

Electromagnetic compatibility (EMC) –

**Part 4-7: Testing and measurement
techniques – General guide on
harmonics and interharmonics
measurements and instrumentation, for
power supply systems and equipment
connected thereto**

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National foreword

This British Standard is the UK implementation of EN 61000-4-7:2002+A1:2009. It is identical with IEC 61000-4-7:2002 incorporating amendment 1:2009. It supersedes BS EN 61000-4-7:2002, which will be withdrawn on 1 March 2012.

The start and finish of text introduced or altered by amendment is indicated in the text by tags. Tags indicating changes to IEC text carry the number of the IEC amendment. For example, text altered by IEC amendment 1 is indicated by **A1** ~~A1~~.

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This publication does not purport to include all the necessary provisions of a contract. Users are responsible for its correct application.

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**Electromagnetic compatibility (EMC)
Part 4-7: Testing and measurement techniques -
General guide on harmonics and interharmonics
measurements and instrumentation,
for power supply systems and equipment connected thereto
(IEC 61000-4-7:2002)**

Compatibilité électromagnétique (CEM)
Partie 4-7: Techniques d'essai
et de mesure -
Guide général relatif aux mesures
d'harmoniques et d'interharmoniques,
ainsi qu'à l'appareillage de mesure,
applicable aux réseaux d'alimentation
et aux appareils qui y sont raccordés
(CEI 61000-4-7:2002)

Elektromagnetische Verträglichkeit (EMV)
Teil 4-7: Prüf- und Messverfahren -
Allgemeiner Leitfadens für Verfahren
und Geräte zur Messung
von Oberschwingungen und
Zwischenharmonischen in
Stromversorgungsnetzen und
angeschlossenen Geräten
(IEC 61000-4-7:2002)

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CENELEC

European Committee for Electrotechnical Standardization
Comité Européen de Normalisation Electrotechnique
Europäisches Komitee für Elektrotechnische Normung

Central Secretariat: rue de Stassart 35, B - 1050 Brussels

Foreword

The text of document 77A/382/FDIS, future edition 2 of IEC 61000-4-7, prepared by SC 77A, Low frequency phenomena, of IEC TC 77, Electromagnetic compatibility, was submitted to the IEC-CENELEC parallel vote and was approved by CENELEC as EN 61000-4-7 on 2002-10-01.

This European Standard supersedes EN 61000-4-7:1993.

The following dates were fixed:

- latest date by which the EN has to be implemented
at national level by publication of an identical
national standard or by endorsement (dop) 2003-07-01
- latest date by which the national standards conflicting
with the EN have to be withdrawn (dow) 2005-10-01

Annexes designated "normative" are part of the body of the standard.

Annexes designated "informative" are given for information only.

In this standard, annex ZA is normative and annexes A, B and C are informative.

Annex ZA has been added by CENELEC.

Endorsement notice

The text of the International Standard IEC 61000-4-7:2002 was approved by CENELEC as a European Standard without any modification.

In the official version, for Bibliography, the following notes have to be added for the standards indicated:

- | | | |
|----------------------|------|--|
| IEC 61000-3 (Series) | NOTE | Partly harmonized in EN 61000-3 series (not modified). |
| IEC 61010-1 | NOTE | Harmonized as EN 61010-1:2001 (not modified). |

Foreword to amendment 1

The text of document 77A/645/FDIS, future amendment 1 to IEC 61000-4-7:2002, prepared by SC 77A, Low frequency phenomena, of IEC TC 77, Electromagnetic compatibility, was submitted to the IEC-CENELEC parallel vote and was approved by CENELEC as amendment A1 to EN 61000-4-7:2002 on 2009-03-01.

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- latest date by which the national standards conflicting
with the amendment have to be withdrawn (dow) 2012-03-01

Annex ZA has been added by CENELEC.

Endorsement notice

The text of amendment 1:2008 to the International Standard IEC 61000-4-7:2002 was approved by CENELEC as an amendment to the European Standard without any modification.

