

Superconductivity —

Part 7: Electronic characteristic measurements — Surface resistance of superconductors at microwave frequencies

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National foreword

This British Standard was published by BSI. It is the UK implementation of EN 61788-7:2006. It is identical with IEC 61788-7:2006. It supersedes BS EN 61788-7:2002 which is withdrawn.

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A list of organizations represented on L/-/90 can be obtained on request to its secretary.

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Résistance de surface des
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Supraleitfähigkeit
Teil 7: Charakteristische elektronische
Messungen -
Oberflächenwiderstand von Supraleitern
bei Frequenzen im Mikrowellenbereich
(IEC 61788-7:2006)

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CENELEC

European Committee for Electrotechnical Standardization
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Foreword

The text of document 90/193/FDIS, future edition 2 of IEC 61788-7, prepared by IEC TC 90, Superconductivity, was submitted to the IEC-CENELEC parallel vote and was approved by CENELEC as EN 61788-7 on 2006-11-01.

This European Standard supersedes EN 61788-7:2002.

Examples of technical changes made are:

- closed type resonators are recommended from the viewpoint of the stable measurements;
- uniaxial-anisotropic characteristics of sapphire rods are taken into consideration for designing the size of the sapphire rods;
- recommended measurement frequency of 18 GHz and 22 GHz are added to 12 GHz described in EN 61788-7:2002.

The following dates were fixed:

- | | | |
|--|-------|------------|
| – latest date by which the EN has to be implemented
at national level by publication of an identical
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| – latest date by which the national standards conflicting
with the EN have to be withdrawn | (dow) | 2009-11-01 |

Annex ZA has been added by CENELEC.

Endorsement notice

The text of the International Standard IEC 61788-7:2006 was approved by CENELEC as a European Standard without any modification.

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INTRODUCTION

Since the discovery of some Perovskite-type Cu-containing oxides, extensive research and development (R & D) work on high-temperature oxide superconductors has been, and is being, made worldwide, and its application to high-field magnet machines, low-loss power transmission, electronics and many other technologies is in progress.

In various fields of electronics, especially in telecommunication fields, microwave passive devices such as filters using oxide superconductors are being developed and are undergoing on-site testing [1,2]¹⁾.

Superconductor materials for microwave resonators, filters, antenna and delay lines have the advantage of very low loss characteristics. Knowledge of this parameter is of primary importance for the development of new materials on the supplier side and for the design of superconductor microwave components on the customer side. The parameters of superconductor materials needed for the design of microwave low loss components are the surface resistance R_s and the temperature dependence of the surface resistance.

Recent advances in high T_c superconductor (HTS) thin films with R_s several orders of magnitude lower than that of normal metals have increased the need for a reliable characterization technique to measure this property [3,4]. Traditionally, the R_s of Nb or any other low temperature superconducting material was measured by first fabricating an entire three dimensional resonant cavity and then measuring its Q -value. The R_s could be calculated by solving the EM field distribution inside the cavity. Another technique involves placing a small sample inside a larger cavity. This technique has many forms but usually involves the uncertainty introduced by extracting the loss contribution due to the HTS films from the experimentally measured total loss of the cavity.

The best HTS samples are epitaxial films grown on flat crystalline substrates and no high quality films have been grown on any curved surface so far. What is needed is a technique that: can use these small flat samples; requires no sample preparation; does not damage or change the film; is highly repeatable; has great sensitivity (down to 1/1 000th the R_s of copper); has great dynamic range (up to the R_s of copper); can reach high internal powers with only modest input powers; and has broad temperature coverage (4,2 K to 150 K).

The dielectric resonator method is selected among several methods [5,6,7] to determine the surface resistance at microwave frequencies because it is considered to be the most popular and practical at present. Especially, the sapphire resonator is an excellent tool for measuring the R_s of HTS materials [8,9].

The test method given in this standard can be also applied to other superconductor bulk plates including low T_c material.

This standard is intended to provide an appropriate and agreeable technical base for the time being to engineers working in the fields of electronics and superconductivity technology.

The test method covered in this standard is based on the VAMAS (Versailles Project on Advanced Materials and Standards) pre-standardization work on the thin film properties of superconductors.

1) Figures in square brackets refer to the Bibliography.

SUPERCONDUCTIVITY –

Part 7: Electronic characteristic measurements – Surface resistance of superconductors at microwave frequencies

1 Scope

This part of IEC 61788 describes measurement of the surface resistance of superconductors at microwave frequencies by the standard two-resonator method. The object of measurement is the temperature dependence of R_s at the resonant frequency.

The applicable measurement range of surface resistances for this method is as follows:

- Frequency: $8 \text{ GHz} < f < 30 \text{ GHz}$
- Measurement resolution: $0,01 \text{ m}\Omega$ at 10 GHz

The surface resistance data at the measured frequency, and that scaled to 10 GHz , assuming the f^2 rule for comparison, are reported.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60050-815, *International Electrotechnical Vocabulary (IEV) – Part 815: Superconductivity*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in IEC 60050-815 apply.

