring set shall be kept tuned to the discrete frequency under investigation and returned if the frequency fluctuates.

6.2.2 Broadband continuous disturbance

For the assessment of broadband continuous disturbance the level of which is not steady, the maximum reproducible measurement value shall be found. See 6.4.1 for further details.

6.2.3 Use of spectrum analyzers and scanning receivers

Spectrum analyzers and scanning receivers are useful for disturbance measurements, particularly in order to reduce measuring time. However, special consideration must be given to certain characteristics of these instruments, which include: overload, linearity, selectivity, normal response to pulses, frequency scan rate, signal interception, sensitivity, amplitude accuracy and peak, average and quasi-peak detection. These characteristics are considered in Annex B.

6.3 Operating conditions of the EUT

The EUT shall be operated under the following conditions:

6.3.1 Normal load conditions

The normal load conditions shall be as defined in the product specification relevant to the EUT, and for EUTs not so covered, as indicated in the manufacturer's instructions.

6.3.2 The time of operation

The time of operation shall be, in the case of EUTs with a given rated operating time, in accordance with the marking; in all other cases, the time is not restricted.

6.3.3 Running-in time

No specific running-in time, prior to testing, is given, but the EUT shall be operated for a sufficient period to ensure that the modes and conditions of operation are typical of those during the life of the equipment. For some EUTs, special test conditions may be prescribed in the relevant equipment publications.

6.3.4 Supply

The EUT shall be operated from a supply having the rated voltage of the EUT. If the level of disturbance varies considerably with the supply voltage, the measurements shall be repeated for supply voltages over the range of 0,9 to 1,1 times the rated voltage. EUTs with more than one rated voltage shall be tested at the rated voltage which causes maximum disturbance.

6.3.5 Mode of operation

The EUT shall be operated under practical conditions which cause the maximum disturbance at the measurement frequency.

6.4 Interpretation of measuring results

6.4.1 Continuous disturbance

- a) If the level of disturbance is not steady, the reading on the measuring receiver is observed for at least 15 s for each measurement; the highest readings shall be recorded, with the exception of any isolated clicks, which shall be ignored (see 4.2 of CISPR 14-1:2005).
- b) If the general level of the disturbance is not steady, but shows a continuous rise or fall of more than 2 dB in the 15 s period, then the disturbance voltage levels shall be observed for a further period and the levels shall be interpreted according to the conditions of normal use of the EUT, as follows:
 - 1) if the EUT is one which may be switched on and off frequently, or the direction of rotation of which can be reversed, then at each frequency of measurement the EUT should be switched on or reversed just before each measurement, and switched off just after each measurement. The maximum level obtained during the first minute at each frequency of measurement shall be recorded;
 - 2) if the EUT is one which in normal use runs for longer periods, then it should remain switched on for the period of the complete test, and at each frequency the level of disturbance shall be recorded only after a steady reading (subject to the provision that item a) has been obtained).
- c) If the pattern of the disturbance from the EUT changes from a steady to a random character part way through a test, then that EUT shall be tested in accordance with item b).
- d) Measurements are taken throughout the complete spectrum and are recorded at least at the frequency with maximum reading and as required by the relevant CISPR publication.

6.4.2 Discontinuous disturbance

Measurement of discontinuous disturbance may be performed at a restricted number of frequencies. For further details, see CISPR 14-1.

6.4.3 Measurement of the duration of disturbances

The EUT is connected to the relevant artificial mains network. If a measuring set is available, it is connected to the network and a cathode-ray oscilloscope is connected to the IF output of the measuring set. If a receiver is not available, the oscilloscope is connected directly to the network. The time base of the oscilloscope can be started by the disturbances to be tested; the time base is set to a value of 1 ms/div – 10 ms/div for EUT with instantaneous switching and 10 ms/div – 200 ms/div for other EUT. The duration of the disturbance can either be recorded directly by a storage oscilloscope or digital oscilloscope or by photograph or hard copy recording of the screen.

6.5 Measurement times and scan rates for continuous disturbance

Both for manual measurements and automated or semiautomated measurements, measurement times and scan rates of measuring and scanning receivers shall be set so as to measure the maximum emission. Especially, where a peak detector is used for prescans, the measurement times and scan rates have to take the timing of the emission under test into account. More detailed guidance on the execution of automated measurements can be found in Clause 8.

6.5.1 Minimum measurement times

Clause B.7 of the present standard provides a table of the minimum sweep times or the fastest – practically achievable – scan rates. From this table the following minimum scan times for measurements over a complete CISPR band have been derived:

Table 1 – Minimum scan times for the three CISPR bands with peak and quasi-peak detectors

Frequency band		Scan time T_s for peak detection	Scan time T_s for quasi-peak detection
A	9 kHz – 150 kHz	14,1 s	2820 s = 47 min
B	0,15 MHz – 30 MHz	2,985 s	5 970 s = 99,5 min = 1 h 39 min
C/D	30 MHz – 1 000 MHz	0,97 s	19 400 s = 323,3 min = 5 h 23 min

The scan times in Table 1 apply to the measurement of CW signals. Depending on the type of disturbance, the scan time may have to be increased – even for quasi-peak measurements. In extreme cases, the measurement time T_m at a certain frequency may have to be increased to 15 s, if the level of the observed emission is not steady (see 6.4.1). However isolated clicks are excluded.

Scan rates and measurement times for use with the average detector will be found in Annex D.

Most product standards call out quasi-peak detection for compliance measurements which is very time consuming, if no time-saving procedures are applied (see Clause 8). Before time-saving procedures can be applied, the emission has to be detected in a prescan. In order to ensure that e.g. intermittent signals are not missed during an automatic scan, the considerations in 6.5.2 to 6.5.4 need to be taken into account.

6.5.2 Scan rates for scanning receivers and spectrum analyzers

One of two conditions need to be met to ensure that signals are not missed during automatic scans over frequency spans:

- 1) for a single sweep: the measurement time at each frequency must be larger than the intervals between pulses for intermittent signals;
- 2) for multiple sweeps with maximum hold: the observation time at each frequency should be sufficient for intercepting intermittent signals.

