

INTERNATIONAL STANDARD



**Low-voltage electrical installations –
Part 4-44: Protection for safety – Protection against voltage disturbances and
electromagnetic disturbances**



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IEC 60364-4-44

Edition 3.0 2024-12
REDLINE VERSION

INTERNATIONAL STANDARD



**Low-voltage electrical installations –
Part 4-44: Protection for safety – Protection against voltage disturbances and
electromagnetic disturbances**

INTERNATIONAL
ELECTROTECHNICAL
COMMISSION

ICS 91.140.50; 33.100.10; 33.100.20

ISBN 978-2-8327-0121-8

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INTERNATIONAL ELECTROTECHNICAL COMMISSION

LOW-VOLTAGE ELECTRICAL INSTALLATIONS –

**Part 4-44: Protection for safety –
Protection against voltage disturbances
and electromagnetic disturbances**

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This redline version of the official IEC Standard allows the user to identify the changes made to the previous edition IEC 60364-4-44:2007+AMD1:2015+AMD2:2018 CSV. A vertical bar appears in the margin wherever a change has been made. Additions are in green text, deletions are in strikethrough red text.

IEC 60364-4-44 has been prepared by IEC technical committee 64: Electrical installations and protection against electric shock. It is an International Standard.

This third edition cancels and replaces the second edition published in 2007, Amendment 1:2015 and Amendment 2:2018. This edition constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition:

- a) the structure of the document has been updated in accordance with the ISO/IEC Directives, Part 2:2021: the terms, definitions and symbols have been regrouped under a new Subclause 440.3, the tables and figures have been renumbered;
- b) Clause 443 has been amended to better introduce the DC SPD and to improve some of the wording.

The text of this International Standard is based on the following documents:

Draft	Report on voting
64/2696/FDIS	64/2737/RVD

Full information on the voting for its approval can be found in the report on voting indicated in the above table.

The language used for the development of this International Standard is English.

This document was drafted in accordance with ISO/IEC Directives, Part 2, and developed in accordance with ISO/IEC Directives, Part 1 and ISO/IEC Directives, IEC Supplement, available at www.iec.ch/members_experts/refdocs. The main document types developed by IEC are described in greater detail at www.iec.ch/publications.

A list of all parts in the IEC 60364 series, published under the general title *Low-voltage electrical installations*, can be found on the IEC website.

The reader's attention is drawn to the fact that Annex C lists all of the "in-some-country" clauses on differing practices of a less permanent nature relating to the subject of this document.

The committee has decided that the contents of this document will remain unchanged until the stability date indicated on the IEC website under webstore.iec.ch in the data related to the specific document. At this date, the document will be

- reconfirmed,
- withdrawn, or
- revised.

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INTRODUCTION

This part of IEC 60364 covers the protection of electrical installations and measures against voltage disturbances and electromagnetic disturbances.

The requirements are arranged into four clauses as follows:

- | | |
|------------|---|
| Clause 442 | Protection of low-voltage installations against temporary overvoltages due to earth faults in the high-voltage system and due to faults in the low-voltage system |
| Clause 443 | Protection against transient overvoltages of atmospheric origin or due to switching |
| Clause 444 | Measures against electromagnetic influences |
| Clause 445 | Protection against undervoltage |

LOW-VOLTAGE ELECTRICAL INSTALLATIONS –

Part 4-44: Protection for safety – Protection against voltage disturbances and electromagnetic disturbances

440 Protection against voltage disturbances and electromagnetic disturbances

440.1 Scope

~~The rules of~~ This part of IEC 60364 ~~are intended to provide~~ provides requirements for the safety of electrical installations in the event of voltage disturbances and electromagnetic disturbances generated for different specified reasons.

The ~~rules~~ requirements of this document are not intended to apply to systems for distribution of energy to the public, or power generation and transmission for such systems (see the scope of IEC 60364-1) although such disturbances ~~may~~ can be conducted into or between electrical installations via these supply systems.

