

Waveguide type dielectric resonators —

Part 2: Guidelines for oscillator and filter applications

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National foreword

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Part 2: Guidelines for oscillator and filter applications
(IEC 61338-2:2004)

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à modes guidés
Partie 2: Guide pour l'application
aux filtres et aux oscillateurs
(CEI 61338-2:2004)

Dielektrische Resonatoren vom
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Foreword

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Endorsement notice

The text of the International Standard IEC 61338-2:2004 was approved by CENELEC as a European Standard without any modification.

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INTRODUCTION

This part of IEC 61338 gives practical guidance on the use of waveguide type dielectric resonators that are used in telecommunications and radar systems (for general information, standard values, and test conditions, see the other parts of this series).

The features of these dielectric resonators are small size without degradation of quality factor, low mass, high reliability and high stability against temperature and ageing. The dielectric resonators are suitable for applications to miniaturized oscillators and filters with high performance.

This standard has been compiled in response to a generally expressed desire on the part of both users and manufacturers for guidelines for the use of dielectric resonators, so that the resonators may be used to their best advantage. For this purpose, general and fundamental characteristics have been explained in this standard.

WAVEGUIDE TYPE DIELECTRIC RESONATORS –

Part 2: Guidelines for oscillator and filter applications

1 Scope

This part of IEC 61338, which contains guidelines for use, is limited to the waveguide type dielectric resonators that are used for oscillator and filter applications. These types of resonators are now widely used in oscillators for direct broadcasting or communication satellite systems, oscillators for radio links, voltage-controlled oscillators for mobile communication systems and so on. In addition, these dielectric resonators are also used as an essential component of miniaturized filters for the same kind of applications.

It is not the aim of this standard either to explain theory or to attempt to cover all the eventualities that may arise in practical circumstances. This standard draws attention to some of the more fundamental questions, which should be considered by the user before he places an order for dielectric resonators for a new application. Such a procedure will be the user's insurance against unsatisfactory performance.

Standard specifications, such as those in the IEC 61338 series and national specifications or detail specifications issued by manufacturers, will define the available combinations of resonance frequency, the quality factor, the temperature coefficient of resonance frequency, etc. These specifications are compiled to include a wide range of dielectric resonators with standardized performances. It cannot be over-emphasized that the user should, wherever possible, select his dielectric resonators from these specifications, when available, even if it may lead to making small modifications to his circuit to enable standard resonators to be used. This applies particularly to the selection of the nominal frequency.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60068-1, *Environmental testing – Part 1: General and guidance*

IEC 60068-2-1, *Environmental testing – Part 2: Tests – Test A: Cold*

IEC 60068-2-2, *Environmental testing – Part 2: Tests – Tests B: Dry heat*

IEC 60068-2-6, *Environmental testing – Part 2: Tests – Test Fc: Vibration (sinusoidal)*

IEC 60068-2-7, *Environmental testing – Part 2: Tests – Test Ga: Acceleration, steady state*

IEC 60068-2-13, *Environmental testing – Part 2: Tests – Test M: Low air pressure*

IEC 60068-2-14, *Environmental testing – Part 2: Tests – Test N: Change of temperature*

IEC 60068-2-20, *Environmental testing – Part 2: Tests – Test T: Soldering*

IEC 60068-2-21, *Environmental testing – Part 2-21: Tests – Test U: Robustness of terminations*

IEC 60068-2-27, *Environmental testing – Part 2: Tests – Test Ea and guidance: Shock*

IEC 60068-2-29, *Environmental testing – Part 2: Tests – Test Eb and guidance: Bump*

IEC 60068-2-30, *Environmental testing – Part 2: Tests – Test Db and guidance: Damp heat, cyclic (12 + 12-hour cycle)*

IEC 60068-2-58, *Environmental testing – Part 2-58: Tests – Test Td: Test methods for solderability, resistance to dissolution of metallization and to soldering heat of surface mounting devices (SMD)*

IEC 60068-2-78, *Environmental testing – Part 2-78: Tests – Test Cab: Damp heat, steady state*

IEC 61338-1-1, *Waveguide type dielectric resonators – Part 1-1: General information and test conditions – General information*

IEC 61338-1-2, *Waveguide type dielectric resonators – Part 1-2: General information and test conditions – Test conditions*

IEC 61338-1-3, *Waveguide type dielectric resonators – Part 1-3: General information and test conditions – Measurement method of complex relative permittivity for dielectric resonator materials at microwave frequency*

3 Technical overview

It is of prime interest to a user that the resonator characteristics should satisfy particular specifications. The selection of oscillating circuits and dielectric resonators to meet that specification should be a matter of agreement between user and manufacturer.

Resonator characteristics are usually expressed in terms of resonance frequency, quality factor, etc. These characteristics are related to the dielectric characteristics in 5.3.

The specifications shall be satisfied between the lowest and highest temperatures of the specified operating temperature range and before and after environmental tests.

4 Fundamentals of waveguide type dielectric resonators

4.1 Principle of operation

When an electromagnetic wave passes through a dielectric waveguide with a relative permittivity of ϵ' , the interface between air and a dielectric will be a perfect reflector if the angle of incidence is greater than the critical angle θ , $\theta = \arcsin (1/\sqrt{\epsilon'})$, as shown in Figure 1.