The frequency scan rate is limited by the instrument's resolution bandwidth and the video bandwidth setting. If the scan rate is chosen too fast for the given instrument state, erroneous measurement results will be obtained. Therefore, a sufficiently long sweep time needs to be chosen for the selected frequency span. Intermittent signals may be intercepted by either a single sweep with sufficient observation time at each frequency or by multiple sweeps with maximum hold. Usually for an overview over unknown emissions, the latter will be highly efficient: as long as the spectrum display changes, there may still be intermittent signals to discover. The observation time has to be selected according to the periodicity at which interfering signals occur. In some cases, the sweep time may have to be varied in order to avoid synchronization effects.

When determining the minimum sweep time for measurements with a spectrum analyzer or scanning EMI receiver, based on a given instrument setting and using peak detection, two different cases have to be distinguished. If the video bandwidth is selected to be **wider** than the resolution bandwidth, the following expression can be used to calculate the minimum sweep time:

$$T_{s \min} = (k \times \Delta f) / (B_{\text{res}})^2 \quad (1)$$

where

$T_{s \min}$ = Minimum sweep time

Δf = Frequency span

B_{res} = Resolution bandwidth

k = Constant of proportionality, related to the shape of the resolution filter; this constant assumes a value between 2 and 3 for synchronously-tuned, near-Gaussian filters. For nearly rectangular, stagger-tuned filters, k has a value between 10 and 15.

If the video bandwidth is selected to be equal to or smaller than the resolution bandwidth, the following expression can be used to calculate the minimum sweep time:

$$T_{s \min} = (k \times \Delta f) / (B_{\text{res}} \times B_{\text{video}}) \quad (2)$$

where B_{video} = video bandwidth

Most spectrum analyzers and scanning EMI receivers automatically couple the sweep time to the selected frequency span and the bandwidth settings. Sweep time is adjusted to maintain a calibrated display. The automatic sweep time selection can be overridden if longer observation times are required, e.g., to intercept slowly varying signals.

In addition, for repetitive sweeps, the number of sweeps per second will be determined by the sweep time $T_{s \min}$ and the retrace time (time needed to retune the local oscillator and to store the measurement results, etc.).

6.5.3 Scan times for stepping receivers

Stepping EMI receivers are consecutively tuned to single frequencies using predefined step sizes. While covering the frequency range of interest in discrete frequency steps, a minimum dwell time at each frequency is required for the instrument to accurately measure the input signal.

For the actual measurement, a frequency step size of roughly 50 % of the resolution bandwidth used or less (depending on the resolution filter shape) is required to reduce measurement uncertainty for narrowband signals due to the stepwidth. Under these assumptions the scan time $T_{s \min}$ for a stepping receiver can be calculated using the following equation:

$$T_{s \min} = T_{m \min} \times \Delta f / (B_{\text{res}} \times 0,5) \quad (3)$$

where $T_{m \min}$ = minimum measurement (dwell) time at each frequency

In addition to the measurement time, some time has to be taken into consideration for the synthesizer to switch to the next frequency and for the firmware to store the measurement result, which in most measuring receivers is automatically done so that the selected measurement time is the effective time for the measurement result. Furthermore, the selected detector, e.g. peak or quasi-peak, determines this time period as well.

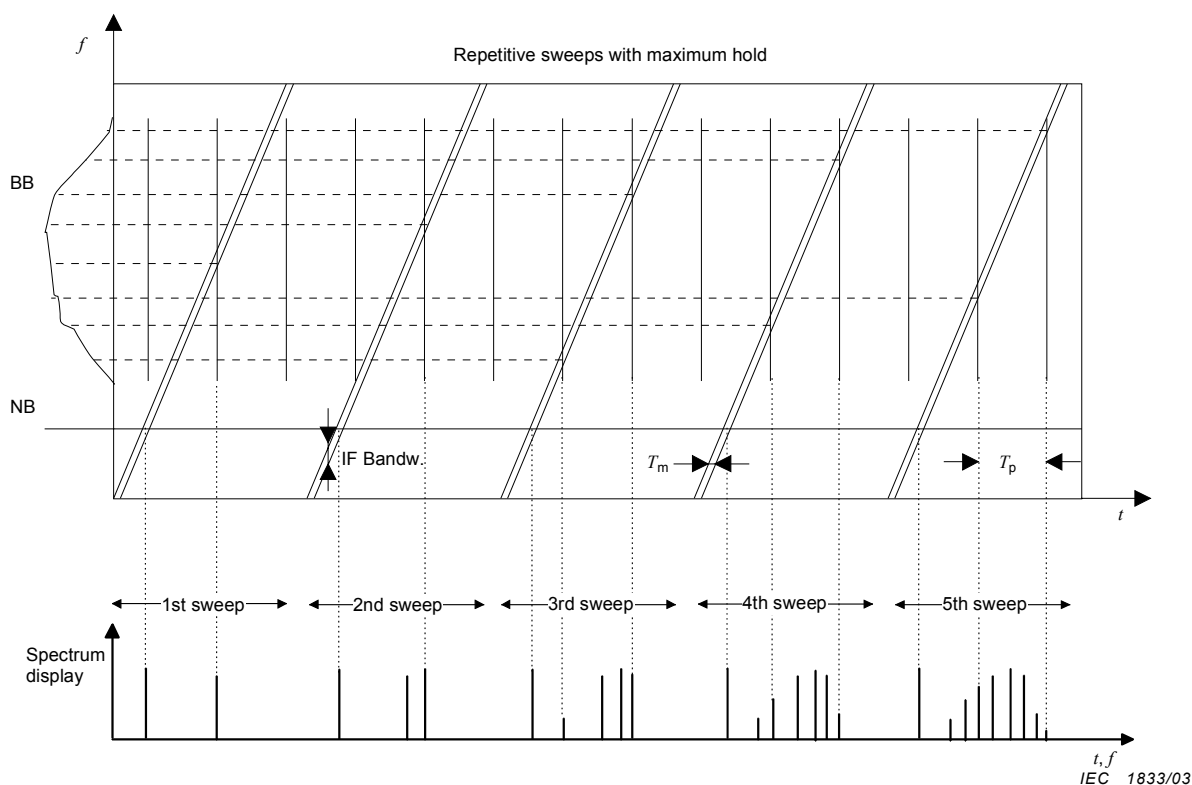
For purely broadband emissions, the frequency step size may be increased. In this case the objective is to find the maxima of the emission spectrum only.