440.2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

~~IEC 60038:2009, IEC standard voltages~~

~~IEC 60050-604:1987, International Electrotechnical Vocabulary – Chapter 604: Generation, transmission and distribution of electricity – Operation~~

IEC 60364-1, *Low-voltage electrical installations – Part 1: Fundamental principles, assessment of general characteristics, definitions*

~~IEC 60364-4-41:2005, Electrical installations of buildings – Part 4-41: Protection for safety – Protection against electric shock~~

IEC 60364-5-52, *Low-voltage electrical installations – Part 5-52: Selection and erection of electrical equipment – Wiring systems*

IEC 60364-5-53:2001/2019, *Low-voltage electrical installations – of buildings – Part 5-53: Selection and erection of electrical equipment – Devices for protection for safety, isolation, switching and, control and monitoring*

IEC 60364-5-53:2001/2019/AMD1:2002/2020

IEC 60364-5-53:2001/2019/AMD2:2015/2024

IEC 60364-5-54:2002/2011, *Low-voltage electrical installations – of buildings – Part 5-54: Selection and erection of electrical equipment – Earthing arrangements and protective bonding conductors*¹

IEC 60364-5-54:2011/AMD1:2021

¹ ~~A third edition is currently in preparation.~~

~~IEC 60479-1:2005, Effects of current on human beings and livestock – Part 1: General aspects~~

IEC 60664-1:2007/2020, Insulation coordination for equipment within low-voltage supply systems – Part 1: Principles, requirements and tests

~~IEC 60950-1, Information technology equipment – Safety – Part 1: General requirements~~

~~IEC 61000-2-5:1995, Electromagnetic compatibility (EMC) – Part 2: Environment – Section 5: Classification of electromagnetic environments – Basic EMC publication~~

~~IEC 61000-6-1, Electromagnetic compatibility (EMC) – Part 6-1: Generic standards – Immunity for residential, commercial and light industrial environments~~

~~IEC 61000-6-2, Electromagnetic compatibility (EMC) – Part 6-2: Generic standards – Immunity for industrial environments~~

~~IEC 61000-6-3, Electromagnetic compatibility (EMC) – Part 6-3: Generic standards – Emission standard for residential, commercial and light industrial environments~~

~~IEC 61000-6-4, Electromagnetic compatibility (EMC) – Part 6-4: Generic standards – Emission standard for industrial environments~~

IEC 61156 (all parts), Multicore and symmetrical pair/quad cables for digital communications

IEC 61196-7, Coaxial communication cables – Part 7: Sectional specification for cables for BCT cabling in accordance with ISO/IEC 15018 11801-4 – Indoor drop cables for systems operating at 5 MHz – 3 000 6 000 MHz

~~IEC 61558-2-1, Safety of power transformers, power supplies, reactors and similar products – Part 2-1: Particular requirements for tests for separating transformers and power supplies incorporating separating transformers for general applications~~

~~IEC 61558-2-4, Safety of power transformers, power supply units and similar – Part 2-4: Particular requirements for isolating transformers for general use~~

~~IEC 61558-2-6, Safety of power transformers, power supply units and similar – Part 2-6: Particular requirements for safety isolating transformers for general use~~

~~IEC 61558-2-15, Safety of power transformers, power supply units and similar – Part 2-15: Particular requirements for isolating transformers for the supply of medical locations~~

~~IEC 61643 (all parts), Low-voltage surge protective devices~~

~~IEC 61643-11:2011, Low-voltage surge protective devices – Part 11: Surge protective devices connected to low-voltage power systems – Requirements and test methods~~

~~IEC 61643-22, Low-voltage surge protective devices – Part 22: Surge protective devices connected to telecommunications and signalling networks – Selection and application principles~~

IEC 61936-1, Power installations exceeding 1 kV AC and 1,5 kV DC – Part 1: Common rules AC

~~IEC 62305 (all parts), Protection against lightning~~

~~IEC 62305-1, Protection against lightning – Part 1: General principles~~

IEC 62305-3, Protection against lightning – Part 3: Physical damage to structures and life hazard

~~IEC 62305-4, Protection against lightning – Part 4: Electrical and electronic systems within structures~~

ISO/IEC 11801-1, *Information technology – Generic cabling for customer premises – Part 1: General requirements*

ISO/IEC 14763-2:2012/2019, *Information technology – Implementation and operation of customer premises cabling – Part 2: Planning and installation*
~~ISO/IEC 14763-2:2012/AMD1:2015~~

ISO/IEC TR 29106, *Information technology – Generic cabling – Introduction to the MICE environmental classification*

440.3 Terms, definitions and symbols

440.3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in IEC 60364-1 and the following apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- IEC Electropedia: available at <https://www.electropedia.org/>
- ISO Online browsing platform: available at <https://www.iso.org/obp>

440.3.1.1

urban environment

area with a high density of buildings or densely populated communities with tall buildings

EXAMPLE Town centre.