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INTRODUCTION

IEC 61000 is published in separate parts, according to the following structure:

Part 1: General

General considerations (introduction, fundamental principles)
Definitions, terminology

Part 2: Environment

Description of the environment
Classification of the environment
Compatibility levels

Part 3: Limits

Emission limits
Immunity limits (in so far as they do not fall under the responsibility of the product committees)

Part 4: Testing and measurement techniques

Measurement techniques
Testing techniques

Part 5: Installation and mitigation guidelines

Installation guidelines
Mitigation methods and devices

Part 6: Generic standards

Part 9: Miscellaneous

Each part is further subdivided into several parts, published either as International Standards or as technical specifications or technical reports, some of which have already been published as sections. Other will be published with the part number followed by a dash and a second number identifying the subdivision (example: 61000-6-1).

These publications will be published in chronological order and numbered accordingly.

This part is an International Standard for the measurement of harmonic currents and voltages in power supply systems and harmonic currents emitted by equipment. It also specifies the performance of a standard measuring instrument.

ELECTROMAGNETIC COMPATIBILITY (EMC) ±

Part 4-7: Testing and measurement techniques ± General guide on harmonics and interharmonics measurements and instrumentation, for power supply systems and equipment connected thereto

1 Scope

This part of IEC 61000 is applicable to instrumentation intended for measuring spectral components in the frequency range up to 9 kHz which are superimposed on the fundamental of the power supply systems at 50 Hz and 60 Hz. For practical considerations, this standard distinguishes between harmonics, interharmonics and other components above the harmonic frequency range, up to 9 kHz.

This standard defines the measurement instrumentation intended for testing individual items of equipment in accordance with emission limits given in certain standards (for example, harmonic current limits as given in IEC 61000-3-2) as well as for the measurement of harmonic currents and voltages in actual supply systems. Instrumentation for measurements above the harmonic frequency range, up to 9 kHz is tentatively defined (see Annex B).

NOTE 1 This document deals in detail with instruments based on the discrete Fourier transform.

NOTE 2 The description of the functions and structure of the measuring instruments in this standard is very explicit and meant to be taken literally. This is due to the necessity of having reference instruments with reproducible results irrespective of the characteristics of the input signals.

NOTE 3 The instrument is defined to accommodate measurements of harmonics up to the 50th order.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

Ⓐ IEC 60038, *IEC standard voltages* Ⓐ

IEC 60050-161, *International Electrotechnical Vocabulary ± Chapter 161: Electromagnetic compatibility*

Ⓐ IEC 61000-2-2, *Electromagnetic compatibility (EMC) – Part 2-2: Environment – Compatibility levels for low-frequency conducted disturbances and signalling in public low-voltage power supply systems* Ⓐ

IEC 61000-3-2, *Electromagnetic compatibility (EMC) ± Part 3-2: Limits ± Limits for harmonic current emissions (equipment input current ≤16 A per phase)*

Ⓐ IEC 61000-3-12, *Electromagnetic compatibility (EMC) – Part 3-12: Limits – Limits for harmonic currents produced by equipment connected to public low-voltage systems with input current >16 A and ≤75 A per phase* Ⓐ

Ⓐ Text deleted Ⓐ

3 Definitions, symbols and indices

For the purposes of this part of IEC 61000, the definitions given in IEC 60050-161 (IEV) and the following, apply.

3.1 Definitions related to frequency analysis

A1 Notations: The following notations are used in the present guide for the Fourier series development because it is easier to measure phase angles by observations of the zero crossings:

$$f(t) = c_0 + \sum_{k=1}^{\infty} c_k \sin\left(\frac{k}{N} \omega_1 t + \varphi_k\right) \quad (1)$$

$$\text{with: } \begin{cases} c_k = |b_k + ja_k| = \sqrt{a_k^2 + b_k^2} \\ Y_{C,k} = \frac{c_k}{\sqrt{2}} \\ \varphi_k = \pi + \arctan\left(\frac{a_k}{b_k}\right) \text{ if } b_k < 0 & \varphi_k = \arctan\left(\frac{a_k}{b_k}\right) \text{ if } b_k > 0 \\ \varphi_k = \frac{\pi}{2} \text{ if } b_k = 0 \text{ and } a_k > 0 & \varphi_k = -\frac{\pi}{2} \text{ if } b_k = 0 \text{ and } a_k < 0 \\ \varphi_k = 0 \text{ if } |b_k| \leq \varepsilon \text{ and } |a_k| \leq \varepsilon, \\ \quad \text{with } \varepsilon = 0,05 \% U_{\text{nom}} \text{ and } \varepsilon = 0,15 \% I_{\text{nom}} \\ \quad \text{or } \varepsilon = 0,15 \% U_{\text{nom}} \text{ and } \varepsilon = 0,5 \% I_{\text{nom}} \\ \quad \text{respectively, see table 1 in IEC 61000-4-7} \end{cases} \quad (2)$$