6.5.4 Strategies for obtaining a spectrum overview using the peak detector

For each prescan measurement, the probability of intercepting all critical spectral components of the EUT spectrum shall be equal to 100 % or as close to 100 % as possible. Depending on the type of measuring receiver and the characteristics of the disturbance, which may contain narrowband and broadband components, two general approaches are proposed:

- stepped scan: the measurement (dwell) time shall be long enough at each frequency to measure the signal peak, e.g. for an impulsive signal the measurement (dwell) time should be longer than the reciprocal of the repetition frequency of the signal.
- swept scan: the measurement time must be larger than the intervals between intermittent signals (single sweep) and the number of frequency scans during the observation time should be maximized to increase the probability of signal interception.

Figures 1, 2 and 3 show examples of the relationship between various time-varying emission spectra and the corresponding display on a measuring receiver. In each case the upper part of the figure shows the position of the receiver bandwidth as it either sweeps or steps through the spectrum.

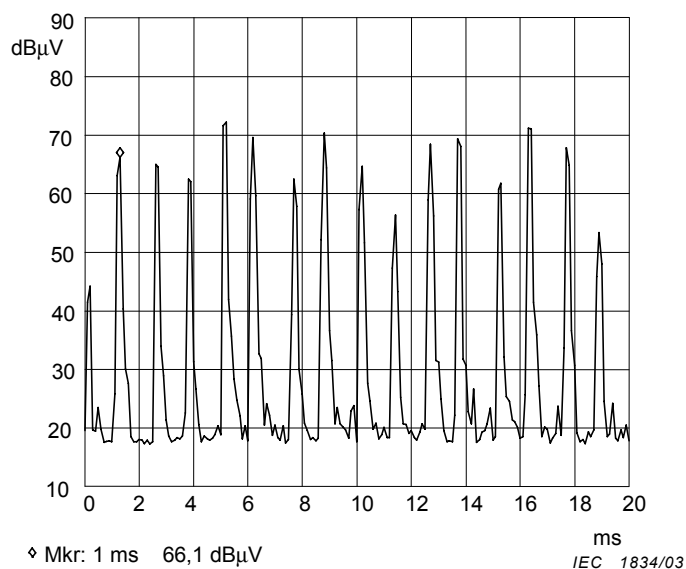


T_p is the pulse-repetition interval of the impulsive signal. A pulse occurs at each vertical line of the spectrum-vs.-time display (upper part of the figure).

Figure 1 – Measurement of a combination of a CW signal (“NB”) and an impulsive signal (“BB”) using multiple sweeps with maximum hold

If the type of emission is unknown, multiple sweeps with the shortest possible sweep time and peak detection allow to determine the spectrum envelope. A short single sweep is sufficient to measure the continuous narrowband signal content of the EUT spectrum. For continuous broadband and intermittent narrowband signals, multiple sweeps at various scan rates using a “maximum hold” function may be necessary to determine the spectrum envelope. For low repetition impulsive signals, many sweeps will be necessary to fill up the spectrum envelope of the broadband component.

The reduction of measurement time requires a timing analysis of the signals to be measured. This can be done either with a measuring receiver which provides a graphical signal display, used in zero-span mode or using an oscilloscope connected to the receiver's IF or video output as e.g. shown in Figure 2.



Disturbance from a DC collector motor: due to the number of collector segments the pulse repetition frequency is high (approx. 800 Hz) and the pulse amplitude varies strongly. Therefore for this example, the recommended measurement (dwell) time with the peak detector is > 10 ms.

Figure 2 – Example of a timing analysis

This way pulse durations and pulse repetition frequencies can be determined and scan rates or dwell times selected accordingly:

- for **continuous unmodulated narrowband** disturbances the fastest scan time possible for the selected instrument settings may be used;
- for **pure continuous broadband** disturbances, e.g. from ignition motors, arc welding equipment, and collector motors, a stepped scan (with peak or even quasi-peak detection) for sampling of the emission spectrum may be used. In this case the knowledge of the type of disturbance is used to draw a polyline curve as the spectrum envelope (see Figure 3). The step size has to be chosen so that no significant variations in the spectrum envelope are missed. A single swept measurement – if performed slowly enough – will also yield the spectrum envelope;
- for **intermittent narrowband** disturbances with unknown frequencies either fast short sweeps involving a “maximum hold” function (see Figure 4) or a slow single sweep may be used. A timing analysis may be required prior to the actual measurement to ensure proper signal interception.