440.3.1.2

suburban environment

area with a medium density of buildings

EXAMPLE Town outskirts.

440.3.1.3

rural environment

area with a low density of buildings

EXAMPLE The countryside.

440.3.1.4

surge protective device

SPD

device that contains at least one non-linear component that is intended to limit surge voltages and divert surge currents

Note 1 to entry: An SPD is a complete assembly, having appropriate connecting means.

~~Note 2 to entry: This note applies to the French language only.~~

[SOURCE: IEC 61643-11:2011, 3.1.1]

440.3.1.5

calculated risk level

CRL

calculated value of risk used to evaluate the need for transient overvoltage protection

~~Note 1 to entry: This note applies to the French language only.~~

440.3.1.6 **rated impulse voltage**

U_W

value of the impulse withstand voltage assigned by the manufacturer to the equipment or to a part of it, characterizing the specified withstand capability of its insulation against transient overvoltages

[SOURCE: IEC 60664-1:2007/2020, ~~3.9.2, Modified~~ ~~symbol added~~ 3.1.19, modified – In the term, "withstand" has been deleted and the symbol U_{imp} has been replaced with U_W .]

440.3.1.7 **bonding network** **BN**

set of interconnected conductive structures that provides an "electromagnetic shield" for electronic systems at frequencies from direct current (DC) to low radio frequency (RF)

~~[3.2.2 of ETS 300 253:1995]~~

Note 1 to entry: The term "electromagnetic shield" denotes any structure used to divert, block or impede the passage of electromagnetic energy. In general, a BN does not need to be connected to earth but BN considered in this standard are connected to earth.

440.3.1.8 **bonding ring conductor** **BRC**

earthing bus conductor in the form of a closed ring

~~[3.1.3 of EN 50310:2000]~~

Note 1 to entry: Normally the bonding ring conductor, as part of the bonding network, has multiple connections to the CBN that improves its performance.

440.3.1.9 **common equipotential bonding system** **common bonding network** **CBN**

equipotential bonding system providing both protective-equipotential-bonding and functional-equipotential-bonding

[SOURCE: IEC 60050-195:2021, 195-02-25]

440.3.1.10 **equipotential bonding**

~~provision~~ ~~set~~ of electric connections intended to achieve equipotentiality between conductive parts

[SOURCE: IEC 60050-195:2021, 195-01-10]

440.3.1.11 **earth-electrode network** **ground-electrode network (US)**

part of an earthing arrangement comprising only the earth electrodes and their interconnections

[SOURCE: IEC 60050-195:2021, 195-02-21]

440.3.1.12 meshed bonding network MESH-BN

bonding network in which all associated equipment frames, racks and cabinets and usually the DC power return conductor, are bonded together as well as at multiple points to the CBN and may have the form of a mesh

~~[3.2.2 of ETS 300 253:1995]~~

Note 1 to entry: The MESH-BN augments the CBN.

440.3.1.13 by-pass equipotential bonding conductor parallel earthing conductor PEC

earthing conductor connected in parallel with the screens of signal ~~and~~ or data cables in order to limit the current flowing through the screens

440.3.2 Symbols

In this document, the following symbols are used (see Figure 1).

I_E	part of the earth fault current in the high-voltage system that flows through the earthing arrangement of the transformer substation
R_E	resistance of the earthing arrangement of the transformer substation
R_A	resistance of the earthing arrangement of the exposed-conductive-parts of the equipment of the low-voltage installation
R_B	resistance of the earthing arrangement of the low-voltage system neutral, for low-voltage systems in which the earthing arrangements of the transformer substation and of the low-voltage system neutral are electrically independent
U_0	in TN- and TT-systems: nominal AC RMS line voltage to earth in IT-systems: nominal AC voltage between line conductor and neutral conductor or mid-point conductor, as appropriate
U_f	power-frequency fault voltage that appears in the low-voltage system between exposed-conductive-parts and earth for the duration of the fault
U_1	power-frequency stress voltage between the line conductor and the exposed-conductive-parts of the low-voltage equipment of the transformer substation during the fault
U_2	power-frequency stress voltage between the line conductor and the exposed-conductive-parts of the low-voltage equipment of the low-voltage installation during the fault

NOTE 1 The power-frequency stress voltage (U_1 and U_2) is the voltage that appears across the insulation of low-voltage equipment and across surge protective devices connected to the low-voltage system.