In general, surface impedance Z_s for conductors, including superconductors, is defined as the ratio of the electric field E_t to the magnetic field H_t , tangential to a conductor surface:

$$Z_s = E_t / H_t = R_s + jX_s$$

where R_s is the surface resistance and X_s is the surface reactance.

4 Requirements

The surface resistance R_s of a superconductor film shall be measured by applying a microwave signal to a dielectric resonator with the superconductor film specimen and then measuring the attenuation of the resonator at each frequency. The frequency shall be swept around the resonant frequency as the centre, and the attenuation–frequency characteristics shall be recorded to obtain Q -value, which corresponds to the loss.

The target precision of this method is a coefficient of variation (standard deviation divided by the average of the surface resistance determinations) that is less than 20 % for the measurement temperature range from 30 K to 80 K .

It is the responsibility of the user of this standard to consult and establish appropriate safety and health practices and to determine the applicability of regulatory limitations prior to use.

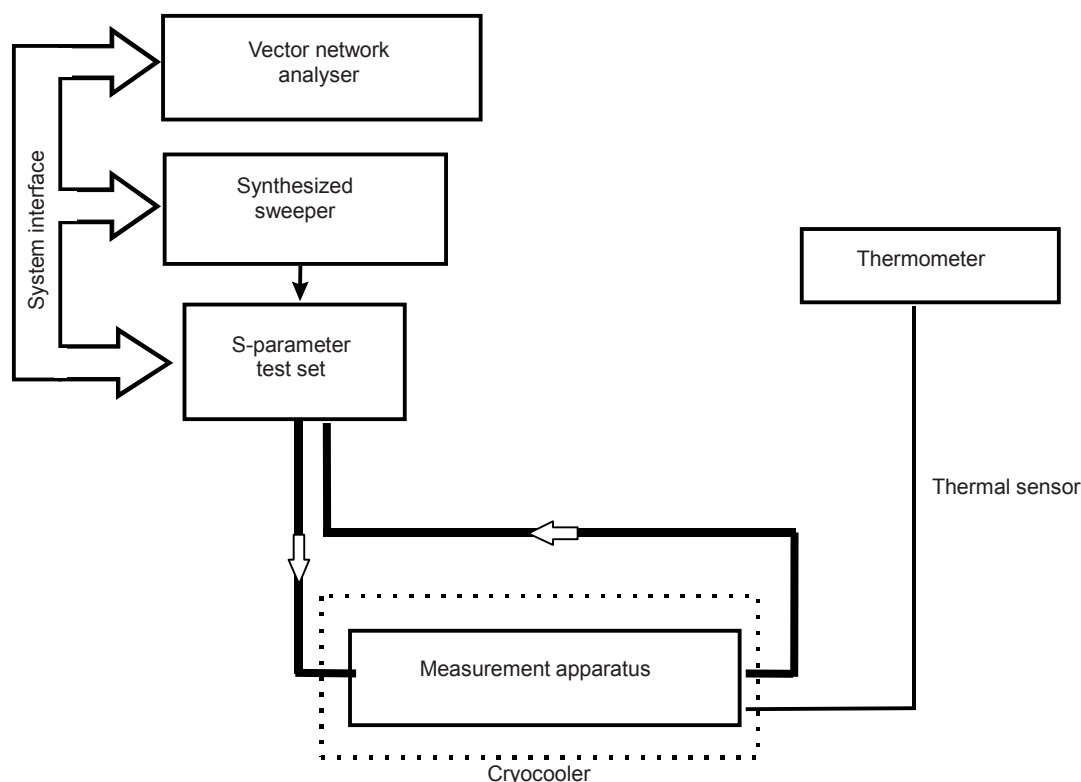
Hazards exist in this type of measurement. The use of a cryogenic system is essential to cool the superconductors to allow transition into the superconducting state. Direct contact of skin with cold apparatus components can cause immediate freezing, as can direct contact with a spilled cryogen. The use of an r.f.-generator is also essential to measure high-frequency properties of materials. If its power is too high, direct contact to human bodies can cause an immediate burn.

5 Apparatus

5.1 Measurement system

Figure 1 shows a schematic diagram of the system required for the microwave measurement. The system consists of a network analyzer system for transmission measurement, a measurement apparatus, and a thermometer for monitoring the measuring temperature.

An incident power generated from a suitable microwave source such as a synthesized sweeper is applied to the dielectric resonator fixed in the measurement apparatus. The transmission characteristics are shown on the display of the network analyzer.