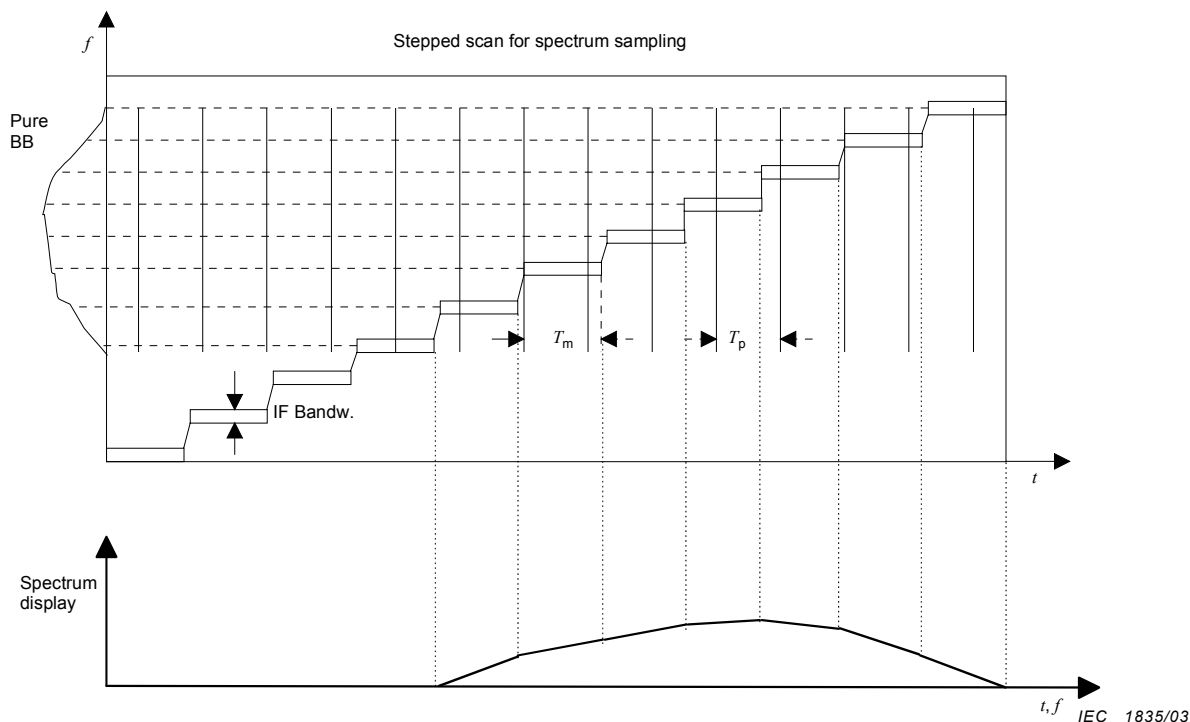
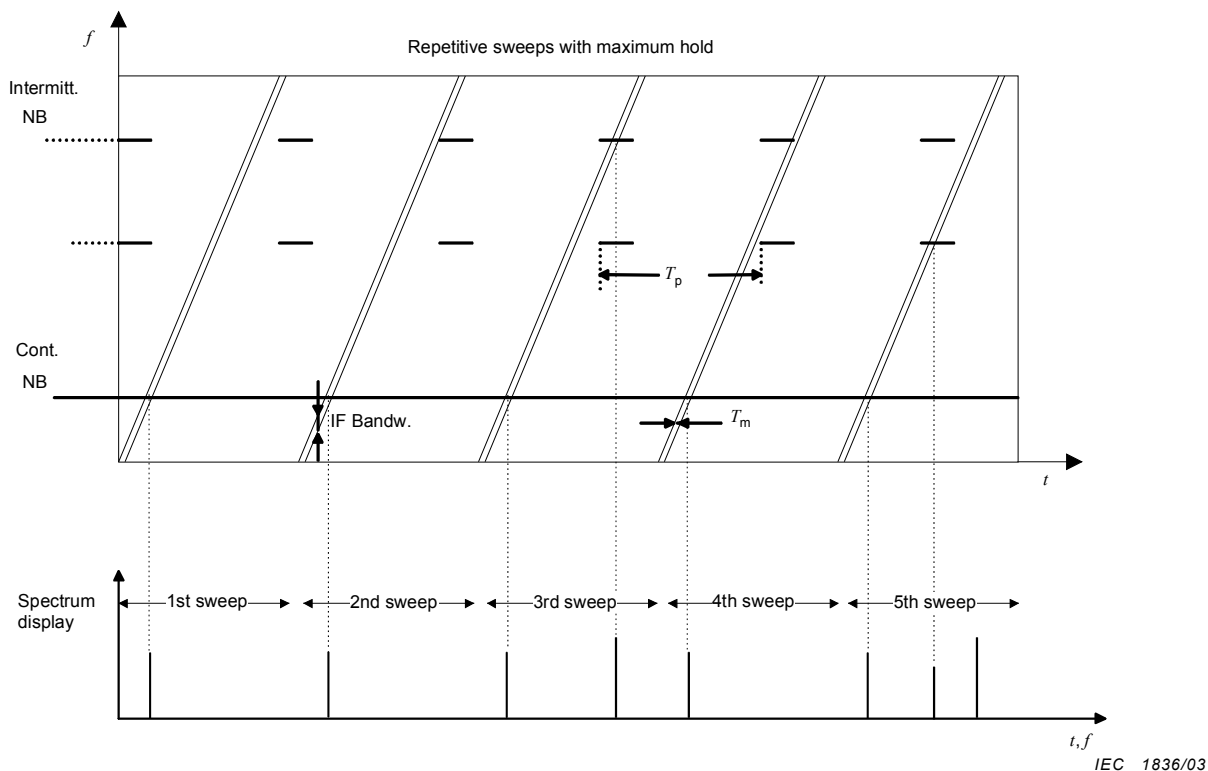


Figure 3 – A broadband spectrum measured with a stepped receiver

The measurement (dwell) time T_m should be longer than the pulse repetition interval T_p , which is the inverse of the pulse repetition frequency.



NOTE In the example above, 5 sweeps are required until all spectral components are intercepted. The number of sweeps required or the sweep time may have to be increased, depending on pulse duration and pulse repetition interval.

Figure 4 – Intermittent narrowband disturbances measured using fast short repetitive sweeps with maximum hold function to obtain an overview of the emission spectrum

Intermittent broadband disturbances have to be measured with discontinuous disturbance analysis procedures, as described in CISPR 16-1-1.

7 Measurement of radiated disturbances

7.1 Introduction

This section sets forth the general procedures for the measurement of the field strength of radio disturbance produced by devices and systems. Experience with radiated disturbance measurements is less extensive than that of voltage measurements. The radiated disturbance measurement procedures are therefore open to revision and extension as knowledge and experience are accumulated. In particular, attention shall be given to the effect of leads and cables associated with the EUT.

For some products, it may be required to measure the electric, the magnetic, or both components of the radiated disturbance. Sometimes a measurement of a quantity related to radiated power is more appropriate. Normally measurements should be made of both the horizontal and vertical components of the disturbance with respect to the reference ground plane. The results of measurements of either the electric or magnetic components may be expressed in peak, quasi-peak, average or r.m.s. values.

The magnetic component of the disturbance is normally measured at frequencies up to 30 MHz. In magnetic field measurements only the horizontal component of the field at the position of the receiving antenna is measured when using the distant antenna procedure. If the large loop antenna (LLA) system is used, the three orthogonal magnetic dipole moments of the EUT are measured. (Note that in the single antenna method, the horizontal component of the field at the position of the antenna is determined by the horizontal and vertical dipole moments of the EUT because reflection plays a part.)

7.2 Field-strength measurements in the frequency range 9 kHz to 1 GHz

Field-strength measurements may be made on an open area test site, in an absorber-lined shielded enclosure, in a reverberating chamber or using a LLA system. For practical reasons other test sites may have to be specified.

