



BSI Standards Publication

Specification for radio disturbance and immunity measuring apparatus and methods

Part 1-4: Radio disturbance and immunity measuring apparatus —
Antennas and test sites for radiated disturbance measurements

National foreword

This British Standard is the UK implementation of EN IEC 55016-1-4:2019+A2:2023. It is identical to CISPR 16-1-4:2019, incorporating amendment 1:2020 and amendment 2:2023. It supersedes [BS EN IEC 55016-1-4:2019](#), which will be withdrawn on 20 July 2023.

The start and finish of text introduced or altered by amendment is indicated in the text by tags. Tags indicating changes to CISPR text carry the number of the CISPR amendment. For example, text altered by CISPR amendment 1 is indicated by **A1** **A1**.

The text of CISPR amendment 2:2023 has been provided in its entirety at the end of this document. BSI's policy of providing consolidated content remains unchanged; however, in the interest of expediency, in this instance BSI have chosen to collate the relevant content at the end of this document.

The UK participation in its preparation was entrusted to Technical Committee GEL/210, EMC - Policy committee.

A list of organizations represented on this committee can be obtained on request to its committee manager.

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Amendments/corrigenda issued since publication

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31 August 2020	Implementation of CISPR amendment 1:2020 with CENELEC endorsement A1:2020

Date	Text affected
30 June 2023	Implementation of CISPR amendment 2:2023 with CENELEC endorsement A2:2023

English Version

Specification for radio disturbance and immunity measuring
apparatus and methods - Part 1-4: Radio disturbance and
immunity measuring apparatus - Antennas and test sites for
radiated disturbance measurements
(CISPR 16-1-4:2019)

Spécifications des méthodes et des appareils de mesure
des perturbations radioélectriques et de l'immunité aux
perturbations radioélectriques - Partie 1-4: Appareils de
mesure des perturbations radioélectriques et de l'immunité
aux perturbations radioélectriques - Antennes et
emplacements d'essai pour les mesures des perturbations
rayonnées
(CISPR 16-1-4:2019)

Anforderungen an Geräte und Einrichtungen sowie
Festlegung der Verfahren zur Messung der hochfrequenten
Störaussendung (Funkstörungen) und Störfestigkeit - Teil 1-
4: Geräte und Einrichtungen zur Messung der
hochfrequenten Störaussendung (Funkstörungen) und
Störfestigkeit - Antennen und Messplätze für Messungen
der gestrahlten Störaussendung
(CISPR 16-1-4:2019)

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European Committee for Electrotechnical Standardization
Comité Européen de Normalisation Electrotechnique
Europäisches Komitee für Elektrotechnische Normung

CEN-CENELEC Management Centre: Rue de la Science 23, B-1040 Brussels

European foreword

The text of document CIS/A/1262/FDIS, future edition 4 of CISPR 16-1-4, prepared by CISPR SC A "Radio-interference measurements and statistical methods" of CISPR "International special committee on radio interference" was submitted to the IEC-CENELEC parallel vote and approved by CENELEC as EN IEC 55016-1-4:2019.

The following dates are fixed:

- latest date by which the document has to be implemented at national level by publication of an identical national standard or by endorsement (dop) 2019-11-12
- latest date by which the national standards conflicting with the document have to be withdrawn (dow) 2022-02-12

This document supersedes EN 55016-1-4:2010.

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IEC 61169-8	NOTE	Harmonized as EN 61169-8
IEC 61000-4-20	NOTE	Harmonized as EN 61000-4-20

Foreword to amendment A1

The text of document CIS/A/1316/FDIS, future CISPR 16-1-4/A1, prepared by CISPR SC A "Radio-interference measurements and statistical methods" of CISPR "International special committee on radio interference" was submitted to the IEC-CENELEC parallel vote and approved by CENELEC as EN IEC 55016-1-4:2019/A1:2020.

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CISPR 11	NOTE	Harmonized as EN 55011
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European foreword to Amendment 2

The text of document CIS/A/1389/FDIS, future CISPR 16-1-4/AMD2, prepared by CISPR SC A "Radio-interference measurements and statistical methods" of CISPR "International special committee on radio interference" was submitted to the IEC-CENELEC parallel vote and approved by CENELEC as EN IEC 55016-1-4:2019/A2:2023.

The following dates are fixed:

- latest date by which the document has to be implemented at national (dop) 2024-02-18 level by publication of an identical national standard or by endorsement
- latest date by which the national standards conflicting with the (dow) 2026-05-18 document have to be withdrawn

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The text of the International Standard CISPR 16-1-4:2019/AMD2:2023 was approved by CENELEC as a European Standard without any modification.

Annex ZA

(normative)

Normative references to international publications with their corresponding European publications

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

NOTE 1 Where an International Publication has been modified by common modifications, indicated by (mod), the relevant EN/HD applies.

NOTE 2 Up-to-date information on the latest versions of the European Standards listed in this annex is available here: www.cenelec.eu.

	<u>Publication</u>	<u>Year</u>	<u>Title</u>	<u>EN/HD</u>	<u>Year</u>	
	CISPR 16-1-1	2019	Specification for radio disturbance and immunity measuring apparatus and methods - Part 1-1: Radio disturbance and immunity measuring apparatus - Measuring apparatus	EN IEC 55016-1-1	2019	
	CISPR 16-1-5	2014	Specification for radio disturbance and immunity measuring apparatus and methods - Part 1-5: Radio disturbance and immunity measuring apparatus - Antenna calibration sites and reference test sites for 5 MHz to 18 GHz	EN 55016-1-5	2015	
	+ A1	2016		+ A1	2017	
	CISPR 16-1-6	2014	Specification for radio disturbance and immunity measuring apparatus and methods - Part 1-6: Radio disturbance and immunity measuring apparatus - EMC antenna calibration	EN 55016-1-6	2015	
	+ MD1	2017		+ 1	2017	
	+ MD2	2022		+ 2	2022	
	CISPR 16-2-3	2016	Specification for radio disturbance and immunity measuring apparatus and methods - Part 2-3: Methods of measurement of disturbances and immunity - Radiated disturbance measurements	EN 55016-2-3	2017	
	+ MD1	2019		+ 1	2019	
	+ MD2	20— ¹		+ 2	20— ¹	

¹ Under preparation.

<u>Publication</u>	<u>Year</u>	<u>Title</u>	<u>EN/HD</u>	<u>Year</u>
CISPR TR 16-3	-	Specification for radio disturbance and immunity measuring apparatus and methods -- Part 3: CISPR technical reports		-
CISPR 16-4-2	-	Specification for radio disturbance and immunity measuring apparatus and methods - Part 4-2: Uncertainties, statistics and limit modelling - Measurement instrumentation uncertainty	EN 55016-4-2	-
IEC 60050-191	-	International Electrotechnical Vocabulary - Chapter 191: Dependability and quality of service	-	-
 IEC 61000-4-20	-	Electromagnetic compatibility (EMC) - Part 4-20: Testing and measurement techniques - Emission and immunity testing in transverse electromagnetic (TEM) waveguides	EN IEC 61000-4-20	-
IEC 61000-4-21	-	Electromagnetic compatibility (EMC) - Part 4-21: Testing and measurement techniques - Reverberation chamber test methods	EN 61000-4-21	-



CONTENTS

FOREWORD	8
1 Scope	10
2 Normative references	10
3 Terms, definitions and abbreviated terms	11
3.1 Terms and definitions.....	11
3.2 Abbreviated terms.....	15
4 Antennas for measurement of radiated radio disturbance	16
4.1 General.....	16
4.2 Physical parameter (measurand) for radiated disturbance measurements	16
4.3 Antennas for the frequency range 9 kHz to 150 kHz.....	17
4.3.1 General.....	17
4.3.2 Magnetic field antenna.....	17
4.3.3 Shielding of loop antenna	17
4.4 Antennas for the frequency range 150 kHz to 30 MHz.....	17
4.4.1 Electric field antenna	17
4.4.2 Magnetic field antenna.....	18
4.4.3 Balance and electric field discrimination of antennas	18
4.5 Antennas for the frequency range 30 MHz to 1 000 MHz.....	18
4.5.1 General.....	18
4.5.2 Low-uncertainty antenna for use if there is an alleged non-compliance to the electric disturbance field strength limit	18
4.5.3 Antenna characteristics.....	18
4.5.4 Balance of antenna	20
4.5.5 Cross-polar response of antenna	22
4.6 Antennas for the frequency range 1 GHz to 18 GHz.....	23
4.6.1 General.....	23
4.6.2 Receive antenna	23
4.7 Special antenna arrangements – large-loop antenna system.....	25
5 Test sites for measurement of radio disturbance field strength for the frequency range of 9 kHz to 30 MHz	26
6 Test sites for measurement of radio disturbance field strength for the frequency range of 30 MHz to 1 000 MHz	26
6.1 General.....	26
6.2 OATS.....	26
6.2.1 General.....	26
6.2.2 Weather-protection enclosure	26
6.2.3 Obstruction-free area	26
6.2.4 Radio-frequency ambient environment of a test site	28
6.2.5 Ground plane.....	28
6.3 Suitability of other test sites	28
6.3.1 Other ground-plane test sites	28
6.3.2 Test sites without ground plane (FAR)	29
6.4 Test site validations	29
6.4.1 General.....	29
6.4.2 Overview of test site validations.....	30
6.5 Basic parameters of the NSA method for OATS and SAC.....	30

6.5.1	General equation and table of theoretical NSA values.....	30
6.5.2	Antenna calibration	34
6.6	Reference site method for OATS and SAC	34
6.6.1	General.....	34
6.6.2	Antennas not permitted for RSM measurements	35
6.6.3	Determination of the antenna pair reference site attenuation on a REFTS	35
6.6.4	Determination of the antenna pair reference site attenuation using an averaging technique on a large OATS.....	36
6.7	Validation of an OATS by the NSA method	39
6.7.1	Discrete frequency method	39
6.7.2	Swept frequency method.....	40
6.8	Validation of a weather-protection-enclosed OATS or a SAC	41
6.9	Possible causes for exceeding site acceptability limits	43
6.10	Site validation for FARs	44
6.10.1	General.....	44
6.10.2	RSM for FAR sites	48
6.10.3	NSA method for FAR sites	50
6.10.4	Site validation criteria for FAR sites	52
6.11	Evaluation of set-up table and antenna tower.....	52
6.11.1	General.....	52
6.11.2	Evaluation procedure for set-up table influences	53
7	Test sites for measurement of radio disturbance field strength for the frequency range 1 GHz to 18 GHz	54
7.1	General.....	54
7.2	Reference test site.....	55
7.3	Test site validation.....	55
7.3.1	General.....	55
7.3.2	Acceptance criterion for site validation.....	56
7.4	Antenna requirements for S_{VSWR} standard test procedure	56
7.4.1	General.....	56
7.4.2	Transmit antenna	57
7.4.3	Antennas and test equipment for the S_{VSWR} reciprocal test procedure	59
7.5	Required positions for site validation testing	60
7.5.1	General.....	60
7.5.2	Descriptions of S_{VSWR} measurement positions in a horizontal plane (Figure 23).....	60
7.5.3	Descriptions of S_{VSWR} additional measurement positions (Figure 24)	61
7.5.4	Summary of S_{VSWR} measurement positions.....	62
7.6	S_{VSWR} site validation – standard test procedure	65
7.7	S_{VSWR} site validation – reciprocal test procedure using an isotropic field probe	66
7.8	S_{VSWR} conditional measurement position requirements	67
7.9	S_{VSWR} site validation test report.....	68
7.10	Limitations of the S_{VSWR} site validation method.....	68
7.11	Alternative test sites	69
8	Common mode absorption devices	69
8.1	General.....	69
8.2	CMAD S -parameter measurements	69
8.3	CMAD test jig.....	69

8.4	Measurement method using the TRL calibration.....	70
8.5	Specification of ferrite clamp-type CMAD	72
8.6	CMAD performance (degradation) check using spectrum analyzer and tracking generator.....	73
9	Reverberating chamber for total radiated power measurement	75
9.1	General.....	75
9.2	Chamber.....	75
9.2.1	Chamber size and shape	75
9.2.2	Door, openings in walls, and mounting brackets.....	75
9.2.3	Stirrers	76
9.2.4	Test for the efficiency of the stirrers.....	76
9.2.5	Coupling attenuation.....	77
10	TEM cells for immunity to radiated disturbance measurement.....	78
Annex A (normative)	Parameters of antennas	79
A.1	General.....	79
A.2	Preferred antennas	79
A.2.1	General.....	79
A.2.2	Calculable antenna	79
A.2.3	Low-uncertainty antennas	79
A.3	Simple dipole antennas.....	80
A.3.1	General.....	80
A.3.2	Tuned dipole.....	81
A.3.3	Shortened dipole.....	81
A.4	Broadband antenna parameters	82
A.4.1	General.....	82
A.4.2	Antenna type	83
A.4.3	Specification of the antenna.....	83
A.4.4	Antenna calibration	84
A.4.5	Antenna user information	84
Annex B (XXX) (Void)		85
Annex C (normative)	Large-loop antenna system for magnetic field induced-current measurements in the frequency range of 9 kHz to 30 MHz.....	86
C.1	General.....	86
C.2	Construction of an LLAS	86
C.3	Construction of a large-loop antenna (LLA).....	86
C.4	Validation of an LLAS	91
C.5	Construction of the LLAS verification dipole antenna.....	93
C.6	Conversion factors	94
C.6.1	General.....	94
C.6.2	Current conversion factors for an LLAS with non-standard diameter	95
C.6.3	Conversion of LLAS measured current to magnetic field strength.....	96
C.7	Examples.....	98
Annex D (normative)	Construction details for open area test sites in the frequency range of 30 MHz to 1 000 MHz (see Clause 6)	100
D.1	General.....	100
D.2	Ground plane construction	100
D.2.1	Material	100
D.2.2	Roughness	100
D.3	Services to EUT.....	101

D.4	Weather-protection enclosure construction	101
D.4.1	Materials and fasteners.....	101
D.4.2	Internal arrangements	102
D.4.3	Size	102
D.4.4	Uniformity with time and weather	102
D.5	Turntable and set-up table	102
D.6	Receive antenna mast installation.....	103
Annex E (xxx)	(Void).....	104
Annex F (informative)	Basis for ± 4 dB site acceptability criterion (see Clause 6).....	105
F.1	General.....	105
F.2	Error analysis.....	105
Annex G (informative)	Examples of uncertainty budgets for site validation of a COMTS using RSM with a calibrated antenna pair (see 6.6)	107
G.1	Quantities to be considered for antenna pair reference site attenuation calibration using the averaging technique	107
G.2	Quantities to be considered for antenna pair reference site attenuation calibration using a REFTS	108
G.3	Quantities to be considered for COMTS validation using an antenna pair reference site attenuation	109
Annex H (informative)	Definition of uncertainty in cross-polar response measurement	110
H.1	General.....	110
H.2	Example uncertainty estimate	112
H.3	Rationale for the estimates of input quantities in Table H.1 and Table H.3	113
H.4	Measurement of XPR below 100 MHz at an OATS	114
Bibliography		116