IEC 004/02

Figure 1 – Schematic diagram of measurement system for temperature dependence of R_s using a cryocooler

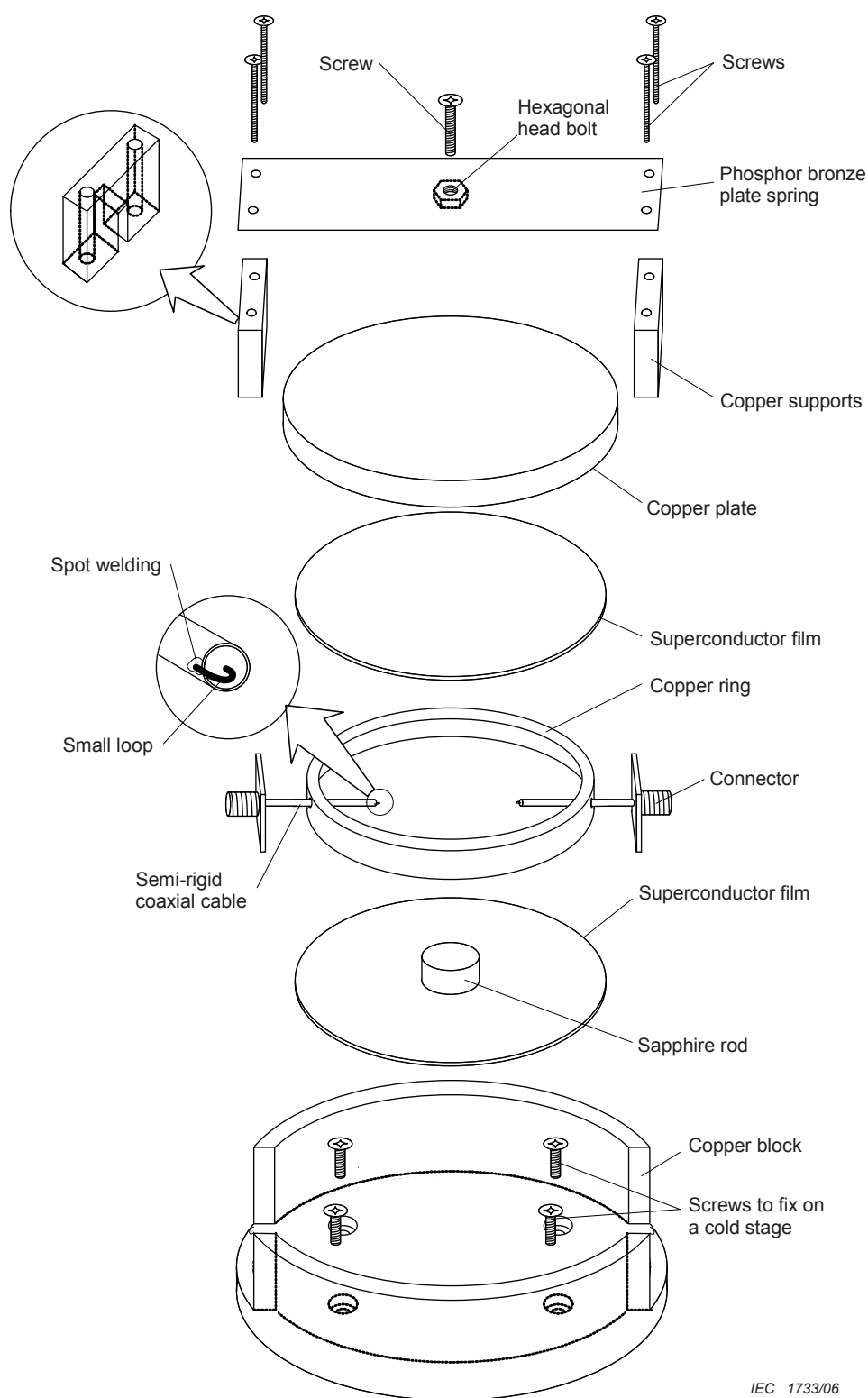
The measurement apparatus is fixed in a temperature-controlled cryocooler.

For the measurement of R_s for superconductor films, a vector network analyzer is recommended. A vector network analyzer has better measurement accuracy than a scalar network analyzer due to its wide dynamic range.

5.2 Measurement apparatus for R_s

Figure 2 shows a schematic of a typical measurement apparatus (closed type resonator) for the R_s of superconductor films deposited on a substrate with a flat surface. The upper superconductor film is pressed down by a spring, which is made of phosphor bronze. The plate type spring is recommended to be used for the improvement of measurement accuracy. This type of spring reduces the friction between the spring and the other part of the apparatus, and allows the smooth movement of superconductor films due to the thermal expansion of the dielectric rod. In order to minimize the measurement error, the sapphire rod and the copper ring shall be set in coaxial.

Two semi-rigid cables for measuring transmission characteristics of the resonator shall be attached on both sides of the resonator in an axial symmetrical position ($\phi = 0$ and π , where ϕ is the rotational angle around the central axis of the sapphire rod). Each of the two semi-rigid cables shall have a small loop at the ends. The plane of the loop shall be set parallel to that of the superconductor films in order to suppress the unwanted TM_{mn0} modes. The coupling loops shall be carefully checked for cracks in the spot weld joint that may have developed upon repeated thermal cycling. These cables can move right and left to adjust the insertion attenuation (IA). In this adjustment, coupling of unwanted cavity modes to the interested dielectric resonance mode shall be suppressed. Unwanted, parasitic coupling to the other modes reduces the high Q value of the TE mode resonator. For suppressing the parasitic coupling, special attention shall be paid to designing high Q resonators. Two other types of resonators along with the closed type shown in Figure 2 can be used. They are explained in Clause A.4.



IEC 1733/06

Figure 2 – Typical measurement apparatus for R_s