$$\text{and: } \begin{cases} b_k = \frac{2}{T_N} \int_0^{T_N} f(t) \times \sin\left(\frac{k}{N} \omega_1 t\right) dt \\ a_k = \frac{2}{T_N} \int_0^{T_N} f(t) \times \cos\left(\frac{k}{N} \omega_1 t\right) dt \\ c_0 = \frac{1}{T_N} \int_0^{T_N} f(t) dt \end{cases} \quad (3)$$

NOTE 1 The above definition setting φ_k to zero for the cases where b_k and a_k have very small values provides guidance to instrument manufacturers, as phase measurements of very small amplitudes may result in very large deviations, hence there is no requirement to measure phase for such small signals.

ω_1 is the angular frequency of the fundamental ($\omega_1 = 2\pi f_{H,1}$);

T_N is the width (or duration) of the time window; the time window is that time span of a time function over which the Fourier transform is performed;

c_0 is the d.c. component;

c_k is the amplitude of the component with frequency $f_{C,k} = \frac{k}{N} f_{H,1}$;

$Y_{C,k}$ is the r.m.s. value of component c_k ;

$f_{H,1}$ is the fundamental frequency of the power system;

k is the ordinal number (order of the spectral component) related to the frequency resolution $\left(f_{C,1} = \frac{1}{T_N}\right)$;

N is the number of fundamental periods within the window width;

φ_k is the phase angle of spectral line k . **A1**

A1 NOTE 2 Strictly speaking these definitions apply to steady-state signals only. The Fourier series is actually in most cases performed digitally, i.e. as a Discrete Fourier Transform DFT, or a variant thereof, being the FFT.

The analogue signal $f(t)$ which has to be analyzed is sampled, A/D-converted and stored. Each group of M samples forms a time window on which DFT is performed. According to the principles of Fourier series expansion, the window width T_N determines the frequency resolution $f_{C,1} = 1/T_N$ (i.e. the frequency separation of the spectral components) for the analysis. Therefore the window width T_N must be an integer multiple N of the fundamental period T_1 of the system voltage: $T_N = N \times T_1$. The sampling rate is in this case $f_s = M/(NT_1)$ (where M = number of samples within T_N).

Before DFT-processing, the samples in the time window are often weighted by multiplying them with a special symmetrical function ('windowing function'). However, for periodic signals and synchronous sampling it is preferable to use a rectangular weighting window which multiplies each sample by unity.

The DFT-processor yields the orthogonal Fourier-coefficients a_k and b_k of the corresponding spectral-component frequencies $f_{C,k} = k/T_N$, $k = 0, 1, 2 \dots M-1$. However, only k values up to and including half of the maximum value are useful, the other half just duplicates them.

Under synchronized conditions, the component of harmonic order h related to the fundamental frequency $f_{H,1}$ appears as the spectral component of order k , where $k = hN$.

NOTE 3 The Fast Fourier Transform FFT is a special algorithm allowing short computation times. It requires that the number of samples M be an integer power of 2, $M = 2^i$, with $i \geq 10$ for example.

NOTE 4 The symbol Y is replaced, as required by the symbol I for currents, by the symbol U for voltages. Index C qualifies the variable as spectral component. **A1**

3.2 Definitions related to harmonics

A1 3.2.1 harmonic frequency

$f_{H,h}$
frequency which is an integer multiple of the fundamental frequency of the power system
($f_{H,h} = h \times f_{H,1}$)

NOTE The harmonic frequency $f_{H,h}$ is identical with the component frequency $f_{C,k}$ with $k = h \times N$.