Figure 1 – Schematic of radiation from EUT reaching an LPDA antenna directly and via ground reflection at a 3 m site, showing the beamwidth half-angle, φ , at the reflected ray.....	19
Figure 2 – RX antenna E-plane radiation pattern example, with limit area shaded for 3 m distance and 2 m EUT width.....	24
Figure 3 – Determination of maximum useable EUT width using half-power beamwidth	24
Figure 4 – Determination of maximum useable EUT height using half-power beamwidth	25
Figure 5 – Obstruction-free area of a test site with a turntable	27
Figure 6 – Obstruction-free area with stationary EUT	27
Figure 7 – Test point locations for 3 m and 10 m test distances	36
Figure 8 – Paired test point locations for all test distances.....	38
Figure 9 – Example of paired test point selection for a test distance of 10 m.....	38
Figure 10 – Illustration of an investigation of influence of antenna mast on A_{APR}	39
Figure 11 – Typical antenna positions for a weather-protected OATS or a SAC – vertical polarization validation measurements	42
Figure 12 – Typical antenna positions for a weather-protected OATS or a SAC – horizontal polarization validation measurements	42
Figure 13 – Typical antenna positions for a weather-protected OATS or a SAC – vertical polarization validation measurements for a smaller EUT	43
Figure 14 – Typical antenna positions for a weather-protected OATS or a SAC – horizontal polarization validation measurements for a smaller EUT	43
Figure 15 – Measurement positions for FAR site validation	46

Figure 16 – Example of one measurement position and antenna tilt for FAR site validation	48
Figure 17 – Typical quasi free-space test site reference SA measurement set-up	50
Figure 18 – Theoretical free-space NSA as a function of frequency for different measurement distances [see Equation (16)].....	52
Figure 19 – Position of the antenna relative to the edge above a rectangle set-up table (top view).....	54
Figure 20 – Antenna position above the set-up table (side view)	54
Figure 21 – Transmit antenna E-plane radiation pattern example (this example is for informative purposes only).....	58
Figure 22 – Transmit antenna H-plane radiation pattern (this example is for informative purposes only)	59
Figure 23 – S_{VSWR} measurement positions in a horizontal plane (see 7.5.2 for description).....	60
Figure 24 – S_{VSWR} positions (height requirements)	62
Figure 25 – S_{VSWR} conditional measurement position requirements	68
Figure 26 – Definition of the reference planes inside the test jig	70
Figure 27 – The four configurations for the TRL calibration	72
Figure 28 – Limits for the magnitude of S_{11} , measured according to the provisions of 8.1 to 8.3	73
Figure 29 – Example of a 50 Ω adaptor construction in the vertical flange of the jig	74
Figure 30 – Example of a matching adaptor with balun or transformer	74
Figure 31 – Example of a matching adaptor with resistive matching network.....	75
Figure 32 – Example of a typical paddle stirrer	76
Figure 33 – Range of coupling attenuation as a function of frequency for a chamber using the stirrer shown in Figure 32	77
Figure A.1 – Short dipole antenna factors for $R_L = 50 \Omega$	82
Figure C.1 – The LLAS, consisting of three mutually perpendicular large-loop antennas	88
Figure C.2 – An LLA containing two opposite slits, positioned symmetrically with respect to the current probe C	89
Figure C.3 – Construction of an LLA slit.....	89
Figure C.4 – Example of an LLA slit construction using a strap of printed circuit board to obtain a rigid construction	90
Figure C.5 – Construction of the metal box containing the current probe.....	90
Figure C.6 – Example showing the routing of several cables from an EUT to minimize capacitive coupling from the leads to the LLAS	91
Figure C.7 – The eight positions of the LLAS verification dipole during validation of an LLA	92
Figure C.8 – Reference validation factors for loops of 2 m, 3 m, and 4 m diameters.....	92
Figure C.9 – Construction of the LLAS verification dipole antenna	94
Figure C.10 – Sensitivity S_D of an LLA with diameter D relative to an LLA with 2 m diameter	95
Figure C.11 – Conversion factor C_{dA} [for conversion into dB(μ A/m)] for three standard measurement distances d	97
Figure D.1 – The Rayleigh criterion for roughness in the ground plane	101

Table 1 – Site validation methods applicable for OATS, OATS-based, SAC, and FAR site types	30
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Table 2 – Theoretical normalized site attenuation, A_N – recommended geometries for broadband antennas ^a (1 of 2)	32
Table 3 – Example template for A_{APR} data sets	35
Table 4 – RSM frequency steps	35
Table 5 – Maximum dimensions of test volume versus test distance	44
Table 6 – Frequency ranges and step sizes for FAR site validation	48
Table 7 – S_{VSWR} measurement position designations (1 of 3)	63
Table 8 – S_{VSWR} reporting requirements	68
Table C.1 – Reference validation factors of Figure C.8 for loops of 2 m, 3 m, and 4 m diameters	93
Table C.2 – Sensitivity S_D of an LLA with diameter D relative to an LLA with 2 m diameter (Figure C.10)	96
Table C.3 – Magnetic field strength conversion factor C_{dA} for three measurement distances (Figure C.11)	98
Table D.1 – Maximum roughness for 3 m, 10 m and 30 m measurement distances	101
Table F.1 – Error budget	105
Table G.1 – Antenna pair reference site attenuation calibration using the large-OATS averaging technique	107
Table G.2 – Antenna pair reference site attenuation calibration using REFTS	108
Table G.3 – COMTS validation using an antenna pair reference site attenuation	109
Table H.1 – Example uncertainty estimate for XPR measurement in a FAR and assumed $a_{xpT} = 22$ dB, $a_{xpR} = 34$ dB	113
Table H.2 – Uncertainties depending on other values of A_{xpT} (other assumptions as in Table H.1)	114
Table H.3 – Example uncertainty estimate for XPR measurement at an OATS and assumed $a_{xpT} = 22$ dB, $a_{xpR} = 34$ dB	115

INTERNATIONAL ELECTROTECHNICAL COMMISSION
INTERNATIONAL SPECIAL COMMITTEE ON RADIO INTERFERENCE

**SPECIFICATION FOR RADIO DISTURBANCE AND
IMMUNITY MEASURING APPARATUS AND METHODS –**

**Part 1-4: Radio disturbance and immunity measuring apparatus –
Antennas and test sites for radiated disturbance measurements**

FOREWORD

- 1) The International Electrotechnical Commission (IEC) is a worldwide organization for standardization comprising all national electrotechnical committees (IEC National Committees). The object of IEC is to promote international co-operation on all questions concerning standardization in the electrical and electronic fields. To this end and in addition to other activities, IEC publishes International Standards, Technical Specifications, Technical Reports, Publicly Available Specifications (PAS) and Guides (hereafter referred to as "IEC Publication(s)"). Their preparation is entrusted to technical committees; any IEC National Committee interested in the subject dealt with may participate in this preparatory work. International, governmental and non-governmental organizations liaising with the IEC also participate in this preparation. IEC collaborates closely with the International Organization for Standardization (ISO) in accordance with conditions determined by agreement between the two organizations.
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This fourth edition cancels and replaces the third edition published in 2010, Amendment 1:2012 and Amendment 2:2017. This edition constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition:

- provisions are added to address test site validation in the frequency range from 30 MHz to 1000 MHz using the reference site method, to take into account the receive antenna radiation pattern in the frequency range from 1 GHz to 18 GHz, and further details on test site validation using the NSA method with broadband antennas in the frequency range from 30 MHz to 1 000 MHz.

International Standard CISPR 16-1-4 has been prepared by CISPR subcommittee A: Radio-interference measurements and statistical methods.

It has the status of a basic EMC publication in accordance with IEC Guide 107, *Electromagnetic compatibility – Guide to the drafting of electromagnetic compatibility publications*.

The text of this International Standard is based on the following documents:

FDIS	Report on voting
CIS/A/1262/FDIS	CIS/A/1275/RVD

Full information on the voting for the approval of this International Standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts of CISPR 16 series, under the general title *Specification for radio disturbance and immunity measuring apparatus and methods*, can be found on the IEC website.

The committee has decided that the contents of the base publication and its amendments will remain unchanged until the stability date indicated on the IEC web site under "<http://webstore.iec.ch>" in the data related to the specific publication. At this date, the publication will be

- reconfirmed,
- withdrawn,
- replaced by a revised edition, or
- amended.

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SPECIFICATION FOR RADIO DISTURBANCE AND IMMUNITY MEASURING APPARATUS AND METHODS –

Part 1-4: Radio disturbance and immunity measuring apparatus – Antennas and test sites for radiated disturbance measurements

1 Scope

This part of CISPR 16 specifies the characteristics and performance of equipment for the measurement of radiated disturbances in the frequency range 9 kHz to 18 GHz. Specifications for antennas and test sites are included.

NOTE In accordance with IEC Guide 107, CISPR 16-1-4 is a basic EMC publication for use by product committees of the IEC. As stated in Guide 107, product committees are responsible for determining the applicability of the EMC standard. CISPR and its sub-committees are prepared to cooperate with product committees in the evaluation of the value of particular EMC tests for specific products.

The requirements of this publication apply at all frequencies and for all levels of radiated disturbances within the CISPR indicating range of the measuring equipment.

Methods of measurement are covered in Part 2-3, further information on radio disturbance is given in Part 3, and uncertainties, statistics and limit modelling are covered in Part 4 of CISPR 16.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

CISPR 16-1-1, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-1: Radio disturbance and immunity measuring apparatus – Measuring apparatus*

CISPR 16-1-5:2014, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-5: Radio disturbance and immunity measuring apparatus – Antenna calibration sites and reference test sites for 5 MHz to 18 GHz*
CISPR 16-1-5:2014/AMD1:2016

CISPR 16-1-6:2014, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 1-6: Radio disturbance and immunity measuring apparatus – EMC antenna calibration*
CISPR 16-1-6:2014/AMD1:2017

CISPR 16-2-3:2016, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 2-3: Methods of measurement of disturbances and immunity – Radiated disturbance measurements*

CISPR TR 16-3, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 3: CISPR technical reports*

CISPR 16-4-2, *Specification for radio disturbance and immunity measuring apparatus and methods – Part 4-2: Uncertainties, statistics and limit modelling – Measurement instrumentation uncertainty*

IEC 60050-161, *International Electrotechnical Vocabulary. Chapter 161: Electromagnetic compatibility*

3 Terms, definitions and abbreviated terms

For the purposes of this document, the terms, definitions and abbreviated terms given in CISPR 16-1-1, CISPR 16-1-5, IEC 60050-161 and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at <http://www.electropedia.org/>
- ISO Online browsing platform: available at <http://www.iso.org/obp>

3.1 Terms and definitions

3.1.1

antenna

transducer that converts the guided electromagnetic energy of the feed line into a radiated wave in space and vice versa

Note 1 to entry: In the context of this document, for antennas for which a balun is intrinsic to the functioning of the antenna, the term “antenna” includes the balun.

3.1.2

antenna factor

AF

F_a

ratio of the electric field strength of a plane wave incident from the direction corresponding to the mechanical boresight (i.e. the main axis of the antenna) to the voltage induced across a specified load connected to the antenna, measured in a free-space environment

Note 1 to entry: The abbreviation AF is used as a general term to denote antenna factor, whereas F_a denotes the boresight AF in free-space. AF is affected by the load impedance (typically 50 Ω) connected to the antenna, and is frequency dependent. For a biconical antenna this impedance could be up to 200 Ω . For antennas with no balun the impedance is equal to the load impedance, typically 50 Ω . AF can be affected by mutual coupling of the antenna to the ground plane, and is directivity dependent. For more details see the definitions and 4.2 in CISPR 16-1-6:2014.

Note 2 to entry: The AF has the physical dimension of m^{-1} and measured data are normally expressed in dB relative to 1/m [dB(m^{-1})]. In radiated disturbance measurements, if F_a is known, the strength of an incident field, E , can be estimated from a reading, V , of a measuring receiver connected to the antenna as follows:

$$E = V + F_a$$

where E is in dB($\mu V/m$), V is in dB(μV) and F_a is in dB(m^{-1}).

3.1.3

antenna pair reference site attenuation

A_{APR}

set of site attenuation measurement results for both vertical and horizontal polarizations using a pair of antennas separated by a defined distance at an ideal open-area test site, with one antenna at a specified fixed height above the ground plane, and the other antenna scanned over a specified height range in which the minimum insertion loss is recorded

Note 1 to entry: A_{APR} is an influence quantity for uncertainty calculation of site validation measurements using RSM.

Note 2 to entry: A_{APR} measurements are used for comparison to corresponding site attenuation measurements of a COMTS to evaluate the performance of the COMTS.

3.1.4

antenna reference point

midpoint of an antenna from which the distance to the EUT or second antenna is measured

Note 1 to entry: The antenna reference point is either defined by the manufacturer using a marker on LPDA antennas or by the calibration laboratory.

3.1.5

balun

device for transforming an unbalanced transmission line to a balanced transmission line and vice versa

Note 1 to entry: A balun is used, for example, to couple balanced antenna elements to an unbalanced feed line, such as a coaxial cable. A balun may exhibit inherent impedance transformation differing from unity.

3.1.6

calibration test site

CALTS

open area test site with metallic ground plane and tightly specified site attenuation performance in horizontal electric field polarization

Note 1 to entry: A CALTS is used for determining the free-space antenna factor of an antenna.

3.1.7

common mode absorption device

CMAD

device that may be applied on cables leaving the test volume in radiated disturbance measurements to reduce the compliance uncertainty

3.1.8

compliance test site

COMTS

environment that assures valid, reproducible measurement results of the disturbance field strength from equipment under test for comparison to a compliance limit

3.1.9

cross-polar response

XPR

measure of the rejection by the antenna of the cross-polarized field, when the antenna is rotated in a linearly polarized electromagnetic field that is uniform in phase and amplitude over the aperture of the antenna under test

3.1.10

EUT volume

cylinder defined by EUT boundary diameter and height that fully encompasses all portions of the actual EUT, including cable racks and 1,6 m of cable length (30 MHz to 1 GHz) and 0,3 m of cable length (1 GHz and above)

Note 1 to entry: The test volume is one of several criteria limiting the EUT volume (see CISPR 16-2-3).

Note 2 to entry: The EUT volume has a diameter D (boundary diameter) and height h .

3.1.11

fully-anechoic room

FAR

an enclosure, the six internal surfaces of which are lined with radio-frequency-energy absorbing material (i.e. RF absorber) that attenuates electromagnetic energy in the frequency range of interest

Note 1 to entry: For general radiated disturbance measurement purposes, a FAR should be constructed inside a shielded enclosure.