The following additional symbols are used in respect of IT-systems in which the exposed-conductive-parts of the equipment of the low-voltage installation are connected to an earthing arrangement that is electrically independent of the earthing arrangement of the transformer substation.

I_h	fault current that flows through the earthing arrangement of the exposed-conductive-parts of the equipment of the low-voltage installation during a period when there is a high-voltage fault and a first fault in the low-voltage installation (see Table 1).
I_d	fault current, in accordance with 411.6.2, that flows through the earthing arrangement of the exposed-conductive-parts of the low-voltage installation during the first fault in a low-voltage system (see Table 1).
Z	impedance (e.g. IMD internal impedance, artificial neutral impedance) between the low-voltage system and an earthing arrangement.

NOTE 2 An earthing arrangement ~~may~~ can be considered electrically independent of another earthing arrangement if a rise of potential with respect to earth in one earthing arrangement does not cause an unacceptable rise of potential with respect to earth in the other earthing arrangement. See IEC 61936-1.

441 ~~(Vacant)~~ Void

442 Protection of low-voltage installations against temporary overvoltages due to earth faults in the high-voltage system and due to faults in the low-voltage system

442.1 Field of application

442.1.1 General

~~The rules of this clause provide~~ This Clause 442 provides requirements for the safety of low-voltage installation in the event of

- a fault between the high-voltage system and earth in the transformer substation that supplies the low-voltage installation,
- a loss of the supply neutral in the low-voltage system,
- a short-circuit between a line conductor and neutral,
- an accidental earthing of a line conductor of a low-voltage IT-system.

The requirements for the earthing arrangement at the transformer substation are given in IEC 61936-1.

442.1.2 General requirements

As Clause 442 covers faults between a high-voltage line and the earth in the HV/LV substation, it gives rules for the designer and installer of the substation. It is necessary to have the following information concerning the high-voltage system:

- quality of the system earthing;
- maximum level of earth fault current;
- resistance of the earthing arrangement.

The following Subclauses 442.2, 442.3, 442.4 and 442.5 consider four situations as proposed in 442.1, which generally cause the most severe temporary overvoltages such as defined in IEC 60050-604614:

- fault between the high-voltage system(s) and earth (see 442.2);
- loss of the neutral in a low-voltage system (see 442.3);
- accidental earthing of a low-voltage IT system (see 442.4);
- short-circuit in the low-voltage installation (see 442.5).

442.2 Overvoltages in LV-systems during a high-voltage earth fault

442.2.1 General

In case of a fault to earth on the HV-side of the substation, the following types of overvoltage may affect the LV-installation:

- power-frequency fault voltage (U_f);
- power-frequency stress voltages (U_1 and U_2).

Table 1 provides the relevant methods of calculation for the different types of overvoltages.

NOTE 1—Table 1 deals with IT systems with a neutral point only. For IT systems with no neutral point, the formulae should be adjusted accordingly.