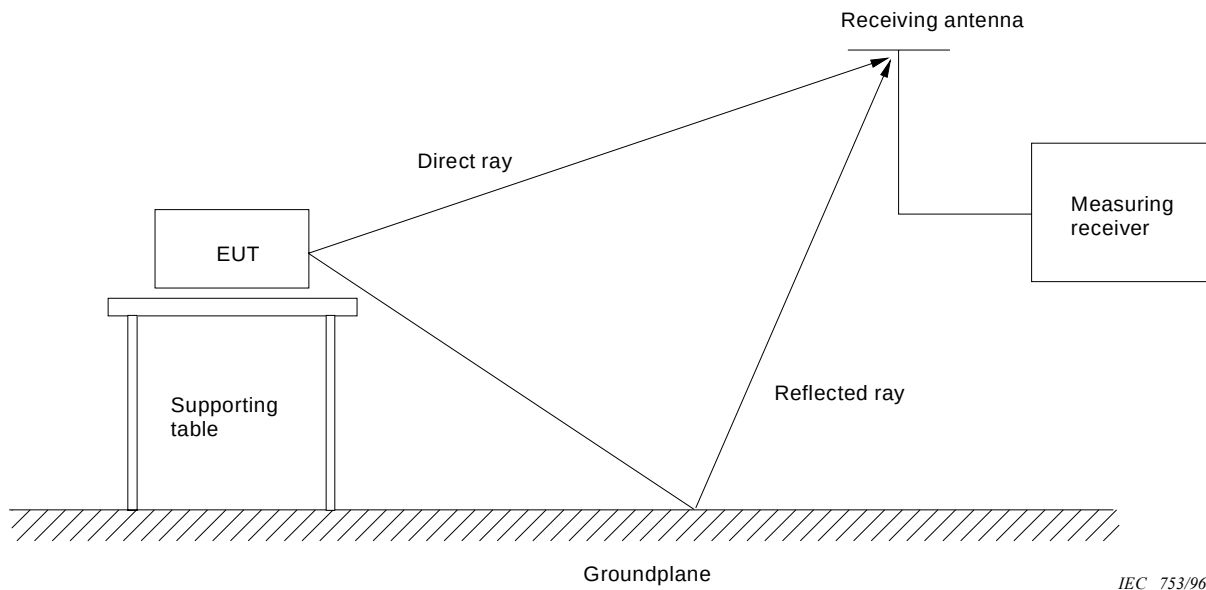
7.2.1 Open area test site measurements

The open area test site shall conform with the relevant specifications of CISPR 16-1-4 and CISPR 16-1-5 for its physical and electrical properties and for its validation.

7.2.2 General measurement method

Figure 5 shows the concept of measurements made on an open area test site with the direct and ground reflected rays arriving at the receiving antenna.

The EUT is set up at a specified height above the ground plane and configured to represent normal operating conditions. The antenna is positioned at the specified separation distance. The EUT is rotated in the horizontal plane and the maximum reading noted. The height of the antenna is adjusted so that the direct and reflected rays approach or meet in-phase addition. The procedural steps may be interchanged and may need to be repeated to find the maximum disturbance. For practical reasons the height variation is restricted and hence perfect in-phase addition may not be achieved.



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Figure 5 – Concept of electric field strength measurements made on an open area test site (OATS) with the direct and reflective rays arriving at the receiving antenna

7.2.3 Measurement distance

An EUT subject to a radiated disturbance limit at a specified distance should be measured at that distance unless to do so would be impractical because of equipment size, etc. The measurement distance is the length of the projection of the EUTs closest point to the antenna and the midpoint of the antenna onto the ground plane. In some test set-ups the distance is measured from the antenna to the radiation centre of the EUT. For a measurement distance of 10 m either method may be used. A distance of 10 m is preferred at most outdoor sites since at this distance the expected level of the disturbance being measured is sufficiently above the general ambient noise level to permit useful testing. Distances of less than 3 m or greater than 30 m are not generally used. If a measurement distance other than the specified distance is necessary, the results should be extrapolated using the procedures specified in the product standards.. If no guidance is given, suitable justification for extrapolation shall be provided. In general, extrapolation does not follow a simple inverse distance law.

Where possible, measurement should be made in the far field. The far field region may be defined by the following conditions.

Measurement distance d is selected so that:

- $d \geq \lambda/6$. At this distance $E/H = Z_0 = 120 \pi = 377 \Omega$, that is electrical and magnetic field strength components are perpendicular to each other and the measurement error is in the order of 3 dB if the EUT is regarded as being a tuned dipole antenna; or
- $d \geq \lambda$, condition for a plane wave, where the error is in the order of 0,5 dB if the EUT is regarded as a tuned dipole antenna; or
- $d \geq 2D^2/\lambda$, where D is the largest dimension of either the EUT or the antenna determining the minimum aperture for the illumination of the EUT, which applies to cases, where $D \gg \lambda$.

7.2.4 Antenna height variation

For electric field-strength measurements the antenna height above the ground plane shall be varied within a specified range to obtain the maximum reading which will occur when the direct and reflected rays are in phase. As a general rule, for measurement distances up to and including 10 m, the antenna height for electric field strength measurements shall be varied between 1 m and 4 m. At greater distances of up to 30 m, preferably the height shall be varied between 2 m and 6 m. It may be necessary to adjust the minimum antenna height above ground down to 1 m in order to maximize the reading. These height scans apply for both horizontal and vertical polarization, except that for vertical polarization, the minimum height shall be increased so that the lowest point of the antenna clears the site ground surface by at least 25 cm. For magnetic field strength measurements using the single magnetic loop antenna, the height of the receiving antenna may be fixed at a specified elevation (typically 1 m from ground to the bottom of the loop antenna). The loop antenna and EUT shall be rotated in azimuth to maximize the measured disturbance.

7.2.5 Product specification details

In addition to specifying the detailed measurement method and the disturbance parameters to be measured, the product standards shall include other relevant details as outlined below.

7.2.5.1 Test environment

The influence of the test environment shall be considered so as to ensure correct functioning of: the EUT. Important parameters in the physical environment shall be specified!, e.g. temperature and humidity.

The electromagnetic environment needs special consideration to ensure accurate disturbance measurements. The ambient radio noise and signal levels measured at the test site with the EUT de-energized should be at least 6 dB below the limit. It is recognized that this is not always realizable at all frequencies. However, in the event that the measured levels of the ambient plus EUT radio noise emissions are not above the limit, the EUT shall be considered to be in compliance with the limit. For further guidance on ambient levels and resulting measurements error, see 6.1.1 and Annex A.