3.2.2 harmonic order

h

(integer) ratio of a harmonic frequency to the fundamental frequency of the power system. In connection with the analysis using DFT and synchronisation between $f_{H,1}$ and f_s (sampling rate), the harmonic order h corresponds to the spectral component $k = h \times N$ (k = number of the spectral component, N = number of periods of the fundamental frequency in time window T_N)

3.2.3 r.m.s. value of a harmonic component

$Y_{H,h}$

r.m.s. value of one of the components having a harmonic frequency in the analysis of a non-sinusoidal waveform

For brevity, such a component may be referred to simply as a "harmonic"

NOTE 1 The harmonic component $Y_{H,h}$ is identical with the spectral component $Y_{C,k}$ with $k = h \times N$; ($Y_{H,h} = Y_{C,h \times N}$). The symbol Y is replaced, as required by the symbol I for currents, by the symbol U for voltages. The index H qualifies the variable I or U as harmonic.

NOTE 2 For the purposes of this standard, the time window has a width of $N = 10$ (50 Hz systems) or $N = 12$ (60 Hz system) fundamental periods, i.e. approximately 200 ms (see 4.4.1). This yields $Y_{H,h} = Y_{C,10 \times h}$ (50 Hz systems) and $Y_{H,h} = Y_{C,12 \times h}$ (60 Hz systems).

3.2.4 r.m.s. value of a harmonic group

$Y_{g,h}$

square root of the sum of the squares of the r.m.s. value of a harmonic and the spectral components adjacent to it within the time window, thus summing the energy contents of the neighbouring components with that of the harmonic proper. See also equation 8 and Figure 4. The harmonic order is given by the harmonic considered.

NOTE The symbol Y is replaced, as required by the symbol I for currents, by the symbol U for voltages. **A1**

A1 3.2.5**r.m.s. value of a harmonic subgroup** $Y_{sg,h}$

square root of the sum of the squares of the r.m.s. value of a harmonic and the two spectral components immediately adjacent to it. For the purpose of including the effect of voltage fluctuation during voltage surveys, a subgroup of output components of the DFT is obtained by summing the energy contents of the frequency components directly adjacent to a harmonic with that of the harmonic proper. (See also equation 9 and Figure 6.) The harmonic order is given by the harmonic considered

NOTE The symbol Y is replaced, as required by the symbol I for currents, by the symbol U for voltages. **A1**

3.3 Definitions related to distortion factors**A1 3.3.1****total harmonic distortion****THD** THD_Y (symbol)

ratio of the r.m.s. value of the sum of all the harmonic components ($Y_{H,h}$) up to a specified order ($h_{\max}$) to the r.m.s. value of the fundamental component ($Y_{H,1}$):

$$THD_Y = \sqrt{\sum_{h=2}^{h_{\max}} \left(\frac{Y_{H,h}}{Y_{H,1}} \right)^2} \quad (4)$$

NOTE 1 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages.

NOTE 2 The value of $h_{\max}$ is 40 if no other value is defined in a standard concerned with limits (IEC 61000-3 series).

3.3.2**group total harmonic distortion****THDG** $THDG_Y$ (symbol)

ratio of the r.m.s. value of the harmonic groups ($Y_{g,h}$) to the r.m.s. value of the group associated with the fundamental ($Y_{g,1}$):

$$THDG_Y = \sqrt{\sum_{h=h_{\min}}^{h_{\max}} \left(\frac{Y_{g,h}}{Y_{g,1}} \right)^2} \quad \text{where } h_{\min} \geq 2 \quad (5)$$

NOTE 1 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages.

NOTE 2 The value of $h_{\min}$ is 2 and that of $h_{\max}$ is 40 if no other values are defined in a standard concerned with limits (for example IEC 61000-3 series).

3.3.3**THDS****subgroup total harmonic distortion** $THDS_Y$ (symbol)

ratio of the r.m.s. value of the harmonic sub-groups ($Y_{sg,h}$) to the r.m.s. value of the sub-group associated with the fundamental ($Y_{sg,1}$):

$$THDS_Y = \sqrt{\sum_{h=h_{\min}}^{h_{\max}} \left(\frac{Y_{sg,h}}{Y_{sg,1}} \right)^2} \quad \text{where } h_{\min} \geq 2 \quad (6)$$

NOTE 1 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages.