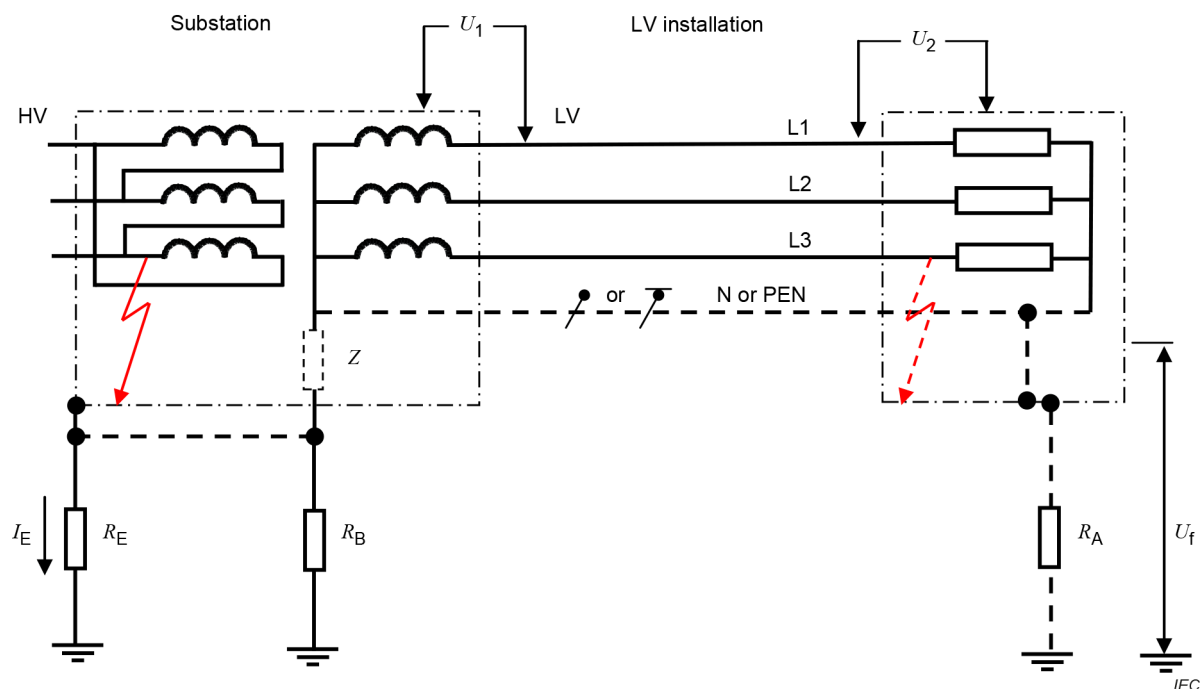


Figure 1 – Representative schematic diagram for possible connections to earth in substation and LV-installation and occurring overvoltages in case of faults

Where high- and low-voltage earthing systems exist in proximity to each other, two practices are presently used:

- interconnection of all high-voltage (R_E) and low-voltage (R_B) earthing systems;
- separation of high-voltage (R_E) from low-voltage (R_B) earthing systems.

The general method used is interconnection. The high- and low-voltage earthing systems shall be interconnected if the low-voltage system is totally confined within the area covered by the high-voltage earthing system (see IEC 61936-1).

NOTE 2 Details of the different types of system earthing (TN, TT, IT) are shown in IEC 60364-1.

Table 1 – Power-frequency stress voltages and power-frequency fault voltage in low-voltage system

Types of system earthing	Types of earth connections	U_1	U_2	U_f
TT	R_E and R_B connected	U_o^a	$R_E \times I_E + U_o$	0^a
	R_E and R_B separated	$R_E \times I_E + U_o$	U_o^a	0^a
TN	R_E and R_B connected	U_o^a	U_o^a	$R_E \times I_E^b$
	R_E and R_B separated	$R_E \times I_E + U_o$	U_o^a	0^a
IT	R_E and Z connected R_E and R_A separated	U_o^a	$R_E \times I_E + U_o$	0^a
		$U_o \times \sqrt{3}$	$R_E \times I_E + U_o \times \sqrt{3}$	$R_A \times I_h$
	R_E and Z connected R_E and R_A interconnected	U_o^a	U_o^a	$R_E \times I_E$
		$U_o \times \sqrt{3}$	$U_o \times \sqrt{3}$	$R_E \times I_E$
	R_E and Z separated R_E and R_A separated	$R_E \times I_E + U_o$	U_o^a	0^a
		$R_E \times I_E + U_o \times \sqrt{3}$	$U_o \times \sqrt{3}$	$R_A \times I_d$

Key

 With existing earth fault in the installation.

^a No consideration ~~needs to~~ shall be given.

^b See 442.2.2 second paragraph.

NOTE 32 The requirements for U_1 and U_2 are derived from design criteria for insulation of low-voltage equipment with regard to temporary power-frequency overvoltage (see also Table 2).

NOTE 43 In a system whose neutral is connected to the earthing arrangement of the transformer substation, such temporary power-frequency overvoltage is also expected across insulation which is not in an earthed enclosure when the equipment is outside a building.