3.1.12 hybrid antenna

antenna consisting of a wire-element log-periodic dipole array (LPDA) section and a broadband dipole section

Note 1 to entry: The longest element of the LPDA section is typically resonant at approximately 200 MHz, and the boom is lengthened at the open-circuit end to feed the connected broadband dipole (e.g. biconical or bowtie) section. Over the range 30 MHz to 200 MHz, the broadband dipole exhibits a performance similar to a biconical antenna, notably in the variation of height-dependent antenna factor.

Note 2 to entry: A common-mode choke is typically used at the open-circuit (i.e. rear) end of the boom to minimize parasitic (unintended) RF currents on the outer conductor of the coaxial cable flowing into the measuring receiver.

3.1.13 ideal open-area test site

open-area test site having a perfectly flat, perfectly conducting ground plane of infinite area, and with no reflecting objects except the ground plane

Note 1 to entry: An ideal OATS is a theoretical construct that is used in the definition of the measurand A_{APR} and in the calculation of the theoretical normalized site attenuation A_N for ground plane sites.

3.1.14 insertion loss

loss arising from the insertion of a device into a transmission line, expressed as the ratio of voltages immediately before and after the point of insertion of a device under test, before and after the insertion

Note 1 to entry: Insertion loss is equal to the inverse of the transmission S -parameter, i.e. $|1/S_{21}|$.

3.1.15 low-uncertainty antenna

robust biconical or LPDA antenna that meets the balance and XPR requirements of this document, and whose antenna factor has an uncertainty of less than 0,5 dB, used for the measurement of electric field strength at a defined point in space

Note 1 to entry: Low-uncertainty antennas are further described in A.2.3.

3.1.16 mechanical boresight

boresight direction

boresight

direction of the main beam, which is defined by the geometric properties of the antenna

Note 1 to entry: For EMC antennas the direction of the main beam is usually: a) coincident with the direction in line with the mechanical longitudinal axis of LPDA antennas; b) orthogonal to the elements of monopole, dipole, and biconical antennas; and c) orthogonal to the front aperture of horn antennas. In each of these cases, the orthogonal line is coincident with the centre of the antenna.

3.1.17 null

minimum in signal level resulting from the vector sum of the direct and ground-reflected signals at the receive antenna and with the level being considerably lower than the in-phase sum of these signals

Note 1 to entry: The depth of a null is measured from the in-phase sum of the direct and ground reflected signals. A null in the received signal occurs when the antennas are above a ground plane at heights such that the direct and ground reflected signals are in anti-phase, which can result in large uncertainty in the measurement of field strength. A null extends from 90° to 180° out of phase. At 90° the null depth is approximately 6 dB. The depth is compared to the nearest adjacent maximum signal in the swept frequency response (or height scan of one antenna at a fixed frequency).

Note 2 to entry: The dip in signal level on boresight for some DRH antennas is sometimes referred to as a null. This definition does not apply to such dips.

Note 3 to entry: IEC 60050-726:1982, 726-02-07 defines standing-wave minimum, with synonym node (of a standing wave), as the location in a propagation medium where the vectorial sum of a specified field quantity of two waves creating a standing wave is a minimum.

3.1.18

quasi free-space test site

facility for radiated disturbance measurements that is intended to achieve free-space conditions

Note 1 to entry: Unwanted reflections from the surroundings are kept to a minimum, to satisfy the site acceptance criterion applicable to the radiated disturbance measurement procedure being considered.

3.1.19

reference test site

REFTS

open-area test site with metallic ground plane and tightly specified site attenuation performance in horizontal and vertical electric field polarizations

Note 1 to entry: Site attenuation measurements of a REFTS are used for comparison to corresponding site attenuation measurements of a compliance test site, in order to evaluate the performance of the compliance test site.

3.1.20

reflection coefficient

ratio of a common quantity to both the reflected and incident travelling waves

Note 1 to entry: Hence, the voltage reflection coefficient is defined as the ratio of the complex voltage of the reflected wave to the complex voltage of the incident wave. The voltage reflection coefficient is equal to the scattering parameter S_{11} .

3.1.21

resonant dipole antenna

tuned dipole antenna

antenna consisting of two straight collinear conductors of equal length, placed end to end, separated by a small gap constituting a balanced feed, with each conductor approximately a quarter-wavelength long such that at the specified frequency the input impedance of the wire antenna measured across the gap has zero reactance when the dipole is located in the free space

3.1.22

scattering parameters

S -parameters

set of four parameters used to describe the properties of a two-port network inserted into a transmission line

3.1.23

semi-anechoic chamber

SAC

shielded enclosure, in which five of the six internal surfaces are lined with radio-frequency absorbing material that attenuates electromagnetic energy (i.e. RF absorber) in the frequency range of interest, and the bottom horizontal surface is a conducting ground plane for use with OATS test set-ups

3.1.24

short-open-load-through calibration method

SOLT

through-open-short-match calibration method

TOSM

calibration method for a vector network analyzer using three known impedance standards – short, open, and match/load, and a single transmission standard – through

Note 1 to entry: The SOLT method is widely used, and the necessary calibration kits with 50 Ω characteristic impedance components are commonly available. A full two-port error model includes six error terms for each of the forward and reverse directions, for a total of twelve separate error terms, and requires twelve reference measurements to perform the calibration.

3.1.25 site attenuation

SA

A_s

minimum site insertion loss measured between two polarization-matched antennas located at a test site when one antenna is moved vertically over a specified height range and the other is set at a fixed height

Note 1 to entry: The terms site insertion loss (see 3.1.26) and site attenuation describe essentially the same measurement, however the term site attenuation (SA) is used in the context of finding the minimum site insertion loss (SIL) between a pair of antennas when one antenna is scanned in height above a ground plane.

3.1.26 site insertion loss

SIL

A_i

transmission loss between two polarization-matched antennas when a direct electrical connection between the signal generator output and the measuring receiver input is replaced by a transmit antenna and a receive antenna placed at specified positions at a test site

3.1.27 test volume

validated volume within a test facility in which an EUT may be positioned

Note 1 to entry: Validation procedures in this document are used to determine the test volume.

Note 2 to entry: The test volume as defined in this document is cylindrical in shape. Different test volume shapes have been defined in other documents, e.g. in cubic form in IEC 61000-4-20 [22] (TEM waveguides).

3.1.28 through-reflect-line (TRL) calibration

calibration method for a vector network analyzer using three known impedance standards “through”, “reflect,” and “line” for the internal or external calibration of the VNA

Note 1 to entry: Four reference measurements are needed for this calibration.

3.1.29 vector network analyzer

VNA

network analyzer capable of measuring complex values of the four S -parameters S_{11} , S_{12} , S_{21} , S_{22}

3.2 Abbreviated terms

The following are abbreviations used in this document that are not already given in 3.1.

AUT antenna under test

 DRH double ridged horn 

EUT equipment under test

FSOATS free-space OATS

HP horizontal polarization

LLA large-loop antenna

LLAS	large-loop antenna system
LPDA	log-periodic dipole array
NSA	normalized site attenuation
OATS	open-area test site
 PDF	probability density function 
RF	radio frequency
RSM	reference site method
RX	receive
S_{VSWR}	site voltage standing wave ratio
TX	transmit
VP	vertical polarization
VSWR	voltage standing wave ratio
 XP	cross polarization 

4 Antennas for measurement of radiated radio disturbance

4.1 General

Antennas of the type that are used for radiated disturbance measurements, having been calibrated, shall be used to measure the field strength, taking into account their radiation patterns and mutual coupling with their surroundings. The antenna and the circuits inserted between it and the measuring receiver shall not appreciably affect the overall characteristics of the measuring receiver. When the antenna is connected to the measuring receiver, the measuring system shall comply with the bandwidth requirements of CISPR 16-1-1 appropriate to the frequency band concerned.

The antenna shall be linearly polarized. It shall be orientable so that all polarizations of incident radiation can be measured. The height of the centre of the antenna above ground or above the absorber in a FAR may have to be adjustable according to a specific measurement procedure.

The accuracy of field-strength measurement of a uniform field of a sine-wave signal shall be better than ± 3 dB when an antenna meeting the requirements of this subclause is used with a measuring receiver meeting the requirements of CISPR 16-1-1.

NOTE This requirement does not include the effect due to a test site.

For additional information about the parameters of broadband antennas, see Annex A.

4.2 Physical parameter (measurand) for radiated disturbance measurements

The physical parameter for radiated disturbance measurements made against a disturbance limit expressed in volts per metre is electric field strength measured at a defined point in space relative to the position of the equipment under test (EUT). More specifically, for measurements in the frequency range 30 MHz to 1 000 MHz on an OATS or in a SAC, the measurand is the maximum field strength as a function of horizontal and vertical polarization and at heights between 1 m and 4 m, and at a horizontal distance of 10 m from the EUT, while the EUT is rotated over all angles in the azimuth plane.

4.3 Antennas for the frequency range 9 kHz to 150 kHz

4.3.1 General

Experience has shown that, in this frequency range, it is the magnetic field component that is primarily responsible for observed instances of interference.

4.3.2 Magnetic field antenna

For measurement of the magnetic component of the radiation, either an electrically-screened loop antenna of dimension such that the antenna can be completely enclosed by a square having sides of 60 cm in length, or an appropriate ferrite-rod antenna, may be used.

The unit of magnetic field strength is $\mu\text{A/m}$. In logarithmic units H is in $\text{dB}(\mu\text{A/m})$, or 20 times the log of the measured field strength level. The associated disturbance limit shall be expressed in the same units.

NOTE Direct measurements can be made of the strength of the magnetic component, in $\text{dB}(\mu\text{A/m})$ or $\mu\text{A/m}$ of a radiated field under all conditions, that is, both in the near field and in the far field. However, many field strength measuring receivers are calibrated in terms of the equivalent plane-wave electric field strength in $\text{dB}(\mu\text{V/m})$, i.e. assuming that the ratio of the E and H components is $120\pi\ \Omega$ or $377\ \Omega$. Calculations for H are as follows:

$$H = \frac{E}{377\ \Omega} \quad (1)$$

where H is typically in $\mu\text{A/m}$ and E in $\mu\text{V/m}$.

For measurements in dB:

$$H = E - 51,5 \quad (2)$$

where H is in $\text{dB}(\mu\text{A/m})$ and E in $\text{dB}(\mu\text{V/m})$.

The impedance used in the above conversions, $Z = 377\ \Omega$, with $20\ \lg Z = 51,5\ \text{dB}(\Omega)$, is a constant originating from the calibration of field strength measuring equipment indicating the magnetic field strength in $\mu\text{V/m}$ (or $\text{dB}(\mu\text{V/m})$).

4.3.3 Shielding of loop antenna

Inadequate shielding of a loop antenna can result in electric field response. The electric field discrimination of the antenna shall be evaluated by rotating the antenna in a uniform field, such that the plane of the loop remains parallel to the electric field vector. When the plane of the loop antenna is perpendicular to the magnetic flux and then the antenna is rotated so that its plane is parallel to the magnetic flux, the measured response shall decrease by at least 20 dB.

4.4 Antennas for the frequency range 150 kHz to 30 MHz

4.4.1 Electric field antenna

For the measurement of the electric component of the radiation, either a balanced or an unbalanced antenna may be used. If an unbalanced antenna is used, the measurement will refer only to the effect of the electric field on a monopole (rod) antenna. The type of antenna used shall be stated with the results of the measurements.

Information pertaining to calculating the performance characteristics of a monopole (rod) antenna and the characterization of its matching network is specified in CISPR 16-1-6. CISPR 16-1-6 states that the antenna factor derived by the Equivalent Capacitance Substitution Method (ECSM) has greater uncertainties for monopole lengths greater than one-eighth of a wavelength.

The unit of electric field strength shall be $\mu\text{V/m}$. In logarithmic units, E shall be expressed in $\text{dB}(\mu\text{V/m})$, or 20 times the logarithm of the measured field strength level. The associated disturbance limit shall be expressed in the same units.

4.4.2 Magnetic field antenna

For the measurement of the magnetic component of the radiation, an electrically-screened loop antenna, as described in 4.3.2 shall be used.

NOTE Tuned electrically balanced loop antennas can be used to make measurements of magnetic field strengths as low as $-51,5 \text{ dB}(\mu\text{A/m})$ using QP detection in the frequency range 1,6 MHz to 30 MHz, i.e. lower than with untuned electrically-screened loop antennas where the noise level is approximately 25 dB higher.

4.4.3 Balance and electric field discrimination of antennas

If a balanced electric field antenna is used, it shall comply with the requirement of 4.5.4. If a balanced magnetic field antenna is used, it shall comply with the requirement of 4.3.3.

4.5 Antennas for the frequency range 30 MHz to 1 000 MHz

4.5.1 General

In this frequency range, the measurements are of the electric field strength, so magnetic field antennas are not included. The antenna shall be a dipole-like antenna designed to measure the electric field strength, and the free-space antenna factor shall be used. The antenna types include:

- tuned dipole antennas, whose element pairs are either straight rods or conical in shape;
- dipole arrays such as the log-periodic dipole array (LPDA) antennas, comprising a series of staggered sets of straight rod elements;
- hybrid antennas.

4.5.2 Low-uncertainty antenna for use if there is an alleged non-compliance to the electric disturbance field strength limit

For lower measurement uncertainty, the value of electric field strength measured by a typical biconical antenna or LPDA antenna is preferred, in particular over hybrid antennas. Typical biconical and LPDA antennas are defined in Annex A, and only calibrated antennas shall be used.

NOTE 1 Improved uncertainties are achieved by using a biconical antenna over the frequency range 30 MHz to 250 MHz and an LPDA antenna over the range 250 MHz to 1 GHz. Alternatively, a change-over frequency of 200 MHz can be used, but uncertainties due to phase centre variations of the LPDA will be higher.

NOTE 2 The measurement uncertainty of radiated disturbance from an EUT depends on many different influence factors such as the quality of the site, antenna factor uncertainty, antenna type, and the measuring receiver characteristics. The reason for defining low-uncertainty antennas is to limit other antenna influences on the measurement uncertainty, such as the effect of mutual coupling with a ground plane, the radiation pattern with respect to height scanning, and the variable phase centre position. Verification of effects of these influences is accomplished by a comparison of the readings of the two antennas at the selected change-over frequency, which should give the same value of electric field strength within a margin of $\pm 1 \text{ dB}$.