NOTE 2 The value of $h_{\min}$ is 2 and that of $h_{\max}$ is 40 if no other values are defined in a standard concerned with limits (for example IEC 61000-3 series). **A1**

A1 3.3.4

partial weighted harmonic distortion

PWHD

$PWHD_{H,Y}$ (symbol)

ratio of the r.m.s. value, weighted with the harmonic order h , of a selected group of higher order harmonics (from the order $h_{\min}$ to $h_{\max}$) to the r.m.s. value of the fundamental:

$$PWHD_{H,Y} = \sqrt{\sum_{h=h_{\min}}^{h_{\max}} h \left(\frac{Y_{H,h}}{Y_{H,1}} \right)^2} \quad (7)$$

NOTE 1 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages.

NOTE 2 The concept of partial weighted harmonic distortion is introduced to allow for the possibility of specifying a single limit for the aggregation of higher order harmonic components. The partial weighted group harmonic distortion $PWHD_{g,Y}$ can be evaluated by replacing the quantity $Y_{H,h}$ by the quantity $Y_{g,h}$. The partial weighted sub-group harmonic distortion $PWHD_{sg,Y}$ can be evaluated by replacing the quantity $Y_{H,h}$ by the quantity $Y_{sg,h}$. The type of $PWHD$ ($PWHD_{H,Y}$, $PWHD_{g,Y}$ or $PWHD_{sg,Y}$) is defined in each standard which uses the $PWHD$, for example in standards concerned with limits (IEC 61000-3 series).

NOTE 3 The values of $h_{\min}$ and $h_{\max}$ are defined in each standard which uses the $PWHD_Y$, for example in a standard concerned with limits (IEC 61000-3 series). **A1**

3.4 Definitions related to interharmonics

A1 3.4.1

r.m.s. value of a spectral component

$Y_{C,k}$

in the analysis of a waveform, the r.m.s. value of a component whose frequency is a multiple of the inverse of the duration of the time window

NOTE 1 If the duration of the time window is multiple of the fundamental period, only some of the spectral components have frequencies which are integer multiples of the fundamental frequency.

NOTE 2 The frequency interval between two consecutive spectral components is the inverse of the width of the time window, approximately 5 Hz for the purposes of this standard.

NOTE 3 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages.

3.4.2

r.m.s. value of an interharmonic component

$Y_{C,i}$

r.m.s. value of a spectral component, $Y_{C,k} \neq h \times N$, with a frequency between two consecutive harmonic frequencies (see Figure 4). For brevity, such a component may be referred to simply as an "interharmonic".

NOTE 1 The frequency of the interharmonic component is given by the frequency of the spectral line. This frequency is not an integer multiple of the fundamental frequency.

NOTE 2 A difference is made between an "interharmonic component" produced as a physical component by an equipment, for example at 183,333 Hz, and a "spectral component" calculated by the instrument as the result of the waveform analysis e.g. for a 50 Hz system at 185 Hz (the frequency of the FFT bin). The "spectral component" is also the "harmonic component" for $h \times N$ where h is an integer.

3.4.3

r.m.s. value of an interharmonic group

$Y_{ig,h}$

r.m.s. value of all spectral components in the interval between two consecutive harmonic frequencies (see Figure 4).

NOTE 1 For the purpose of this standard, the r.m.s. value of the interharmonic group between the harmonic orders h and $h + 1$ is designated as $Y_{ig,h}$, for example the group between $h = 5$ and $h = 6$ is designated as $Y_{ig,5}$.

NOTE 2 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages. **A1**

A1 3.4.4

r.m.s. value of an interharmonic centred subgroup

$Y_{isg,h}$

r.m.s. value of all spectral components in the interval between two consecutive harmonic frequencies, excluding spectral components directly adjacent to the harmonic frequencies (see Figure 6)

NOTE 1 For the purpose of this standard, the r.m.s. value of the centred subgroup between the harmonic orders h and $h + 1$ is designated as $Y_{isg,h}$, for example the centred subgroup between $h = 5$ and $h = 6$ is designated as $Y_{isg,5}$.

NOTE 2 The symbol Y is replaced, as required, by the symbol I for currents or by the symbol U for voltages.

3.4.5

interharmonic group frequency

$f_{ig,h}$

mean of the two harmonic frequencies between which the group is situated, i.e. $f_{ig,h} = (f_{H,h} + f_{H,h+1})/2$.