If the ambient field-strength level at frequencies within the specified measurement ranges exceeds the limit(s), the following alternatives may be used:

- a) perform measurements at a closer distance and extrapolate results to the distance at which the limit is specified. The extrapolation formula shall be as recommended by the product standard or shall be verified by measurements at no less than three different distances;
- b) perform measurements in critical frequency bands during hours when broadcast stations are off the air and the ambients from industrial equipment are lower;
- c) compare the amplitude of the EUT disturbance at the frequency under investigation with the amplitude of disturbance on adjacent frequencies in a shielded room or anechoically treated shielded room. The amplitude of the EUT disturbance at the frequency under investigation can be estimated by measuring the amplitude of the adjacent frequency disturbance and making a comparison;

NOTE The shielded or anechoic room should not be used for compliance determination at the other EUT frequencies unless the anechoic room data is correlatable to the open area test site data.

- d) in orienting the axis of an open field area test site, it is desirable to consider the directions of strong ambient signals, so that the orientation of the receiving antenna on the site discriminates against such signals as far as possible;
- e) for narrowband disturbances from the EUT occurring near an RF ambient, when both are within the standard bandwidth, a narrower instrument bandwidth may be useful.

7.2.5.2 Configuration of equipment under test

The operating conditions of the EUT shall be specified, e.g., the characteristics of the input signals, the modes of operation, the arrangement of components, the lengths and types of interconnecting cables, etc.

The testing of individual and multi-component systems shall satisfy the following two conditions:

- a) the system is configured for use in a typical manner.
- b) the system is configured in a manner that will maximize disturbances.

The term "system" refers to the EUT in combination with the components that are connected to the EUT and all required connecting cables.

The term "configuration" refers to the orientation of the EUT, the other components of the system, the interconnecting cables, and the power mains leads that comprise the system. During all measurements, the configuration of the system shall be adjusted so that the above two conditions, the condition a) being satisfied first and followed by condition b), are fulfilled, within the guidelines described in the following paragraphs.

The term "typical" is used to describe the arrangement of how the EUT will actually be used. Guidelines for setting up a typical configuration are outlined below.

For equipment designed to be part of a multi-unit system, the EUT shall be installed in a typical system and configured in accordance with the manufacturer's instructions. It shall also be operated in a manner that is representative of the typical usage for that EUT. During all tests, the EUT and all system components shall be manipulated within the confines of typical usage to maximize each disturbance.

Interface cables shall be connected to each interface port on the EUT. The effect of varying the position of each cable shall be investigated to find the configuration that maximizes each disturbance as constrained by its typical configuration in actual use. The number of manipulations may be limited if a few such cable configurations will lead to maximum disturbances over the frequency range investigated.

Interface cables shall be of the type and length specified by the equipment manufacturer.

Any excess length of each cable shall be separately bundled in a serpentine fashion at the approximate centre of the cable with the bundle 30 cm to 40 cm in length. If it is impractical to do so because of cable bulk or stiffness or because the testing is being done at a user installation, disposition of the excess cable length is left to the discretion of the test engineer and should be noted in the test report. Different requirements for excess cabling may be specified in the product standard.

Cables shall not be placed underneath, on top of the EUT or on system components unless it is appropriate to do so, e.g. a cable is normally routed through overhead cable racks or under the ground plane. Cables shall be positioned adjacent to the exterior cabinets of the EUT and all system components only if typically used in that manner. The EUT should be investigated in different modes of operation.

For an EUT normally operated on top of a table, radiated emission tests should be performed with the EUT on a non-conducting table, the top of which is of suitable size. The table should be placed on a remotely controlled rotating platform constructed with non-conducting materials. The top of the rotating platform should normally be less than 0,5 m above the ground plane and the height of the table and platform together 0,8 m above the ground plane. If the rotating platform is at the same elevation as the ground plane, its surface shall be of conducting material and the 0,8 m height shall be measured with respect to the top of the rotating platform. An EUT normally placed on the floor will be tested on the floor. A flush-mounted rotating platform is useful in this situation.

The EUT shall be grounded in accordance with the manufacturer's requirements and conditions of intended use. If the EUT is operated without a ground connection, it shall be tested ungrounded. When the EUT is furnished with a grounding terminal or internally grounded lead which is to be connected in actual installation conditions, the ground lead or connection shall be connected to a ground plane (or facility for earth ground), simulating actual installation conditions. Any internally grounded lead included in the plug end of the a.c. mains cord of the EUT shall be connected to ground through the mains power service.

7.2.6 Measurement instrumentation

The measurement instrumentation, including antennas, shall conform with the relevant requirements in CISPR 16-1-1 and CISPR 16-1-4.

7.2.7 Field-strength measurements on other out-door sites

Out-door test sites similar to an open area test site but without any metal ground plane may have to be prescribed for practical reasons for some products, e.g. ISM equipment and motor vehicles. The provisions given in 7.2.3 to 7.2.6 are valid.

7.2.8 Measurements in reverberating chambers

(Under consideration)

7.2.9 Measurement in absorber-lined shielded enclosures

7.2.9.1 Measurement in absorber-lined shielded enclosures with groundplane (semi-anechoic chambers = SAC or semi-anechoic Room = SAR)

(Under consideration.)

7.2.9.2 Measurement in fully absorber-lined shielded enclosures (fully anechoic chamber = FAC or fully anechoic room = FAR)

7.2.9.2.1 Test set-up

The same type of antenna shall be used for EUT emission testing as the receive antenna used for the FAR validation testing. The antenna height is fixed at the geometrical middle height of the test volume. Measurement will be done in horizontal and vertical polarisation of

the receive antenna. Emission should be measured while the turntable rotates with the EUT in each of at least three successive azimuth positions (0°, 45°, 90°), when continuous rotation is not required.

The test distance is measured from the reference point of the antenna to the boundary of the EUT. In the case of a difference between the reference point on an antenna and the phase centre, a correction factor may be applied to obtain the field strength at the test distance.