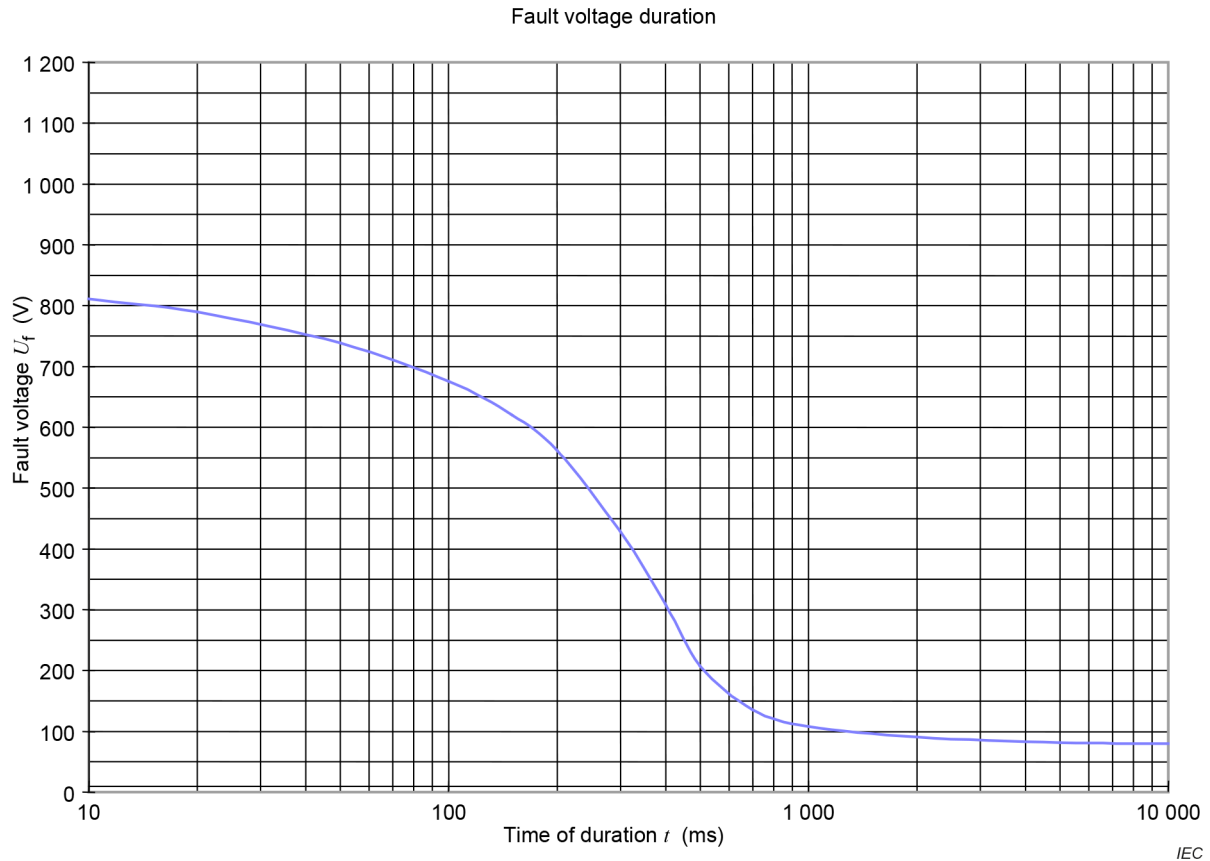
NOTE 54 In TT- and TN-systems the statement "connected" and "separated" refers to the electrical connection between R_E and R_B . For IT-systems it refers to the electrical connection between R_E and Z and the connection between R_E and R_A .

442.2.2 Magnitude and duration of power-frequency fault voltage

The magnitude and the duration of the fault voltage U_f (as calculated in Table 1) which appears in the LV installation between exposed-conductive-parts and earth, shall not exceed the values given for U_f by the curve of Figure 2 for the duration of the fault.

Normally, the PEN conductor of the low-voltage system is connected to earth at more than one point. In this case, the total resistance is reduced. For these multiple grounded PEN conductors, U_f can be calculated as:

$$U_f = 0,5 R_E \times I_E$$



NOTE ~~The curve shown in Figure 44.A2 is taken from IEC 61936-1.~~ On the basis of probabilistic and statistical evidence this curve represents a low level of risk for the simple worst case where the low-voltage system neutral conductor is earthed only at the transformer substation earthing arrangements. Guidance is provided in IEC 61936-1 concerning other situations.