3.4.6

interharmonic centred subgroup frequency

$f_{isg,h}$

mean of the two harmonic frequencies between which the subgroup is situated, i.e. $f_{isg,h} = (f_{H,h} + f_{H,h+1})/2$. **A1**

3.5 Notations

A1 3.5.1 Symbols

In this standard, voltage and current values are r.m.s. unless otherwise stated.

a	amplitude coefficient of a cosine component in a Fourier series
b	amplitude coefficient of a sine component in a Fourier series
c	amplitude coefficient in a Fourier series
f	frequency; function
$f_{C,k}$	spectral component frequency of order k
$f_{C,1}$	the frequency of the spectral component of order 1. The frequency resolution is equal to this frequency
$f_{g,h}$	harmonic-group frequency of order h
$f_{sg,h}$	harmonic-subgroup frequency of order h
$f_{ig,h}$	interharmonic-group frequency of order h
$f_{isg,h}$	interharmonic centred subgroup frequency of order h
$f_{H,h}$	harmonic component frequency of order h
$f_{H,1}$	fundamental frequency of the power system
f_s	sampling rate
$h_{\max}$	the order of the highest harmonic that is taken into account
$h_{\min}$	the order of the lowest harmonic that is taken into account
j	$\sqrt{-1}$
t	running time
B	bandwidth
I	current (r.m.s. value)
M	integer number; number of samples within the window width
N	number of power supply periods within the window width
P	power
T	time interval
T_1	fundamental period of the power supply system
T_N	window width comprising N fundamental periods
U	voltage (r.m.s. value)
Y	Variable replaceable by I , U A1

$Y_{C,k}$	r.m.s. value of the spectral component of order k
$Y_{g,h}$	r.m.s. value of harmonic group
$Y_{H,h}$	r.m.s. value of the harmonic component of order h
$Y_{ig,h}$	r.m.s. value of interharmonic group
$Y_{isg,h}$	r.m.s. value of interharmonic centred subgroup
$Y_{sg,h}$	r.m.s. value of harmonic subgroup
ω	angular frequency
ω_1	angular frequency of the power supply
φ	phase angle

3.5.2 Subscripts

b	centre-band frequency
h	running-integer number for harmonic orders
k	running-integer number for spectral components
m	measured value
max	maximum value
min	minimum value
o	smoothed value
g	grouped value
sg	sub-grouped value
i	interharmonic value
g,h	harmonic group associated with harmonic order h
sg,h	harmonic subgroup associated with harmonic order h
ig,h	interharmonic group above harmonic order h
isg,h	interharmonic centred sub-group above harmonic order h
og,h	smoothed harmonic group of order h
nom	nominal value
s	sampled
C	value related to spectral component
H	harmonic
f	frequency
0	d.c. related $\langle A1 \rangle$

4 General concepts and common requirements for all types of instrumentation

4.1 Characteristics of the signal to be measured

$\langle A1 \rangle$ Instruments for the following types of measurement are considered:

- harmonic emission measurement,
- interharmonic emission measurement,
- measurements above harmonic frequency range up to 9 kHz.

Strictly speaking the (Fast) Fourier Transform produces accurate results for steady state signals only. Signals whose amplitudes vary with time cannot be described correctly by their harmonic components only. In order to obtain reproducible harmonic emission analysis results when measuring products with fluctuating power, and thus fluctuating fundamental current and possibly fluctuating harmonic current levels, a combination of averaging techniques and sufficiently long measurement cycles can be used. This standard therefore provides a simplified method employing specific averaging methods (see 5.5.1). Furthermore, a test observation period, long enough to obtain successive measurement results that are within acceptable tolerance levels is specified in the harmonic emission standards referring to this standard. $\langle A1 \rangle$

4.2 Accuracy classes of instrumentation

Two classes of accuracy (I and II) are considered, to permit the use of simple and low-cost instruments, consistent with the requirements of the application. For emission tests, the upper class I is required if the emissions are near to the limit values (see also note 2 of table 1).

4.3 Types of measurement

Requirements for harmonic and interharmonic measurements are given. Measurements in the frequency range up to 9 kHz are also considered.