4.5.3 Antenna characteristics

Given that the sensitivity of the simple dipole antenna is low in the frequency range 300 MHz to 1 000 MHz, a more complex antenna may be used. Such an antenna shall have characteristics as follows:

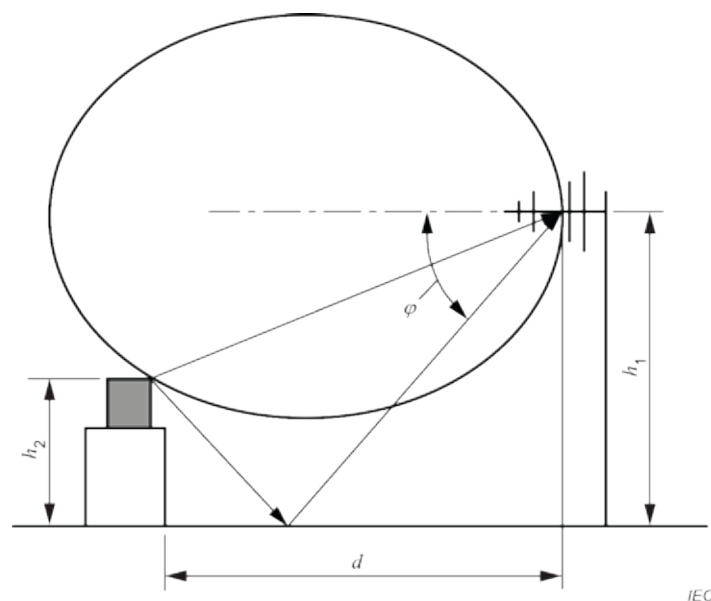
- a) The antenna shall be linearly polarized, which shall be evaluated by applying the cross-polarization test procedure of 4.5.5.
- b) Balanced dipole antennas, such as tuned-dipole and biconical antennas, shall have validated balun performance, which shall be evaluated by applying the balance test procedure of 4.5.4. This requirement also applies to hybrid antennas below 200 MHz.

- c) The return loss of the antenna with the antenna feeder connected shall not be less than 10 dB. A matching attenuator may be part of the antenna feeder cable for antennas if needed to meet this requirement.
- d) An antenna factor (AF) shall be given making it possible to fulfil the accuracy requirements of 4.1.

Accounting for the antenna directivity: a test site with a conducting ground plane is assumed for the following antenna characteristic description. The amplitude of the received signal will be reduced if either or both the direct and ground-reflected signals from the EUT to the antenna are not entering the main lobe of the radiation pattern of the antenna at its peak. The peak is usually in the boresight direction of the antenna. This reduction in amplitude is taken to be an error in the radiated disturbance measurement result; the ensuing uncertainty tolerance is based on the beamwidth, 2φ (see Figure 1).

Conditions for ensuring that this error is no larger than + 1 dB are given in item 1) for a 10 m site, and in item 2) for a 3 m site. Alternatively, a condition based on antenna gain is given in item 3), in lieu of the rigorous radiation pattern conditions.

Radiated disturbance measurements are performed with the antenna horizontally and vertically polarized in turn. If it is chosen to measure the radiation patterns in only one plane, the narrower beamwidth pattern results shall be used, and with the condition that the pattern of the antenna shall be verified in the horizontal plane while orienting it for horizontal polarization.



NOTE Parameters are defined in Equation (4).

Figure 1 – Schematic of radiation from EUT reaching an LPDA antenna directly and via ground reflection at a 3 m site, showing the beamwidth half-angle, φ , at the reflected ray

- 1) For a 10 m OATS or SAC, the antenna response in the direction of the direct ray differs negligibly from the boresight amplitude when the antenna is aligned such that its boresight direction is parallel to the ground plane. The directivity component of the uncertainty in the disturbance measurement can be kept to less than +1 dB if the antenna response in the direction of the reflected ray is no more than 2 dB lower than the antenna boresight response. To ensure this condition, the total vertical beamwidth 2φ of the measurement antenna, within which the antenna gain is within 2 dB of its maximum, shall be such that:

$$\varphi > \tan^{-1} \frac{h_1 + h_2}{d} \quad (3)$$

- 2) For sites with less than 10 m separation, typically 3 m, the total vertical beamwidth 2φ of the measurement antenna, within which the antenna gain is within 1 dB of its maximum, shall be such that:

$$2\varphi > \left(\tan^{-1} \frac{h_1 + h_2}{d} \right) - \left(\tan^{-1} \frac{h_1 - h_2}{d} \right) \quad (4)$$

where

h_2 is the height of the equipment under test;

h_1 is the measurement antenna height;

d is the horizontal distance between the phase centre of the measurement antenna and the device under test.

Antenna down-tilting can reduce the associated uncertainties; if that is not employed, the reduction in received signal shall be calculated from the radiation patterns and applied as a correction with associated directivity uncertainties. Example uncertainty budgets are given in CISPR 16-4-2.

NOTE 1 Assuming an E-plane radiation pattern normalized to unity on boresight (i.e. peak of the mainlobe) record the electric field at the angles of declination from the antenna for the direct ray, E_D , and reflected ray, E_R . The error, compared to an electric field of unity magnitude for each of the direct and reflected rays, is given in decibels by $20 \lg [2/(E_D + E_R)]$.

NOTE 2 The reduction in signal strength caused by reduced directivity at angles off antenna boresight is a systematic error and therefore can be corrected. If a correction is applied, from knowledge of the radiation patterns at each frequency and polarization, the uncertainty of field-strength measurement can be reduced accordingly.

- 3) For the broad beamwidth antenna types typically used for radiated disturbance measurements, such as biconical, LPDA, and hybrid antennas, the beamwidth is inversely related to the antenna directivity. An alternative to the criterion based on beamwidths in items 1) and 2) is to specify the maximum gain of an antenna, then refer to generic uncertainty tolerances for the directivity component in the uncertainty budget for the disturbance measurement results. The generic uncertainties, based on the narrowest beamwidths in the frequency range used for a specific antenna, are given in CISPR 16-4-2. The maximum isotropic antenna gain for biconical antennas shall be 2 dB, and shall be 8 dB for LPDA and hybrid antennas. For V-type LPDA antennas, whose H-plane beamwidth is equal to the E-plane beamwidth, the maximum permitted isotropic gain shall be 9 dB.

4.5.4 Balance of antenna

4.5.4.1 General

In radiated disturbance measurements, common-mode (CM) currents can be present on the cable attached to the receive antenna (antenna cable). In turn, these CM currents create electromagnetic fields that can be picked up by the receive antenna if the balun is not perfectly balanced. Consequently, the radiated disturbance measurement results can be influenced.

The major contributions to the antenna cable CM currents are caused by:

- the electric field strength to be measured, if it has a component parallel to the antenna cable, and
- the conversion of the differential mode (DM) antenna signal (the desired signal) into a CM signal by the imperfection of the balun of the receive antenna.

In general, LPDA antennas do not exhibit significant DM/CM (DM to CM) conversion. Therefore the following check applies for dipole and biconical antennas over their entire

operating frequency range, and to hybrid antennas over the frequency range of the broadband dipole section (in most cases 30 MHz to 200 MHz).

4.5.4.2 Balun DM/CM conversion check

The following method describes the measurement of two voltages V_1 and V_2 . The ratio of these voltages, both expressed in identical units, e.g. μV , is a measure of the DM/CM conversion (also known as the balun imbalance, balun symmetry, or antenna symmetry).

- a) Set the receive AUT vertically polarized with its centre at a height of 1,0 m above the ground plane of an OATS or SAC. The tip of the antenna shall be at least 0,25 m above the ground plane. Extend a $1,5 \text{ m} \pm 0,1 \text{ m}$ length of the antenna cable horizontally behind the rear active element of the receive antenna at a height of 1,0 m above the ground plane, and then allow it to drop vertically to the ground plane.
- b) For a standard characterization of the receive antenna imbalance, place a second (transmit) antenna vertically polarized at a horizontal distance of 10 m from the centre of the AUT. The centre of the transmit antenna shall be at a height of 1,0 m above the ground plane, and its tip shall be at least 0,25 m above the ground plane. The transmit antenna shall be linearly polarized, and have a cross-polar rejection greater than 20 dB over the frequency range of the balun test. For the frequency range above 200 MHz, transmit antenna height variation shall be used to avoid nulls in the SIL response. Measurements at shorter distances (e.g. 3 m and 5 m) may be made to determine the uncertainty contribution of balun imbalance at these distances.
- c) Connect the transmit antenna to a signal source (for example, a tracking generator or the source output of a network analyzer). Next, set the output level of that signal source so that over the frequency range of interest, and for both vertical orientations of the antenna, the signal-to-ambient noise ratio at the receiver is 34 dB (17 dB for average detection) or more.
- d) Record the voltage V_1 at the receiver over the frequency range of interest.
- e) Invert the receive antenna (i.e. rotate that antenna through 180°) without changing anything else in the set-up, in particular the receive antenna cable, and without changing the setting of the signal source.
- f) Record the voltage V_2 at the receiver over the frequency range of interest.
- g) The DM/CM conversion is sufficiently low if $|20 \lg (V_1/V_2)| < 1 \text{ dB}$.

NOTE 1 For the purpose of radiated disturbance measurements, if the DM/CM conversion criterion is not met, ferrite rings around the antenna cable can reduce the DM/CM conversion. The EMC test laboratory can repeat the test with four ferrite rings spaced approximately 20 cm apart; the first placed within 10 cm of the input to the balun. If the criterion is met by using these ferrite rings, then the ferrite rings also apply in the actual disturbance measurements. Likewise, the interaction with the cable can be reduced by extending the cable several metres horizontally behind the antenna before dropping to the ground plane.

NOTE 2 If the receive antenna is used in a FAR, the DM/CM check can be performed in that FAR, with the receive antenna at its usual location and the transmit antenna at least 3 m away. The antennas are best positioned centrally in the room with a clearance behind the antennas of at least 1 m between the vertical portion of cable and the tips of the absorbers.

NOTE 3 The measuring site and its conducting ground plane (OATS or SAC), or the FAR, are assumed to comply with the respective site validation requirements.

NOTE 4 The horizontal distance of 1,5 m over which the antenna cable runs horizontally behind the centre of the antenna is understood as kept as the minimum distance allowed during the actual vertically polarized radiated disturbance measurements.

NOTE 5 In general it is not necessary to strictly define a test set-up, because the imbalance effect is dominated by the interaction of the antenna and that part of the antenna cable that lies parallel to the antenna elements. Also there is a much smaller effect that is dependent on the uniformity of the field incident on the receive antenna in normal EMC measurement set-ups at an OATS or in a FAR.

NOTE 6 For baluns that have the receive cable connector mounted on the side (90° to the antenna boom), a right angle connector can be used to reduce the movement of the cable.

NOTE 7 The uncertainty of the balun DM/CM measurement result will be caused only by any nonlinearity of the receiver, because everything else remains unchanged during the V_1 and V_2 measurements. A nonlinearity of less than 0,1 dB within the $\pm 1 \text{ dB}$ range from the reference indication V_1 is good enough to meet the 1 dB criterion.

4.5.5 Cross-polar response of antenna

When an antenna is placed in a linearly-polarized electromagnetic field, the terminal voltage when the antenna and field are cross-polarized shall be at least 20 dB below the terminal voltage when they are co-polarized. This requirement applies over the entire frequency range of 30 MHz to 18 GHz. In practice, this requirement is not satisfied by some types of LPDA antennas for which the two halves of each dipole are in echelon, which intrinsically generates a cross-polar response (XPR).

The majority of testing with LPDA antennas is above 200 MHz. To achieve free-space conditions, a high-quality fully anechoic room, or antenna support towers of sufficient height above ground on an outdoor range may be used; see 6.3.2 of this document and Clause 6 of CISPR 16-1-5:2014 for associated site characteristics. A uniform field shall be set up across the effective length of the AUT. The separation between the centre of the AUT and the transmit antenna shall be greater than one wavelength. For an LPDA antenna, the separation is to its centre mark. When the lowest frequency is 200 MHz, a fixed separation of 1,5 m over the entire frequency range is recommended.

Set the transmit antenna and the AUT vertically polarized and note the signal strength over the frequency range. Rotate the transmit antenna by 90° and note the difference in signal strength relative to the co-polar reading.

NOTE A good-quality site is needed to set up a uniform field across the effective area of the AUT. The cross-polar discrimination afforded by the linearly-polarized wave can be proven by transmitting between a pair of standard-gain horn antennas or open-ended waveguides as test antennas, and checking that the combination of site error and inherent cross-polar performance with the test antennas yields a suppression of the horizontal component by more than 30 dB. If the site errors are very low, and if the test antennas have identical performance, the cross-polar rejection of one test antenna is approximately 6 dB lower than the combined cross-polar coupling of the pair of test antennas. For example, if the combined cross-polar level is 30 dB, then the level for a single test antenna is 36 dB. The criterion for the site set-up, including antenna separation and site performance, is the achievement of a combined cross-polar level of 30 dB. A pair of horn antennas can be set up, horizontally polarized, with a separation between their front apertures of 1,5 m. The site insertion loss (SIL) is recorded over the frequency range of interest. One of the antennas is rotated by 90° so that it is vertically polarized. The change in SIL of at least 30 dB will provide acceptable measurement uncertainty. For frequencies below 1 GHz, V-shaped LPDA antennas can be used in place of horn antennas to prove the suitability of the site. It is possible to use dipole or biconical antennas, but due to their uniform H-plane radiation patterns a greater antenna height would be needed.

An interfering signal 20 dB lower in level than the desired signal gives a maximum error on the desired signal of $\pm 0,9$ dB. The maximum error occurs when the cross-polar signal is in phase with the co-polar signal. If the XPR of the LPDA is worse than 20 dB, the operator shall calculate the uncertainty and declare it with the result. For example, a cross-polar level of 14 dB implies a maximum uncertainty of +1,6 dB to -1,9 dB; the larger value and an assumed rectangular distribution shall be used when calculating the standard uncertainty.

To add a signal of 0 dB to another of -14 dB, first convert to relative voltages by dividing by 20 and taking the anti-logarithm. Then add the smaller signal to the unity signal. Take the logarithm and multiply by 20. The result is the positive decibel error. Repeat, but subtract the smaller signal from the unity signal to give the negative decibel error.

For the purpose of calculating the uncertainty of a radiated disturbance measurement, if the signal level measured in one polarization exceeds the signal measured in the orthogonal polarization by 6 dB or more, then an LPDA whose XPR is only 14 dB will have been deemed to have met the specification of 20 dB. If the difference between the vertically and horizontally polarized signal levels is less than 6 dB, additional uncertainty shall be calculated if the sum of this difference and the XPR is less than 20 dB.

Considerations on measurement uncertainty for XPR measurement results can be found in Annex H. ~~Text deleted~~ Annex H provides an example of an XPR of an AUT sufficient to meet the 20 dB XPR requirement in the measurement.

4.6 Antennas for the frequency range 1 GHz to 18 GHz

4.6.1 General

Radiated disturbance measurements above 1 GHz shall be made using calibrated linearly polarized antennas. Examples are LPDA antennas, double-ridged guide horn antennas, and standard gain horn antennas. The "beam" or main lobe of the pattern of any antenna used shall be wide enough to encompass the EUT when located at the measuring distance. The width of the main lobe is defined as the 3 dB beamwidth of the antenna, and information allowing determination of this parameter should be given in the antenna documentation. For horn antennas, the following condition shall be satisfied:

$$d \geq \frac{D^2}{2\lambda} \quad (5)$$

where

- d is the measurement distance (m);
 D is the largest dimension of the aperture of the antenna (m); and
 λ is the free space wavelength at the frequency of measurement (m).