SOURCE: IEC 61936-1:2021, Figure 12

Figure 2 – Tolerable fault voltage due to an earth-fault in the HV system

442.2.3 Magnitude and duration of power-frequency stress voltages

The magnitude and the duration of the power-frequency stress voltage (U_1 and U_2) as calculated in Table 1 of the low-voltage equipment in the low-voltage installation due to an earth fault in the high-voltage system shall not exceed the requirements given in Table 2.

Table 2 – Permissible power-frequency stress voltage

Duration of the earth fault in the high-voltage system t	Permissible power-frequency stress voltage on equipment in low-voltage installations U
$> 5 \text{ s}$	$U_o + 250 \text{ V}$
$\leq 5 \text{ s}$	$U_o + 1\,200 \text{ V}$

In systems without a neutral conductor, U_o shall be the line-to-line voltage.

NOTE 1 The first line of the table relates to high-voltage systems having long disconnection times, for example, isolated neutral and resonant earthed high-voltage systems. The second line relates to high-voltage systems having short disconnection times, for example low-impedance earthed high-voltage systems. Both lines together are relevant design criteria for insulation of low-voltage equipment with regard to temporary power frequency overvoltage, see IEC 60664-1.

NOTE 2 In a system whose neutral is connected to the earthing arrangement of the transformer substation, such temporary power-frequency overvoltage is also expected across insulation which is not in an earthed enclosure when the equipment is outside a building.

442.2.4 Requirements for calculation of limits

Where required by Table 1, the permissible power-frequency stress voltage shall not exceed the value given in Table 2.

Where required by Table 1, the permissible power-frequency fault voltage shall not exceed the value given in Figure 2.

The requirements of 442.2.2 and 442.2.3 are deemed to be fulfilled for installations receiving a supply at low-voltage from a public electricity distribution system.

To fulfil the above requirements, coordination between the HV-system operator and the LV-system installer is necessary. Compliance with the above requirements mainly falls into the responsibility of the substation installer, owner, operator for whom it is also necessary to fulfil requirements provided by IEC 61936-1. Therefore the calculation for U_1 , U_2 and U_f is normally not necessary for the LV system installer.

Possible measures to fulfil the above requirements are for example:

- separation of earthing arrangement between HV and LV;
- change of LV system earthing;
- reduction of earth resistance R_E .

442.3 Power-frequency stress voltage in case of loss of the neutral conductor in a TN and TT system

Consideration shall be given to the fact that, if the neutral conductor in a multi-phase system is interrupted, basic, double and reinforced insulation as well as components rated for the voltage between line and neutral conductors can be temporarily stressed with the line-to-line voltage. The stress voltage can reach up to $U = \sqrt{3} U_o$.

442.4 Power-frequency stress voltage in the event of an earth fault in an IT system with distributed neutral

Consideration shall be given to the fact that, if a line conductor of an IT system is earthed accidentally, insulation or components rated for the voltage between line and neutral conductors can be temporarily stressed with the line-to-line voltage. The stress voltage can reach up to $U = \sqrt{3} U_o$.

442.5 Power-frequency stress voltage in the event of a short-circuit between a line conductor and the neutral conductor

Consideration shall be given to the fact that if a short-circuit occurs in the low-voltage installation between a phase conductor and the neutral conductor, the voltage between the other line conductors and the neutral conductor can reach the value of $1,45 \times U_o$ for a time up to 5 s.

443 Protection against transient overvoltages of atmospheric origin or due to switching

443.1 General

Clause 443 specifies requirements for protection of electrical installations against transient overvoltages of atmospheric origin transmitted by the supply distribution system including direct strikes to the supply system and against switching overvoltages. Clause 443 does not specify requirements for protection against transient overvoltage due to direct or nearby lightning strokes on the structure.

NOTE 1 For risk management for protection against transient overvoltage due to direct or nearby lightning strokes on the structure, see IEC 62305-2.

In general, switching overvoltages have lower amplitude than transient overvoltages of atmospheric origin and therefore the requirements regarding protection against transient overvoltages of atmospheric origin normally cover protection against switching overvoltages.