NOTE The correction factor, C_{Rd} dB, equation (4a), may be added to the field strength in order to reduce its uncertainty. In the calibration procedure of the antenna a phase correction factor C_{Rd} will be measured for each frequency. (The procedure will be defined with antenna calibration or calculated from the mechanical spacing of the log.-periodic elements) together with the Antenna Factor (AF). The two factors (C_{Rd} , and AF) will be added in dB to the voltage at the output of the antenna to get the field strength equation (4b). If a phase centre correction is not included, an additional term must be included in the uncertainty budget.

$$C_{Rd} = 20 \lg [(R + P_f - d)/R] \quad (4a)$$

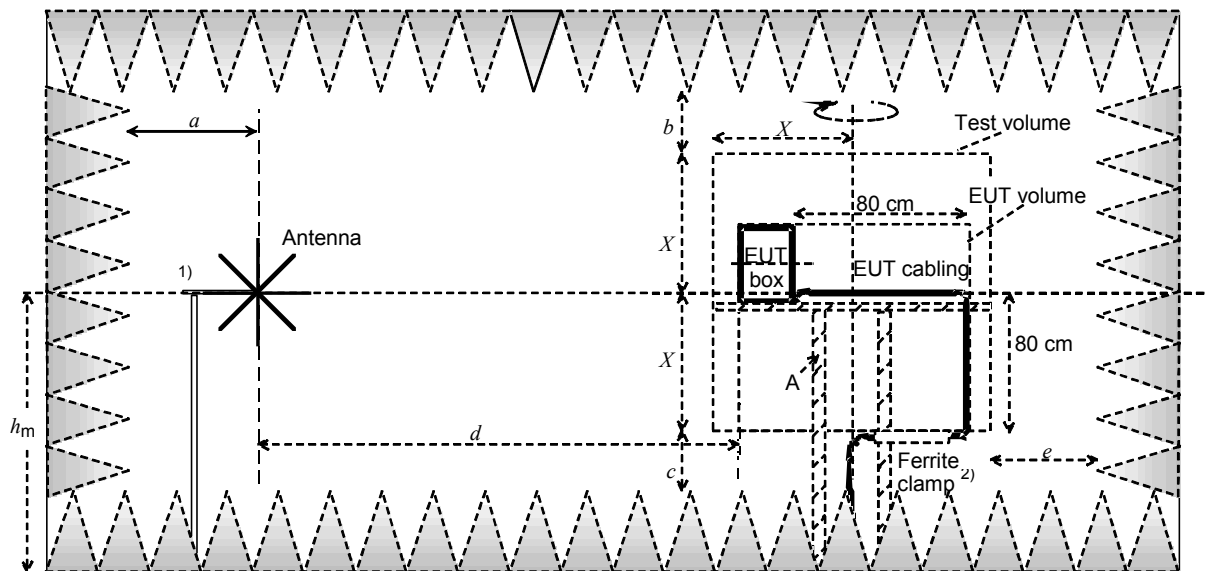
E-field strength is given by equation (4b):

$$E_f = V_f + AF_{FS(f)} + C_{Rd} \quad (4b)$$

where

- f = frequency, (MHz)
- R = the required separation point from the source to the reference point on the antenna (m).
- P_f = phase centre position as a function of frequency, (m from tip of antenna)
- d = distance of the reference point on the antenna from the antenna tip (m).
- E_f = E-field at distance d from source; expressed in dB ($\mu\text{V}/\text{m}$).
- V_f = voltage at output of antenna at frequency f ; expressed in dB (μV).
- C_{Rd} = phase centre correction factor; expressed in dB
- $AF_{FS(f)}$ = antenna factor (free space) for E-field at the phase centre; expressed in dB (m^{-1}).

Figure 6 illustrates typical test set-up.



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- A = turntable and EUT-support
- $2X = 1,5 \text{ m}; 2,5 \text{ m}; 5 \text{ m}$, i.e. corresponds to test distance used (3 m, 5 m, or 10 m respectively)
- h_m = middle level of the test volume
- a, b, c and $e \geq 0,5 \text{ m}$ recommended (≥ 1 is more convenient), the actual value is consistent with the FAR calibration procedure of CISPR 16-2-3.
- $d = 3 \text{ m}; 5 \text{ m}$ or 10 m

- 1) The antenna and cable lay-out shall be validated together and used in the same configuration during EUT-test.
- 2) Ferrite clamps are to be used in accordance with the applicable product standard. Their possible use (if required) must be documented in the test report.

Figure 6 – Typical test set-up in FAR, where a, b, c and e depend on the room performance

The EUT shall be placed on a turntable. Figures 6, 7 and 8 explain the different dimensions within the FAR. The turntable, antenna mast and supporting floor shall be in place during the validation procedure, and consist largely of material transparent to electromagnetic waves. The distances a , b , c and e may be limited by the size of the test volume. The level of the bottom plane (absorber height plus c) will be the level for floor standing equipment (transport pallet height will be outside the test volume).

7.2.9.2.2 EUT position

The EUT shall be configured, installed, arranged and operated in a manner consistent with typical applications. Interface cables shall be connected to each type of interface port of the EUT.

If the EUT consists of separate devices, the space between the devices shall be in normal configuration but with 10 cm separation if possible. Interconnecting cables shall be bundled. The bundle shall be around 30 cm to 40 cm long and longitudinal to the cable.

Ancillary equipment, which is required to exercise the EUT but does not form part of the EUT, shall be located outside the screened room.

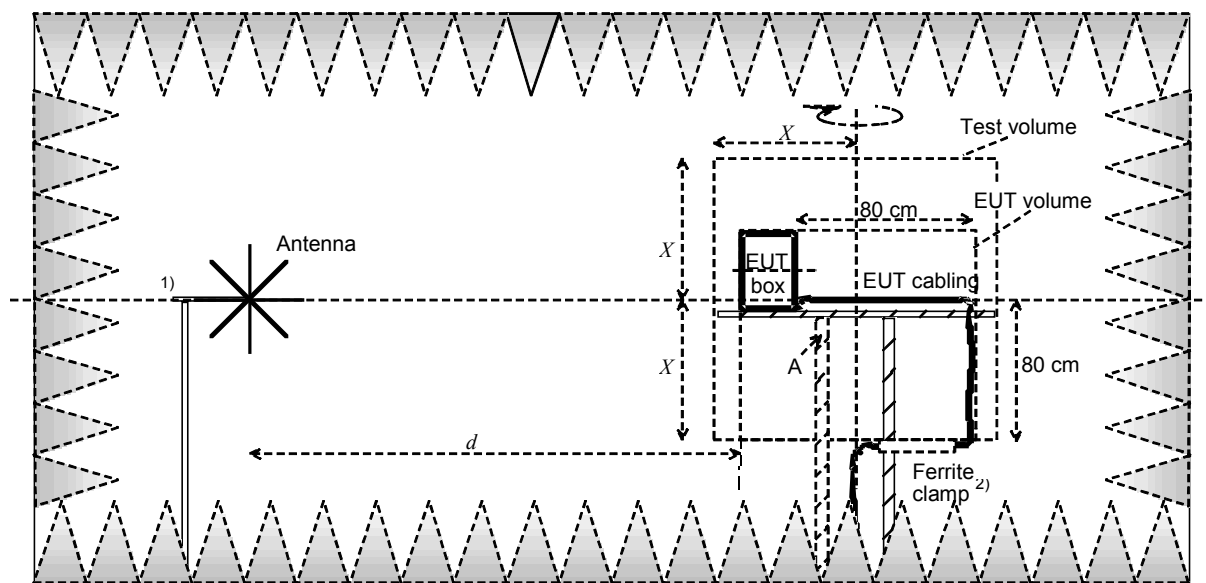
The entire EUT shall fit in the test volume.