The requirement for the XPR of the antenna in 4.5.5 also applies for the 1 GHz to 18 GHz frequency range.

4.6.2 Receive antenna

4.6.2.1 General

The receive antenna shall be linearly polarized and for site validation be the same type as used for EUT disturbance measurements.

Some antenna models may have different versions with possibly different radiation patterns, and users are advised to verify the preceding condition.

NOTE 1 "Antenna type" means a shape or a kind of antenna, for example horn antenna or LPDA antenna.

NOTE 2 "Antenna model" means the specified manufacturer's model number.

NOTE 3 "Version" means the specified manufacturer's revision number, if applicable, of a particular antenna model number.

4.6.2.2 Receive antenna radiation pattern

E-plane and H-plane radiation patterns shall be measured with reference to the antenna boresight. The measurand is the antenna pattern in dB, presented using a polar-coordinate plot such as in Figure 2. Radiation pattern plots should be normalized to 0 dB. The 0° angle shall be equal to the mechanical boresight.

E-plane and H-plane radiation patterns of each individual antenna shall be recorded over the frequency range of the antenna with a step size of 500 MHz or less, per Annex I of CISPR 16-1-6:2014/AMD1:2016.

Type-test results, including statistical data, supplied by the manufacturer may be used to provide evidence that the receive antenna radiation pattern requirements are met. Service measures shall be taken to assure pattern stability during the antenna life.

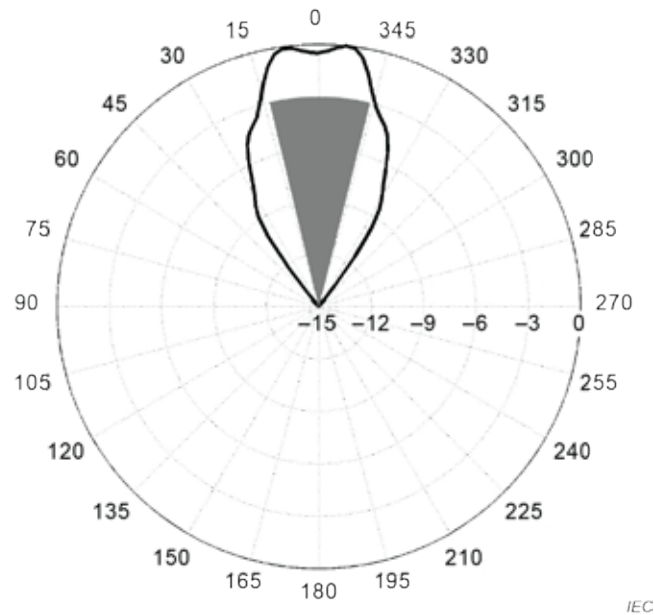


Figure 2 – RX antenna E-plane radiation pattern example, with limit area shaded for 3 m distance and 2 m EUT width

NOTE In general, the boresight direction is the direction of maximum radiation from the antenna. However, it may happen that the pattern has two radiation maxima but with none of the maxima in the direction of the mechanical boresight, e.g. as in Figure 2.

4.6.2.3 Receive antenna radiation pattern requirements

The grey-shaded areas shown in the polar plots of Figure 3 and Figure 4 are defined by the maximum height, h , and the maximum width, w , of the EUT, and the test distance, d .

For the receive antenna to sufficiently illuminate the EUT, the half-power beamwidth of the receive antenna shall not fall inside the shaded area in the E-plane and H-plane pattern cuts shown in Figure 3 and Figure 4.

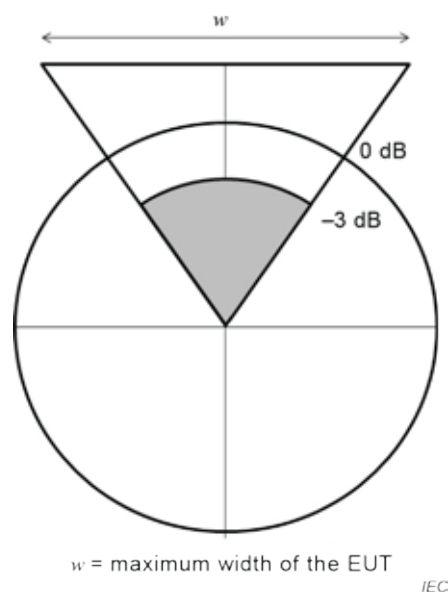


Figure 3 – Determination of maximum useable EUT width using half-power beamwidth

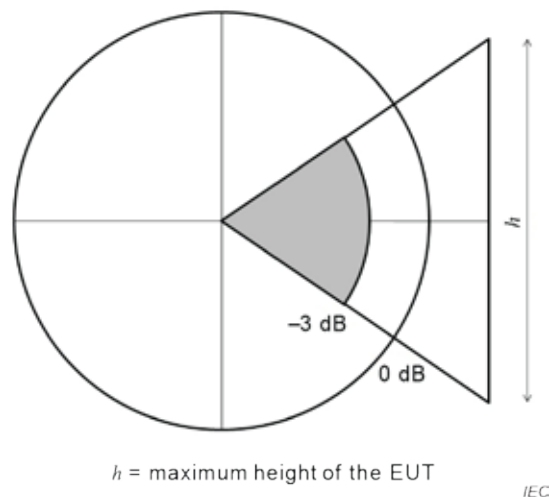


Figure 4 – Determination of maximum useable EUT height using half-power beamwidth

4.7 Special antenna arrangements – large-loop antenna system

In the frequency range 9 kHz to 30 MHz, the interference capability of the magnetic field component of the radiation of a single EUT can be determined by using a large-loop antenna system (LLAS). In the LLAS, the interference capability is measured in terms of the currents induced by the magnetic field in each LLA of the LLAS. The LLAS measures the current induced by the magnetic field component of a single EUT. The LLAS allows indoor measurements.

The LLAS consists of three circular mutually-perpendicular large-loop antennas, each having a diameter of 2 m, supported by a non-metallic base. A full description of the LLAS is given in Annex C.

[A1] The EUT shall be positioned in the centre of the LLAS on a non-conductive support table. **[A1]** The maximum dimensions of the EUT are limited so that the distance between the EUT and each LLAS loop is at least 0,20 m. **[A1]** Guidelines for routing of EUT cables are given in C.3 and Figure C.6. **[A1]** Cables shall be routed together, leave the LLAS volume in the same octant of the LLAS, and be no closer than 0,4 m to any of the LLAS loops.

[A1] The LLAS may be placed in any environment. Placement inside a shielded room, SAC, FAR, or weather-protected OATS is permitted. Placement in a shielded environment is recommended to eliminate ambient signals allowing for better sensitivity to EUT emissions. A minimum distance of 0,5 m between the LLAS and any metallic plane is recommended. The validation of the LLAS shall be performed at the location where the LLAS measurements normally take place to take into account the effect of the environment (see C.4). **[A1]**

The three mutually-perpendicular LLAS loops allow measurement of the interference capability of all polarizations of the radiated field with the prescribed accuracy, and without rotation of the EUT or changing the orientation of the LLAS loops.

Each of the three LLAS loops shall comply with the validation requirements given in C.4.

NOTE Circular LLAS loops with diameters different from the standard diameter of 2 m can be used, provided their diameter $D \leq 4$ m, and the distance in metres between the EUT and an LLAS loop is at least $0,10 \times D$. **[A1]** Conversion factors **[A1]** for non-standard diameters are given in C.6.

5 Test sites for measurement of radio disturbance field strength for the frequency range of 9 kHz to 30 MHz

(Void)

6 Test sites for measurement of radio disturbance field strength for the frequency range of 30 MHz to 1 000 MHz

6.1 General

An environment is required that assures valid, reproducible measurement results of disturbance field strength from an EUT. For an EUT that can only be tested at its place of use, other provisions shall be utilized (i.e. see details on in-situ measurements in CISPR 16-2-3).

6.2 OATS

6.2.1 General

An OATS is an area characterized by cleared level terrain and with the presence of a conducting ground plane. To meet the validation requirements of this document, a metallic ground plane is recommended. Such a test site shall be free of buildings, electric lines, fences, trees, etc. and free from underground cables, pipelines, etc., except as required to supply and operate the EUT. Refer to Annex D for specific construction recommendations of an OATS for disturbance field-strength measurements in the range of 30 MHz to 1 000 MHz. The site validation procedures for an OATS are given in 6.6 and 6.7. Annex F explains the basis for the acceptability criterion.

6.2.2 Weather-protection enclosure

Weather protection is desirable if the test site is used throughout the year. A weather-protection structure can protect either the entire test site (including EUT and field-strength measuring antenna) or the EUT only. The materials used shall be RF-transparent, to preclude undesirable reflections and attenuation of the emitted field from the EUT (see 6.3.1).

The structure of a weather-protection enclosure shall be shaped to allow easy removal of snow, ice, or water. See Annex D for further details.

6.2.3 Obstruction-free area

For open-area test sites, an obstruction-free area surrounding the EUT and field-strength measuring antenna is required. The obstruction-free area shall be free from significant scatterers of electromagnetic fields, and shall be large enough so that scatterers outside the obstruction-free area will have little effect on the fields measured by the field-strength measuring antenna. To determine the adequacy of an obstruction-free area, site validation tests shall be performed.

Because the magnitude of the field scattered from an object depends on many factors (size of the object, distance from the EUT, orientation with respect to the EUT, conductivity and permittivity of the object, frequency, etc.), it is impractical to specify a reasonable obstruction-free area that is necessary and sufficient for all applications. The size and shape of the obstruction-free area are dependent upon the measurement distance, and whether or not the EUT will be rotated. If the site is equipped with a turntable, the recommended obstruction-free area is an ellipse with the receive antenna and EUT at the two foci, with a major axis equal to twice the measurement distance and a minor axis equal to the product of the measurement distance and $\sqrt{3}$ (see Figure 5).

For this ellipse, the length of the path taken by the undesired indirect ray reflected from any object on the perimeter is twice the length of the path taken by the direct ray between the foci.

If a large EUT is installed on the turntable, the obstruction-free area shall be expanded so that the obstruction clearance distances are established relative to the perimeter of the EUT.

If the site is not equipped with a turntable, i.e. the EUT is stationary, the recommended obstruction-free area is a circular area such that the radial distance from the boundary of the EUT to the boundary of the area is greater than or equal to the measurement distance multiplied by 1,5 (see Figure 6). In this case, the antenna is moved around the EUT at the measurement distance.

The terrain within the obstruction-free area shall be flat. Small slopes needed for adequate drainage are acceptable. The flatness of the metallic ground plane, if used, is discussed in D.2. Measuring apparatus and all personnel shall be situated outside the obstruction-free area.

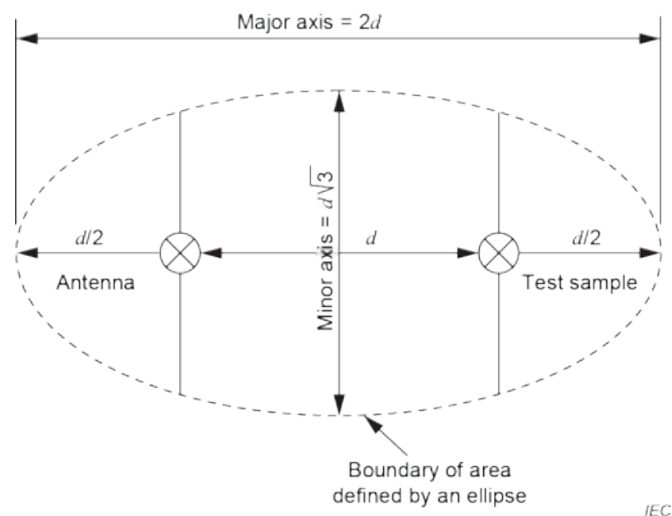


Figure 5 – Obstruction-free area of a test site with a turntable

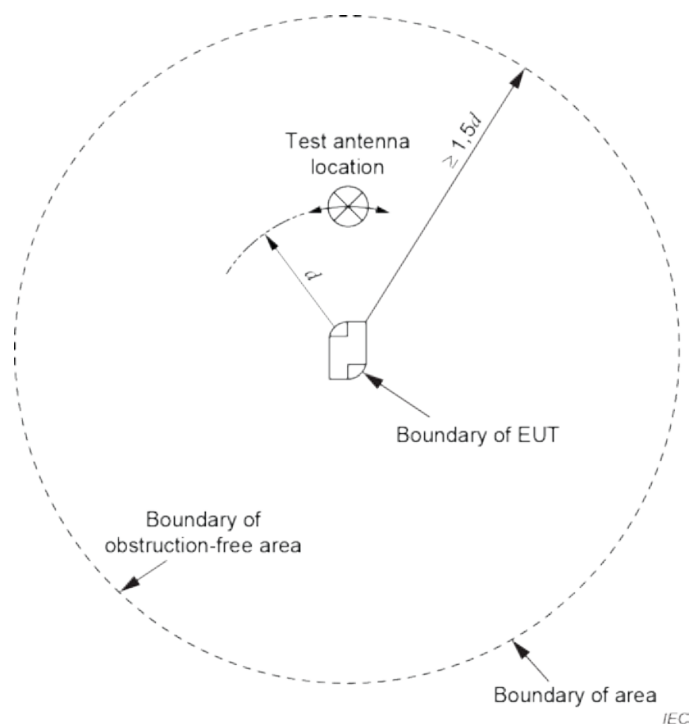


Figure 6 – Obstruction-free area with stationary EUT

6.2.4 Radio-frequency ambient environment of a test site

The radio-frequency ambient levels at an OATS shall be sufficiently low compared to the levels of the disturbance measurements to be performed. The quality of the site for this condition may be evaluated under four categories, listed as follows in order of merit:

- a) the ambient emissions are 6 dB or more below the measurement levels;
- b) some ambient emissions are within 6 dB of the measurement levels;
- c) some ambient emissions are above the measurement levels, but are either aperiodic (i.e. sufficiently long in time between transmissions to allow a measurement to be made) or continuous, but only on limited identifiable frequencies;
- d) the ambient levels are above the measurement levels over a large portion of the measurement frequency range and occurring continuously.

The selection of a test site should ensure that the accuracy of the measurement is maintained, given the ambient environment and the degree of engineering skill available.

In addition to the RF ambient environment, the receiver intrinsic noise floor contributes to the uncertainty of the results of radiated disturbance measurements. Hence both the RF ambient emissions and the receiver intrinsic noise shall be minimized, to allow a valid comparison of the measured disturbance level with the disturbance limit.

6.2.5 Ground plane

The OATS ground plane can be at earth level, or elevated on a suitably-sized platform or horizontal rooftop site. A metal ground plane is preferred, but for certain equipment and applications, product publications may recommend other site types. Adequacy of the metal ground plane will be dependent on whether the test site meets the site validation requirements of 6.4. If metallic material is not used for the ground plane, caution is required to select a site that does not change its reflective characteristics with time, weather conditions, or effects due to buried metallic material, such as pipes, conduits, and non-homogeneous soil. Such sites generally give different SA characteristics compared to those with metallic surfaces.