In a very rough approximation, the air/dielectric interface can be considered to work as a magnetic wall (open-circuit), on which a normal component of the electric field and a tangential component of a magnetic field vanish. Thus, a dielectric rod with finite length functions as a resonator due to internal reflections of electromagnetic waves at the air/dielectric interface.

The size of a dielectric resonator can be considerably smaller than an empty resonant cavity at the same frequency. This is because the resonance frequency is determined when the resonator dimensions are of the order of half a wavelength of the electromagnetic wave, and because the wavelength is shortened in the dielectric according to the following equation:

$$\lambda_g = \frac{\lambda_0}{\sqrt{\epsilon'}} \quad (1)$$

where λ_g and λ_0 are the wavelengths in a dielectric with relative permittivity ϵ' and in vacuum. This size-reduction effect on microwave components is the biggest advantage in using the dielectric resonator.

4.2 Basic structure

The shape of a dielectric resonator is usually a disc or a cylinder which is a dielectric rod waveguide with finite length. Although the air/dielectric interface is considered to work roughly as a magnetic wall, some of the field actually leaks out (radiates) especially at the end faces, where the angle of incidences is less than the critical angle. In order to prevent such radiation losses, the resonator must be inside some form of shielding conductor.

As in a conventional metal wall cavity, there are various types of dielectric resonator structure and a number of modes can exist in each structure. Among these modes, the one with the lowest resonance frequency for certain diameter/length ratio is designated as the dominant mode. Figure 2 shows the three most commonly utilized dominant modes for dielectric resonators.

The $TE_{01\delta}$ mode dielectric resonator is characterized by a dominant TE (transverse electric) mode field distribution, the field of which leaks in the direction of wave propagation. This kind of mode resonator consists of a disc or a cylindrical-shaped dielectric resonator, a low ϵ' dielectric support, and a shielding conductor made of high-conductivity metals such as copper and silver. A high unloaded quality factor can be achieved using this mode.

The TM_{010} mode dielectric resonator is characterized by a TM (transverse magnetic) mode field distribution. This mode resonator has the middle levels of unloaded Q and size reduction effect between $TE_{01\delta}$ and TEM mode resonators. The TM_{010} mode resonator is often used for high-power applications such as filters for cellular base stations because of its construction which aids in the release of heat.

The TEM (transverse electromagnetic) mode dielectric resonator is characterized by a guided mode field distribution of a TEM mode with standing wave of a quarter wavelength. The inside, outside and one end of walls of a cylindrical dielectric resonator are fired or plated with a high-conductivity metal such as copper and silver. This mode dielectric resonator causes a significant size-reduction effect.

5 Dielectric resonator characteristics

5.1 Characteristics of dielectric resonator materials

The materials used to produce dielectric resonators should have a high relative permittivity (ϵ'), a low loss factor ($\tan \delta$) and a minimal temperature coefficient of resonance frequency (TCF). Table 1 shows the composition of several resonator materials with their dielectric properties at microwave frequencies.

Table 2 shows the dielectric properties of substrate materials. Dielectric resonators are mounted on these boards.

5.1.1 Relative permittivity (ϵ')

Relative permittivity of dielectric resonator materials is independent of frequency (i.e. constant) over the practical microwave frequency range, because the materials are made of para-electric ceramics. Materials with ϵ' from 20 to 100 are now typically used for dielectric resonators.

5.1.2 Loss factor ($\tan \delta$)

The quality factor of a material (Q_0) is defined as the reciprocal of loss factor:

$$Q_0 = 1/\tan \delta \quad (2)$$

As $\tan \delta$ increases proportionately with frequency for the ionic crystals, the product of Q_0 and frequency is approximately constant at microwave frequencies. So, the $Q_0 f$ product is often used as a figure of merit for each material. The materials with lower ε' generally have the lower $\tan \delta$.

5.1.3 Temperature coefficient of resonance frequency (TCF)

The TCF is given by the following equation as a material constant:

$$TCF = -\frac{1}{2}TC\varepsilon - \alpha \quad (3)$$

where

$TC\varepsilon$ is the temperature coefficient of relative permittivity, and

α is the coefficient of thermal expansion of the dielectric resonator.

The TCF is obtained by the following equation:

$$TCF = \frac{f_T - f_{ref}}{f_{ref}(T - T_{ref})} \times 10^6 \quad (4)$$

where

f_T is the resonance frequency at temperature T , and

f_{ref} is the resonance frequency at reference temperature T_{ref} .

The TCF of dielectric resonator material can be selected with a precision of $\pm 1 \cdot 10^{-6}/K$.

In the case where a material has a significant non-linear dependency on temperature, the following second-order temperature coefficient of resonance frequency TCF'' is used.

$$\frac{f_T - f_{ref}}{f_{ref}} = TCF'(T - T_{ref}) + TCF''(T - T_{ref})^2 \quad (5)$$

5.1.4 Insulation breakdown voltage

The breakdown voltage of dielectric resonator materials is usually higher than 10 kV/mm. For high-power applications such as filters for cellular base stations, precautions should be taken to ensure good heat dissipation from dielectric resonators, so as to prevent the decrease of breakdown voltage.

5.1.5 Coefficient of linear thermal expansion (α)

Dielectric resonators have a coefficient of linear thermal expansion from $+6 \cdot 10^{-6}/K$ to $+12 \cdot 10^{-6}/K$. When the resonator is soldered direct on a printed wired board (PWB), care must be taken to avoid the cracking of the ceramic body caused by the difference of coefficient of linear thermal expansion between the dielectric resonator and the PWB.