To improve the measurement repeatability, the following guidelines shall be taken into account:

The EUT (including the cables laid out according to 7.2.9.2.3) shall be placed so that its centre is at the same height as the centre of the test volume. A non-conductive support of a suitable height may be used to achieve this.

Where it is not physically possible to elevate a large EUT to the centre of the test volume (Figures 6 and 7), the EUT may remain on a non-conductive transport pallet during the test (Figure 8). The height of the pallet shall be recorded in the test report.

Figures 7 and 8 illustrate the set-up of several types of EUT in the FAR.



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A = turntable and EUT-support

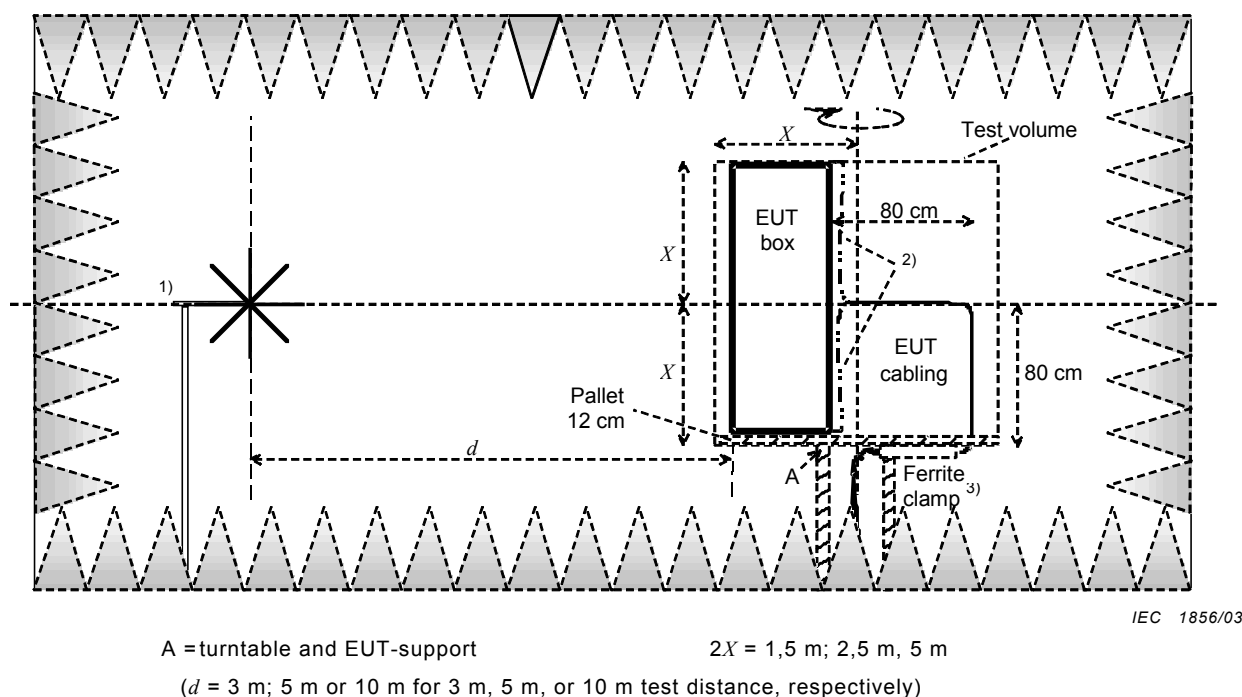
$2X = 1,5 \text{ m}; 2,5 \text{ m}, 5 \text{ m}$

$d = 3 \text{ m}; 5 \text{ m} \text{ or } 10 \text{ m}$ (for 3 m, 5 m, or 10 m test distance, respectively)

1) The antenna cable layout shall be the same as in the validation procedure (see Figure 6).

2) Ferrite clamps are to be used in accordance with the applicable product standard. Their possible use (if required) must be documented in the test report.

Figure 7 – Typical test set-up for table-top equipment within the test volume of a FAR



Pallet of 12 cm (10 cm to 14 cm) is a compromise between metal- and wooden ground.

- 1) The antenna cable layout shall be the same as in the validation procedure (see Figure 6).
- 2) The cable layout depends on the location of the cable outlets and shall be close to the surface of the housing
- 3) Ferrite clamps are to be used in accordance with the applicable product standard. Their possible use (if required) must be documented in the test report.

Figure 8 – Typical test set-up for floor standing equipment within the test volume of a FAR

The installation specifications for some floor standing equipment require the unit to be installed and bonded directly to a conductive floor. The reader is advised of the following notes for testing of floor standing equipment in a FAR:

For results obtained showing non-compliance to a FAR limit of floor standing equipment that is intended to be installed and bonded directly to a conductive floor may be lower if tested on a ground plane that better simulates the final installation environment. This is particularly true if the emissions are at a frequency below 200 MHz, horizontal polarisation, and the source of emissions is from a height on the equipment that would correspond to a height above ground of 0,4 m or less in a typical installation. The reader is advised that prior to a determination of non-compliance based on FAR measurements, additional investigation in a ground plane test environment (i.e. an Open Area Test Site or Semi-Anechoic chamber) is recommended to better simulate the equipment's intended installation condition.