6.3 Suitability of other test sites

6.3.1 Other ground-plane test sites

There are many different test sites and facilities that have been constructed and used to make radiated disturbance measurements. Most are protected from the weather and the adverse effects of the RF ambient. For example in a SAC, all walls and the ceiling are equipped with appropriate RF absorbing material, while the floor consists of a metallic ground plane to emulate an OATS. A SAC isolates the receive antenna from the ambient RF environment, and permits EUT testing independent of weather conditions.

Whenever construction material encloses a ground-plane test site, it is possible that the results of a validation measurement at a single location, as specified in 6.7, are not adequate to show acceptability of such an alternative site.

Therefore to evaluate suitability of an alternative ground-plane test site, the procedure of 6.8 shall be used, which is based on making validation measurements at multiple positions throughout a volume occupied by the EUT. For a site to be judged suitable as an equivalent to an OATS, the results of these validation measurements shall all be within a tolerance of ± 4 dB.

NOTE SACs typically meet site quality category a) in 6.2.4.

6.3.2 Test sites without ground plane (FAR)

A fully-absorber-lined shielded enclosure, also known as a fully-anechoic room (FAR), can be used for radiated disturbance measurements. When a FAR site is used, appropriate radiated disturbance limits shall be defined in relevant standards (generic, product, or product family standards). Compliance of an EUT with the requirements for the protection of radio-services (i.e. limits) shall be evaluated at FAR sites using similar methods as with measurements done at an OATS.

A FAR is intended to simulate a free-space environment, such that only the direct ray from the transmit antenna or EUT reaches the receive antenna. All indirect and reflected ray waves shall be minimized by appropriate placement of RF absorbing material on all walls, ceiling, and floor of a FAR. Like a SAC, a FAR isolates the receive antenna from the RF ambient environment, and permits EUT testing independent of weather conditions.

NOTE FARs typically meet site quality category a) in 6.2.4.

6.4 Test site validations

6.4.1 General

Three methods for site validation of a COMTS may be used for the purposes of this document:

- NSA method with tuned dipoles;
- NSA method with broadband antennas;
- Reference site method (RSM) with broadband antennas.

The NSA method with tuned dipoles is not specifically described, but it may be used for the purposes of this document. Theoretical NSA tables for tuned dipoles, including tables of the theoretical mutual impedance correction factors, are given in [20]¹.

Validations for test sites with a ground plane (i.e. OATS and SAC) are introduced in 6.4.2 and 6.5.1, followed by detailed procedures for the RSM in 6.6 and for the NSA method in 6.7. Validation of a SAC and a weather-protection enclosed OATS requires additional measurements as described in 6.8.

Table 1 summarizes the site validation methods applicable for these specific test site types. As shown in this table, two or three site validation methods are described for each of these test site types. These methods are deemed to be equivalent for the purposes of this document; meaning compliance with the validation criterion can be evaluated using only one method. Furthermore, no one of these documented methods is defined as the reference method.

The site validation methods in this document provide a measure of uniformity of the validated test volume using a comparison between ideal (theoretical) and measured site attenuation between the transmit antenna and the receive antenna. The transmit antenna does not simulate the EUT; therefore, the validation procedure does not define the maximum EUT volume. Considerations on EUT sizes depending on measurement distance are given in CISPR 16-2-3.

¹ Numbers in square brackets refer to the bibliography.

Table 1 – Site validation methods applicable for OATS, OATS-based, SAC, and FAR site types

Test site type	Applicability of site validation methods		
	Tuned dipoles NSA	Broadband antennas NSA	Broadband antennas RSM
OATS	Yes	Yes	Yes
OATS with weather protection	No	Yes	Yes
SAC	No	Yes	Yes
FAR	No	Yes	Yes

6.4.2 Overview of test site validations

The validation of a test site is performed using two co-polarized antennas. The validation shall be performed separately for both horizontal and vertical polarizations.

SA is obtained from the difference of:

- the source voltage level, V_i , applied to a transmit antenna;
- the maximum received voltage level, V_R , measured on the terminals of a receive antenna during a specified antenna height scan.

The voltage measurements are performed in a 50 Ω system.

The measured SA of an OATS (as in 6.2) and other ground-plane test sites (as in 6.3.1) is compared to the SA characteristics obtained at an ideal OATS – this is the definition of the measurand for test site validations. The result of this comparison is the SA deviation, ΔA_s , in dB; see Equation (6) and Equation (7). The site is considered suitable when the SA deviation results are within a tolerance of ± 4 dB.

If the ± 4 dB tolerance is exceeded, the test site configuration shall be investigated as described in 6.9.

NOTE The basis for the ± 4 dB site acceptability criterion is given in Annex F.

Additionally, SA deviations shall not be used to correct field-strength measurement data for an EUT. The procedures of 6.4 shall be used only for test site validations.

6.5 Basic parameters of the NSA method for OATS and SAC

6.5.1 General equation and table of theoretical NSA values

NSA values calculated at specific frequencies are provided in Table 2 for broadband antennas. The quantities d , h_1 , h_2 , f_M , and A_N used are identified at the end of Table 2.

NOTE 1 NSA values for frequencies other than shown in Table 2 can be obtained using linear interpolation between the tabulated values.

NOTE 2 The spacing d between LPDA antenna pairs is measured from the projection on the ground plane of the mid-point of the longitudinal axis of each antenna.

NOTE 3 The spacing d between biconical antennas is measured from the element centreline axes at the feedpoint.

For measurements in each polarization, the NSA method requires two different measurements of the received voltage, V_R .

The first reading of V_R (V_{DIRECT}) is taken with the two coaxial cables disconnected from the two antennas and connected to each other via an adaptor. The second reading of V_R (V_{SITE}) is taken with the coaxial cables reconnected to their respective antennas, then the maximum signal is measured when the receive antenna is scanned in height (1 m to 4 m, for 3 m, 5 m 10 m and 30 m separation distances). For both measurements, the signal source voltage, V_i , is kept constant. The measured results, along with the theoretical NSA (A_N), are used in Equation (6) to obtain the SA deviation results. All terms are in dB.

$$\Delta A_s = V_{\text{DIRECT}} - V_{\text{SITE}} - F_{aT} - F_{aR} - A_N \quad (6)$$

where

ΔA_s is the SA deviation;
 F_{aT} is the transmit antenna factor;
 F_{aR} is the receive antenna factor;
 A_N is the theoretical NSA, according to Table 2.

F_{aT} and F_{aR} shall be calibrated as free-space antenna factors; see 6.5.2.

Note that the first two terms represent the actual measurement of SA, i.e. in the classical view SA is equal to ($V_{\text{DIRECT}} - V_{\text{SITE}}$), which is the insertion loss of the propagation path with the inclusion of the properties of the two antennas used.

To confirm the absence of voltage drift due to temperature changes in measurement devices or cables, re-measure V_{DIRECT} after a suitable time period to confirm stability of the results.

For the respective NSA measurement method used (swept frequency method per 6.7.2, or discrete frequency method per 6.7.1), the validation criterion shall be satisfied at all frequencies in the desired frequency range.

Table 2 lists NSA values for broadband antennas, such as biconical and LPDA, for both horizontal and vertical polarizations relative to the ground plane.

If ΔA_s is greater than ± 4 dB, proceed as described in 6.9.

Table 2 – Theoretical normalized site attenuation, A_N –

Polariza- tion		Horizontal										Vertical											
		3	3	5	5	5	10	10	10	10	30	30	3	3	5	5	5	10	10	10	10	30	30
d	m	1	2	1	2	2,5	1	2	3	4	1	2	1	1,5	1	1,5	2,0	1	1,5	2,5	3,5	1	1,5
h_1	m	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
$h_{2,min}$	m	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	
f_M	MHz	A_N																					
		dB(m ²)																					
30		15,8	11,0	20,7	15,6	14,3	29,8	24,1	21,3	19,7	47,8	41,7	8,2	9,3	11,4	12,0	12,7	16,7	16,9	17,4	18,2	26,0	26,0
35		13,4	8,8	18,2	13,3	12,2	27,1	21,6	18,9	17,4	45,1	39,1	6,9	8,0	10,1	10,7	11,5	15,4	15,6	16,1	16,9	24,7	24,7
40		11,3	7,0	16,0	11,4	10,5	24,9	19,4	16,9	15,6	42,8	36,8	5,8	7,0	8,9	9,6	10,4	14,2	14,4	15,0	15,8	23,5	23,5
45		9,4	5,5	14,1	9,8	9,1	22,9	17,5	15,2	14,2	40,8	34,7	4,9	6,1	7,9	8,6	9,5	13,2	13,4	14,0	14,9	22,5	22,5
50		7,8	4,2	12,4	8,5	7,9	21,1	15,9	13,7	13,1	38,9	32,9	4,0	5,4	7,1	7,8	8,7	12,3	12,5	13,2	14,1	21,6	21,6
60		5,0	2,2	9,5	6,3	6,0	18,0	13,1	11,5	11,3	35,8	29,8	2,6	4,1	5,6	6,3	7,4	10,7	11,0	11,7	12,7	20	20
70		2,8	0,6	7,2	4,6	4,4	15,5	10,9	9,9	9,9	33,1	27,2	1,5	3,2	4,3	5,2	6,4	9,4	9,7	10,5	11,7	18,7	18,7
80		0,9	-0,7	5,3	3,2	3,2	13,3	9,2	8,6	8,7	30,8	24,9	0,6	2,6	3,3	4,3	5,6	8,3	8,6	9,5	10,9	17,5	17,5
90		-0,7	-1,8	3,7	2,0	2,1	11,4	7,8	7,5	7,7	28,8	23,0	-0,1	2,1	2,4	3,5	5,1	7,3	7,6	8,7	10,2	16,5	16,5
100		-2,0	-2,8	2,3	1,0	1,1	9,7	6,7	6,6	6,7	27	21,2	-0,7	1,9	1,6	2,9	4,7	6,4	6,8	8,0	9,6	15,6	15,6
120		-4,2	-4,4	0,1	-0,7	-0,5	7,0	5,0	4,9	5,1	23,9	18,2	-1,5	1,3	0,3	2,1	3,4	4,9	5,4	7,0	6,8	14,0	14,0
140		-6,0	-5,8	-1,7	-2,1	-1,9	4,8	3,5	3,5	3,8	21,2	15,8	-1,8	-1,5	-0,6	1,7	1,0	3,7	4,3	6,2	5,2	12,7	12,7
160		-7,4	-6,7	-3,1	-3,3	-3,1	3,1	2,3	2,4	2,6	19	13,8	-1,7	-3,7	-1,3	1,0	-0,7	2,6	3,4	4,1	3,9	11,5	11,6
180		-8,6	-7,2	-4,3	-4,4	-4,1	1,7	1,2	1,3	1,6	17	12,0	-1,3	-5,3	-1,8	-1,0	-2,2	1,8	2,7	2,8	2,8	10,5	10,6
200		-9,6	-8,4	-5,3	-5,3	-4,7	0,6	0,3	0,4	0,6	15,3	10,6	-3,6	-6,7	-2,0	-2,6	-3,3	1,0	2,1	1,6	1,7	9,6	9,7
250		-11,7	-10,6	-7,5	-6,7	-6,7	-1,6	-1,7	-1,6	-1,2	11,6	7,8	-7,7	-9,1	-3,2	-5,5	-5,6	-0,5	0,3	-0,6	-0,3	7,7	7,9

Table 2 (2 of 2)

Polariza- tion	Horizontal										Vertical									
	3	3	5	5	5	10	10	10	10	30	3	3	5	5	5	10	10	10	10	30
d m	3	3	5	5	5	10	10	10	10	30	3	3	5	5	5	10	10	10	10	30
h_1 m	1	2	1	2	2,5	1	2	3	4	1	2	1	1,5	1	2,0	1	1,5	2,5	3,5	1
$h_{2,min}$ m	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
$h_{2,max}$ m	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4
f_M MHz	A_N dB(m ²)																			
300	-12,8	-12,3	-9,2	-8,5	-8,4	-3,3	-3,3	-3,0	-2,8	8,8	6,1	-10,5	-10,9	-6,2	-7,5	-7,3	-1,5	-2,4	-1,9	6,2
400	-14,8	-14,9	-11,8	-11,2	-11,0	-5,9	-5,8	-5,6	-5,4	4,6	3,5	-14,0	-12,6	-10,0	-10,5	-10,0	-4,1	-5,0	-5,1	3,9
500	-17,3	-16,7	-13,0	-13,3	-13,0	-7,9	-7,6	-7,6	-7,3	1,8	1,6	-16,4	-15,1	-12,5	-12,6	-11,6	-6,7	-7,2	-7,1	2,1
600	-19,1	-18,3	-14,9	-14,9	-14,5	-9,5	-9,3	-9,2	-8,9	0,0	0,0	-16,3	-16,9	-14,4	-13,5	-13,4	-8,7	-9,0	-8,7	0,8
700	-20,6	-19,7	-16,4	-16,1	-15,9	-10,8	-10,6	-10,5	-10,2	-1,3	-1,4	-18,4	-18,4	-15,9	-15,1	-14,8	-10,2	-10,4	-9,9	-0,3
800	-21,3	-20,8	-17,6	-17,3	-17,1	-12,0	-11,8	-11,6	-11,4	-2,5	-2,5	-20,0	-19,3	-17,2	-16,5	-16,0	-11,5	-11,6	-11,1	-2,3
900	-22,5	-21,8	-18,7	-18,4	-18,0	-12,8	-12,9	-12,7	-12,4	-3,5	-3,5	-21,3	-20,4	-17,4	-17,6	-16,9	-12,6	-12,7	-12,1	-3,4
1 000	-23,5	-22,7	-19,7	-19,3	-19,0	-13,8	-13,8	-13,6	-13,6	-4,4	-4,5	-22,4	-21,4	-18,5	-18,6	-17,9	-13,6	-13,1	-12,4	-4,3
^a These data apply to antennas that have at least 25 cm of ground plane clearance when the centre of the antennas is 1 m above the ground plane in vertical polarization. Values at other frequencies are found via linear interpolation.																				
d	is the horizontal separation between the projection of the transmit antenna and receive antenna midpoints on the ground plane;																			
h_1	is the height of the centre of the transmit antenna above the ground plane;																			
h_2	is the range of heights of the centre of the receive antenna above the ground plane. The maximum received signal in this height scan range is used for NSA results;																			
f_M	is the frequency;																			
A_N	is the NSA.																			

6.5.2 Antenna calibration

For site validation using the NSA method, free-space antenna factors are used, as measured with the methods of CISPR 16-1-6.

The use of free-space antenna factors for the calculation of NSA, as in Equation (6), can cause errors, particularly for biconical and tuned dipole antennas below 300 MHz. This is because the model for the theoretical NSA values in Table 2 is based on a Hertzian dipole and not on the actual antennas used to measure SA. This model does not take account of the significant change in antenna factor due to mutual coupling to the ground plane, or account of the radiation pattern of the antenna. This problem does not occur with the RSM because it does not involve antenna factors. A partial solution is available in [19] which significantly reduces uncertainties of the antenna factors in the NSA method.

6.6 Reference site method for OATS and SAC

6.6.1 General

The RSM is another method for validating the suitability of a test site, using broadband antennas. As with the NSA method, the evaluation of V_{DIRECT} and V_{SITE} is required. These results are obtained using exactly the same geometries and polarizations as specified for the NSA method. For a weather-protection-enclosed OATS or a SAC, the configurations are:

- 3 m, 5 m, or 10 m test distance;

NOTE 1 Although RSM may be applied to 30 m sites, it is impractical due to the limited number of appropriate reference test sites.

- transmit antenna heights are 1 m and 2 m for horizontal polarization, and 1 m and 1,5 m for vertical polarization;

NOTE 2 For other transmit antenna heights, see Table 2.

- 1 m to 4 m receive antenna height scan range.

The main difference between the RSM and NSA methods is in the calculation of SA deviations, using Equation (7):

$$\Delta A_s = V_{\text{DIRECT}} - V_{\text{SITE}} - A_{\text{APR}} \quad (7)$$

Rather than using antenna factors for the transmit antenna and the receive antenna and the calculated NSA (A_N) values, as in the NSA method Equation (6), measured results for the antenna-pair reference SA (A_{APR}) are used.

NOTE 3 A_{APR} does not involve antenna factors, but comprises coupling between the antennas, including the effects of coupling of each antenna to the ground. Furthermore, the radiation patterns of the antennas are included, different from the NSA method where the radiation patterns are approximated as being those of Hertzian dipoles.

For a weather-protection enclosed OATS and a SAC, four data sets are required, i.e. two antenna heights with two polarizations. For each additional distance, polarization and antenna height, a different A_{APR} is needed, as shown in the example template of Table 3.

Table 3 – Example template for A_{APR} data sets

Frequency MHz	Antenna pair reference site attenuation, A_{APR} dB			
	Horizontal		Vertical	
	$h_1 = 1$ m	$h_1 = 2$ m	$h_1 = 1$ m	$h_1 = 1,5$ m
30	...	...	...	...
31	...	...	...	...
32	...	...	...	...
...	...	...	...	...

When using a network analyzer or a stepped-frequency receiver to perform an RSM measurement, the frequency steps of Table 4 shall be used.

NOTE 4 RSM is a swept frequency method; Table 4 defines the maximum step size.

NOTE 5 When using a continuously-tuned receiver or a spectrum analyzer for an RSM measurement, the frequency step size definition of Table 4 does not apply.

Table 4 – RSM frequency steps

Frequency range MHz	Maximum frequency step size MHz
30 to 100	1
100 to 500	5
500 to 1 000	10

Frequencies used for the RSM measurement of a test site shall be identical to the frequencies used to obtain the A_{APR} data (e.g. at a REFTS; see 6.6.3).

The ΔA_s criterion, see Equation (7), shall be satisfied at the frequencies given in Table 4.

6.6.2 Antennas not permitted for RSM measurements

For the purposes of this document, hybrid antennas shall not be used for RSM site validation measurements.

NOTE 1 When specific SAC sites are validated using biconical and hybrid antennas, a large deviation in the results has been observed. The main reason for deviations is the different distance between the phase centres of the antennas, e.g. 10 m for biconical antennas and approximately 11,2 m for typical hybrid antennas. To avoid such reproducibility issues, hybrid antennas are excluded.

NOTE 2 Hybrid antennas typically are not used for site validation because of the larger uncertainties in positioning of these typically larger and bulkier antennas, especially for a 3 m test site where the overall combined length of the two hybrid antennas may be nearly 3 m.

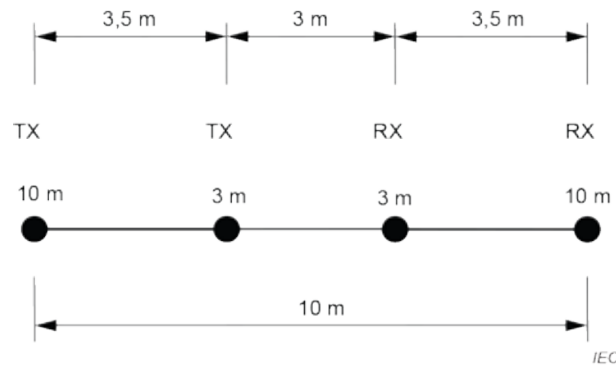
NOTE 3 Better performance for a SAC is typically obtained with standard antennas (biconical or LPDA) for a lower ΔA_s ; adjustment of SAC design parameters to achieve site validation compliance using hybrid antennas is strongly discouraged. To construct a SAC with better performance than those required, the standard requires the manufacturer to fulfil e.g. $\Delta A_s = 3,5$ dB.

6.6.3 Determination of the antenna pair reference site attenuation on a REFTS

One approach to measuring A_{APR} is to use a reference test site (REFTS), which has performance established according to procedures described in CISPR 16-1-5. A separate second approach is given in 6.6.4.

For a test distance of 10 m, identical positions on the REFTS shall be used to determine A_{APR} as were used for the REFTS validation according to CISPR 16-1-5 procedures.

For a test distance of 3 m, measurements shall be made on the axis drawn between the transmit antenna and the receive antenna positions as were used for the REFTS validation according to CISPR 16-1-5 procedures (see Figure 7).



Key

TX = transmit antenna

RX = receive antenna

Figure 7 – Test point locations for 3 m and 10 m test distances

The following procedure shall be used to determine A_{APR} :

- determine V_{DIRECT} ;
- place the transmit antenna in horizontal polarization at a height of 1 m;
- place the receive antenna in the same polarization at a distance d ;
- determine V_{SITE} during the 1 m to 4 m height scan of the receive antenna;
- calculate A_{APR} as follows using Equation (8):

$$A_{APR} = V_{DIRECT} - V_{SITE} \quad (8)$$

- repeat steps b) to e) for transmit antenna height of 2 m with horizontal polarization, and then for transmit heights of 1 m and 1,5 m with vertical polarization.

6.6.4 Determination of the antenna pair reference site attenuation using an averaging technique on a large OATS

Another method to determine A_{APR} is by measurements on a large OATS (see the following paragraphs in this subclause for the criteria to be large). Deviations of the SA from the ideal behavior are caused by the limited area and flatness of the ground plane, and reflections from objects in the near vicinity such as buildings and trees. Also, reflections from the edges of the ground plane can cause a sinusoidal ripple in the measured SA, predominantly for vertical polarization measurements. By varying the location of the antenna pair on the ground plane, the magnitude and the phase of the ripple will also change.

To minimize these effects, the SA is measured at several antenna pair positions, and an average value is calculated. This average value will converge to the SA of an ideal site.

NOTE 1 A similar technique is given in reference [19].

The large OATS shall meet the following requirements:

- minimum ground plane size of 30 m by 20 m;

- deviation from flatness less than ± 10 mm;
- without protective layer (dielectric) on the metal ground plane.

The following procedure shall be used to determine A_{APR} .

- a) Identify paired test points on the OATS, according to the scheme shown in Figure 8. All nine points for each antenna shall be located on the ground plane. If a weather-protection cover is present on the OATS, the minimum distance between any test point and any part of the cover shall be greater than 3 m. Measurement locations inside the cover are prohibited.

NOTE 2 It is advantageous that the local grid (coordinate system) be placed at some non-zero angle relative to the (straight) edges of the ground plane, likewise at some non-zero angle relative to welded seams. An example of such a layout is given in Figure 9.

Under the following conditions, the use of less than nine measurement positions (18 points) shall be allowed.

- 1) Where compliance was shown in the past:

If compliance with the standard deviation $s \leq 0,3$ dB criterion [see Equation (10)] was shown for at least one pair of antennas for each frequency subrange within the past 24 months, the following minimum numbers of antenna-pair measurement positions shall be allowed:

- one position (centre) for biconical antennas, in horizontal polarization;
- three positions (centre, plus two other positions) for biconical antennas, in vertical polarization;
- one position (centre) for LPDA antennas, in both polarizations.

- 2) Where compliance can be shown with fewer points, if the compliance criterion is met with fewer than nine points it is permitted to use that number of points.

NOTE 3 For determining the most accurate A_{APR} , the use of all nine antenna-pair positions will improve the averaging result.

- b) Number the selected measurement positions from 1 to N ($N \leq 9$).
- c) Place the antennas at position 1.
- d) Measure $A_{APR,1}$ for all required heights and polarizations at all frequencies listed in Table 4.
- e) Repeat step d) for all other positions.
- f) Calculate the average of the measured $A_{APR,i}$ expressed in dB, using Equation (9):

$$A_{APR} = \frac{1}{N} \sum_{i=1}^N A_{APR,i} \quad (9)$$

- g) Calculate the standard deviation of the mean (i.e. of A_{APR}) in dB, using Equation (10):

$$s(A_{APR}) = \sqrt{\frac{1}{N(N-1)} \sum_{i=1}^N (A_{APR,i} - A_{APR})^2} \quad (10)$$

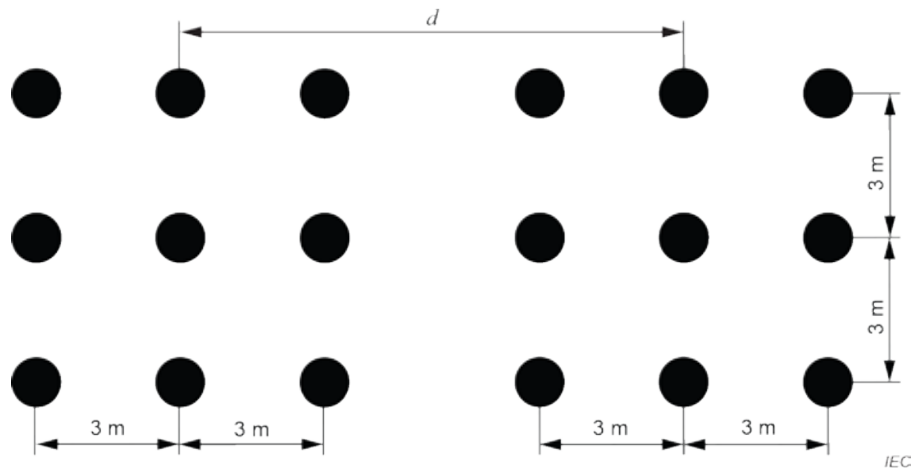
The calibrated A_{APR} values shall be deemed acceptable to use for subsequent COMTS validation if $s \leq 0,6$ dB at all measured frequencies.

If $N \geq 2$, Equation (10) shall be used to calculate the accuracy of $s(A_{APR})$ needed for an uncertainty calculation. If $N = 1$, $s = 0,6$ dB shall be assumed.

Special care shall be taken that no common offset (systematic effect) in the data for all selected positions is introduced. Such an effect could be due to influence of the antenna mast. For some antenna masts, a significant coupling between the metallic cover of the antenna

box and the antenna can occur. The magnitude of this influence shall be investigated by changing the distance between the antenna and the motor cover d_{Ant} (see Figure 10), and repeating A_{APR} measurements with these new configurations. This influence shall be included in the uncertainty calculation.

Another cause for a common offset can be reflections from the antenna cable. To minimize this influence, the cable shall be extended horizontally for at least 2 m behind the antenna before routing down to the ground. Clamp-on ferrites shall be used on the cables to reduce surface currents. This influence factor shall be included in the uncertainty calculation as well.



d is the distance between the projections of the two antenna reference points

Figure 8 – Paired test point locations for all test distances

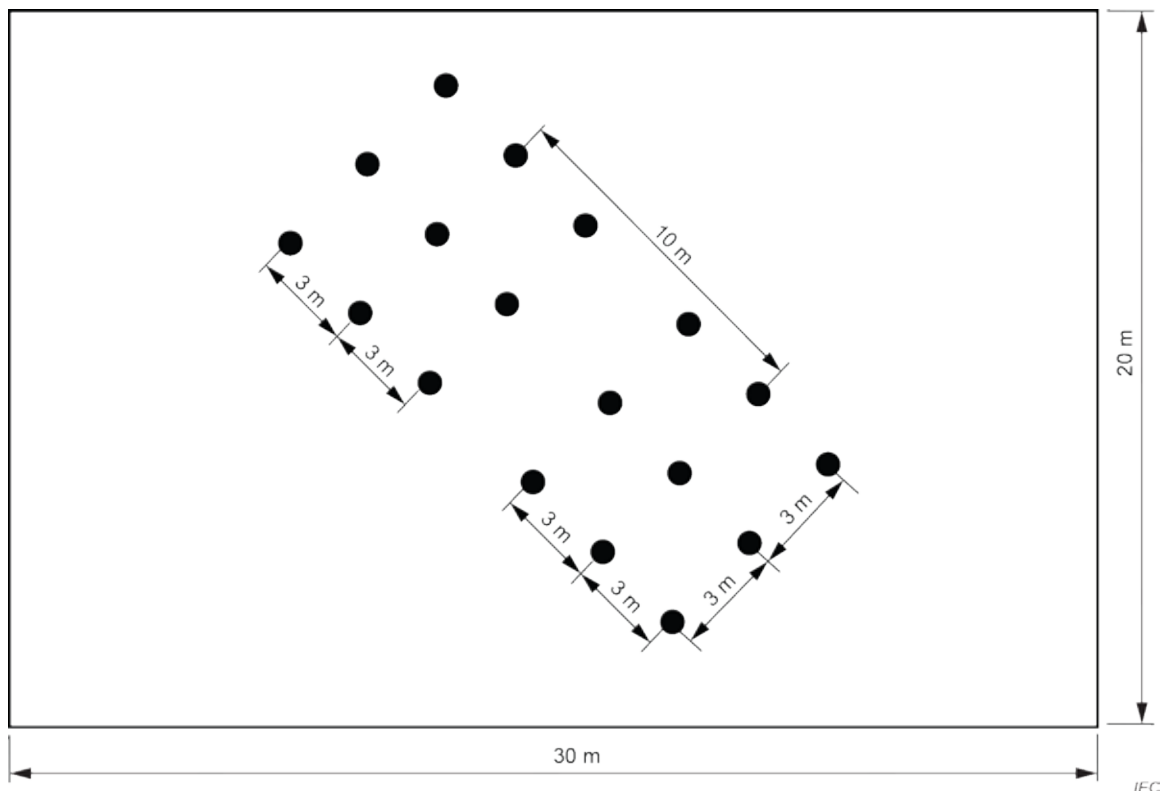


Figure 9 – Example of paired test point selection for a test distance of 10 m

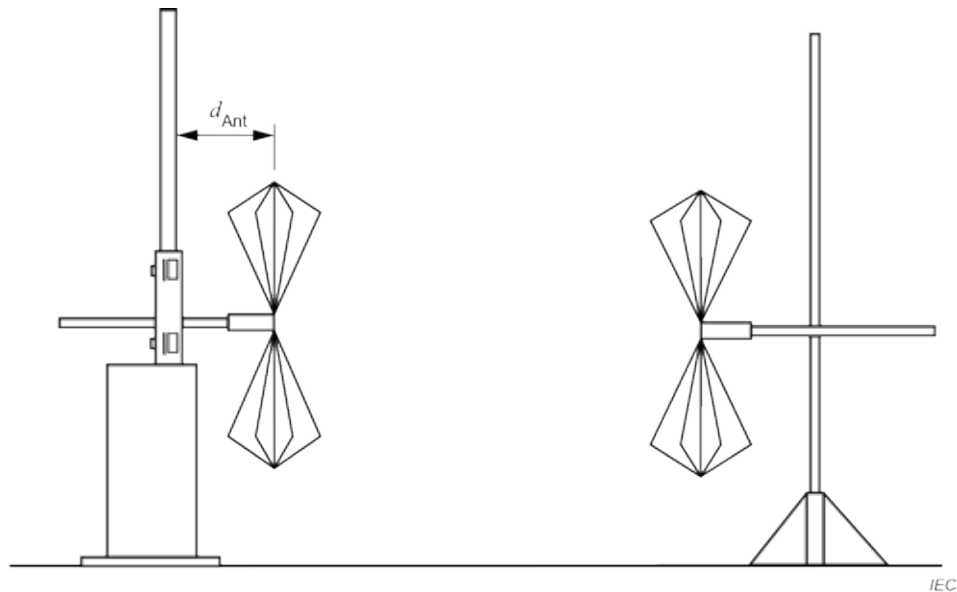


Figure 10 – Illustration of an investigation of influence of antenna mast on A_{APR}

6.7 Validation of an OATS by the NSA method

6.7.1 Discrete frequency method

6.7.1.1 Measurement set-up

Refer to Figure 11 and Figure 12 in 6.8 for specific test set-up details. The signal generator is connected to the transmit antenna with an appropriate length of cable. The transmit antenna is placed at the desired location. The transmit antenna height is set to h_1 (see Table 2 for the values of h_1) and the desired polarization is selected. For broadband antennas, the antenna heights shall be $h_1 = h_{2,min} = 1$ m.

The receive antenna is mounted on a mast that allows scanning over the height range $h_{2,min}$ to $h_{2,max}$, placed at a distance d from the transmit antenna, and connected to the measuring receiver or spectrum analyzer via a suitable length of cable. The same polarization as that for the transmit antenna is selected.

NOTE In contrast to the test set-up shown in Figure 11 and Figure 12, site validation of an OATS requires only a single site attenuation measurement.

6.7.1.2 Measurement procedure

The following steps shall be used for each frequency indicated in Table 2. The measurements are first made for antennas horizontally aligned and then for antennas vertically aligned with the transmit antenna height set at h_1 .

- Adjust the output level of the signal generator to give a received voltage display well above ambient and measuring receiver or spectrum analyzer noise.
- Raise the receive antenna on the mast through the h_2 scan range as specified in Table 2. Record the maximum signal level; this value is V_{SITE} for Equation (6) (see 6.5).
- Disconnect the cables from the transmit antenna and the receive antenna, then connect these cables directly together with a straight-through adaptor.
- Record the signal level with the transmit antenna and receive antenna cables connected. This value is V_{DIRECT} for Equation (6).
- At each frequency and for each polarization, enter the values from steps b) and d) in Equation (6).

- f) Insert the antenna factors of the transmit antenna and the receive antenna at the measurement frequency in Equation (6).
- g) Solve $A_s = V_{\text{DIRECT}} - V_{\text{SITE}} - F_{\text{aT}} - F_{\text{aR}}$ for A_s , which is the NSA for the measurement frequency and polarization used.
- h) Subtract the value in step g) from the appropriate theoretical NSA contained in Table 2, to obtain ΔA_s .
- i) If the ΔA_s results from step h) are less than ± 4 dB, the site is deemed to be acceptable at that frequency and polarization.
- j) Repeat steps a) through i) for the next frequency and polarization combination.

NOTE For NSA measurements, an impedance mismatch at the output of the signal source or at the input of the measuring receiver or spectrum analyzer can result in reflections which could cause errors. This can be avoided by use of attenuators of 10 dB, i.e. one at the transmit antenna and one at the receive antenna. If system sensitivity allows, these attenuators remain attached to the cables during the entire NSA measurement process.

6.7.2 Swept frequency method

6.7.2.1 Measurement set-up

The set-up is similar to that of 6.7.1, except that only broadband antennas are used. No restrictions on vertical polarization antenna height scan are necessary, due to the physically small size of such broadband antennas (compared to e.g. tuned dipoles). The antenna heights shall be $h_1 = h_{2,\text{min}} = 1$ m.

6.7.2.2 Measurement procedure

The following steps should be made using automatic measuring equipment having a peak hold ('max. hold'), storage capability, and tracking generator. In this method, both receive antenna height h_2 and frequency are scanned or swept over the required height and frequency ranges. The frequency ranges are usually determined by the type of broadband antenna used. The frequency sweep speed shall be much greater than the antenna height scan rate. Set the transmit antenna height to h_1 .

- a) Adjust the output level of the tracking generator to give a received voltage display well above ambient and scanning receiver or spectrum analyzer noise.
- b) Raise the receive antenna on the mast to the maximum height of the scan range, as specified in Table 2.
- c) Set the spectrum analyzer to sweep the desired frequency range. Ensure that the spectrum analyzer is adjusted so that a similar signal up to 60 dB higher can be displayed on the same amplitude scale. This will accommodate the levels to be recorded in step d).
- d) Slowly lower the receive antenna to the minimum height of the scan range, as specified in Table 2 for the appropriate site geometry. Store or record the maximum received voltage display V_{SITE} in dB(μ V). (The time it takes to lower the antenna should be much longer than the frequency sweep time.)
- e) Disconnect the cables from the transmit antenna and the receive antenna and connect them directly together with a straight-through adaptor. Store or record the resulting voltage display V_{DIRECT} in dB(μ V).
- f) At each frequency, subtract the voltage measured in step d) from the voltage measured in step e). Also subtract the antenna factors of the transmit antenna and the receive antenna, F_{aT} in dB(m⁻¹) and F_{aR} in dB(m⁻¹), respectively (antenna factors as a continuous function of frequency can be obtained by using simple linear curve fitting on a set of discrete antenna factor values). The result is the measured A_s over the range of frequencies used, which should be plotted. Also plot the theoretical NSA for an ideal site shown in Table 2.
- g) The differences ΔA_s found shall fall within the ± 4 dB criterion.

NOTE For NSA measurement methods, an impedance mismatch at the output of the signal source or at the input of the measuring receiver or spectrum analyzer may result in reflections which could cause errors. This can be avoided by use of padding attenuators of 10 dB, i.e. a 10 dB attenuator between each the transmit antenna connector and the receive antenna connector and the corresponding antenna cables. If system sensitivity allows, these attenuators typically remain attached to the cables during the entire NSA measurement process.

6.8 Validation of a weather-protection-enclosed OATS or a SAC

For an OATS with a weather-protection enclosure, or a SAC, a single site attenuation measurement is insufficient to pick up possible reflections from the construction materials and/or the RF-absorbing materials comprising the walls and ceiling of the facility. For these sites a "test volume" is defined as that volume traced out by the largest EUT or system to be tested as it is rotated about its centre location through 360°, such as by a turntable. Evaluating horizontal and vertical polarizations, such as illustrated in Figure 11 and Figure 12, may require a maximum of 20 separate SA measurements, i.e. five positions in the horizontal plane (centre, left, right, front, and rear, measured with respect to the centre and a line drawn from the centre to the position of the measuring antenna), for two polarizations (horizontal and vertical), and for two heights (1 m and 2 m for horizontal, 1 m and 1,5 m for vertical).

These measurements are performed with broadband antennas, and distances are measured with respect to the centres of the antennas. The transmit antenna and the receive antenna shall be aligned with the antenna elements parallel to each other, and orthogonal to the measurement axis.

For both horizontal and vertical polarizations, all antenna positions are at the periphery of the test volume, except for the centre position. As a guideline, the test volume should allow at least 25 cm between the antenna tip and the closest absorber tip, or at least 1 m between the antenna midpoint and the closest absorber tip. For vertical polarization, the lower tip of the antenna shall be greater than 25 cm from the floor, which may require the centre of the antenna to be slightly higher than 1 m for the lowest height measurement.

The number of required measurements can be reduced under the following conditions.

- a) The vertical and horizontal polarization measurements in the rear position may be omitted if the closest point of the construction and/or absorbing materials is at a distance greater than 1 m from the rear boundary of the test volume.

NOTE Radiated disturbance sources located near dielectric interfaces have been shown to have variations in current distribution that can affect the radiated properties of the source at that location. When an EUT can be located near these interfaces, additional SA measurements are necessary.

- b) The total number of horizontal polarization measurements along the test volume diameter joining the left and right positions may be reduced to the minimum number necessary for the antenna footprints to cover 90 % of the diameter.
- c) The vertical polarization measurements at the 1,5 m height may be omitted if the top of the EUT, including any mounting set-up table, is less than 1,5 m high.
- d) If the test volume is no larger than 1 m deep by 1,5 m wide by 1,5 m high, including a set-up table if used, horizontal polarization measurements need only be made at the centre, front and rear positions, but at both 1 m and 2 m heights. If the condition of item a) applies, the rear position may be omitted. This will require a minimum of eight measurements: four positions with vertical polarization (left, centre, right, and front) for one height, and four positions with horizontal polarization (centre and front) for two heights; see Figure 13 and Figure 14.

The receive antenna shall be re-positioned to maintain the appropriate separation along a line towards the turntable centre (see Figures 11, 12, 13 and 14). The test site is considered suitable for performing radiated disturbance measurement if all measurements prescribed above meet the requirements of 6.4.2.

If the test volume height h exceeds 2 m, two transmit antenna heights h_1 shall be used; i.e., $h_1 = 1$ m and $h_1 = h$ m for horizontal polarization, and $h_1 = 1$ m and $h_1 = (h - 0,5)$ m for vertical polarization. For example, if the test volume height $h = 3$ m, then the transmit antenna heights h_1 shall be 1 m and 3 m for horizontal polarization, and 1 m and 2,5 m for vertical polarization.

if the test volume height $h = 4$ m, then h_1 shall be 1 m and 4 m for horizontal polarization, and 1 m and 3,5 m for vertical polarization.

NSA data for additional transmit antenna heights of 3,0 m and 4,0 m (HP) and 2,5 m and 3,5 m (VP) for a measurement distance of 10 m, and for an additional transmit antenna height of 2,5 m (HP) and 2,0 m (VP) for a measurement distance of 5 m, are provided in Table 2.

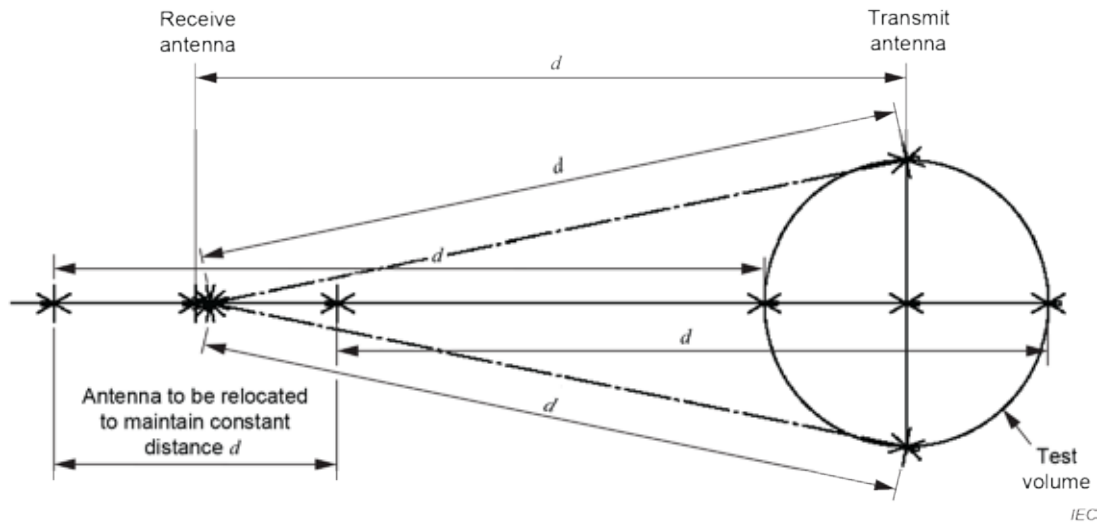


Figure 11 – Typical antenna positions for a weather-protected OATS or a SAC – vertical polarization validation measurements

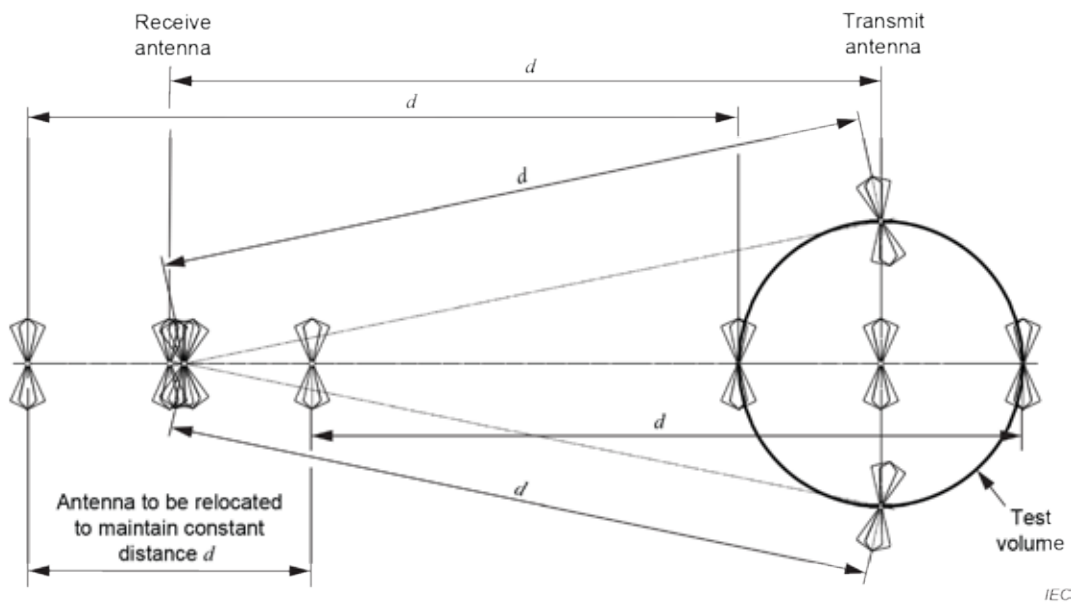


Figure 12 – Typical antenna positions for a weather-protected OATS or a SAC – horizontal polarization validation measurements