If no transient overvoltage protection against disturbances of atmospheric origin is installed, it can be necessary for protection against switching overvoltages ~~may need~~ to be provided.

NOTE 2 Overvoltages due to switching can be longer in duration and can contain more energy than the transient overvoltages of atmospheric origin. See 443.4.

The characteristics of transient overvoltages of atmospheric origin depend on factors such as:

- the nature of the supply distribution system (underground or overhead);
- the possible existence of at least one surge protective device (SPD) upstream of the origin of the installation;
- the voltage level of the supply system.

NOTE 3 As regards transient overvoltages of atmospheric origin, no distinction is made between earthed and unearthed systems.

Protection against transient overvoltages is provided by the installation of surge protective devices (SPDs).

Selection and installation of SPDs shall be in compliance with IEC 60364-5-53:2001, ~~IEC 60364-5-53:2001/AMD1:2002~~2019, Clause 534 and IEC 60364-5-53:2019/AMD2:20152024, Clause 534.

If there is a need for SPDs on the power supply lines, additional SPDs on other lines such as telecom lines are also recommended.

Requirements for protection against transient overvoltages transmitted by data transmission systems are not covered by Clause 443. See IEC 61643-22.

Clause 443 does not apply to installations where the consequences caused by overvoltages affect:

- a) structures with a risk of explosion;
- b) structures where the damage ~~may~~ can also involve the environment (e.g. chemical or radioactive emissions).

443.2 Void

443.3 Void

443.4 Overvoltage control

Protection against transient overvoltage shall be provided where the consequence caused by overvoltage affects:

- a) human life, e.g. safety services, medical care facilities;
- b) public services and cultural heritage, e.g. loss of public services, IT centres, museums;
- c) commercial or industrial activity, e.g. hotels, banks, industries, commercial markets, farms.

For all other cases, a risk assessment according to 443.5 shall be performed in order to determine if protection against transient overvoltage is required. If the risk assessment is not performed, the electrical installation shall be provided with protection against transient overvoltage.

However the transient overvoltage protection is not required for single dwelling units where the total economic value of the electrical installation to be protected is less than five times the economic value of the SPD located at the origin of the installation.

~~NOTE 1—National Committees can modify the exception criteria related to single dwelling units or to not apply it.~~

Protection against switching overvoltages should be considered in the case of equipment likely to produce switching overvoltages or disturbances exceeding the values according to the overvoltage category of the installation, for example where a LV generator supplies the installation or where inductive or capacitive loads (e.g. motors, transformers, capacitor banks), storage units or high current loads are installed.

NOTE Annex B provides guidance for overvoltage control where utility provided SPDs are installed on overhead lines.

For a low-voltage installation supplied from a high-voltage distribution network through a separate transformer (i.e. an industrial application), additional means for protection against overvoltages due to lightning should be installed on the high-voltage side of the transformer.

443.5 Risk assessment method

NOTE 1 For protection of a structure and its electrical systems against lightning and surges of atmospheric origin, IEC 62305-2 applies.

Calculated risk level (CRL) is used to determine if protection against transient overvoltages of atmospheric origin is required. The CRL is found by the following formula

$$CRL = f_{env} / (L_P \times N_g)$$

where

- f_{env} is an environmental factor and the value of f_{env} shall be calculated according to Table 3;

Table 3 – Calculation of f_{env}

Environment	f_{env}
Rural and suburban environment	$85 \times F$
Urban environment	$850 \times F$

The value of coefficient F shall be taken equal to 1 for all installations. ~~However, National Committees may adjust the value of coefficient F from 1 to 3 for dwellings.~~

- N_g is the lightning ground flash density (flash per km² per year) relevant to the location of the power line and connected structure;

NOTE 2 According to IEC 62305-2:2010, Clause A.1, 25 thunderstorm days per year are equivalent to a value of 2,5 flashes per km² per year. This is derived from the formula $N_g = 0,1 \times T_d$, where T_d is the number of thunderstorm days per year (keraunic level).

- the risk assessment length L_P is calculated as below:

$$L_P = 2 L_{PAL} + L_{PCL} + 0,4 L_{PAH} + 0,2 L_{PCH}$$

where

L_{PAL} is the length (km) of the low-voltage overhead line;

L_{PCL} is the length (km) of the low-voltage underground cable;

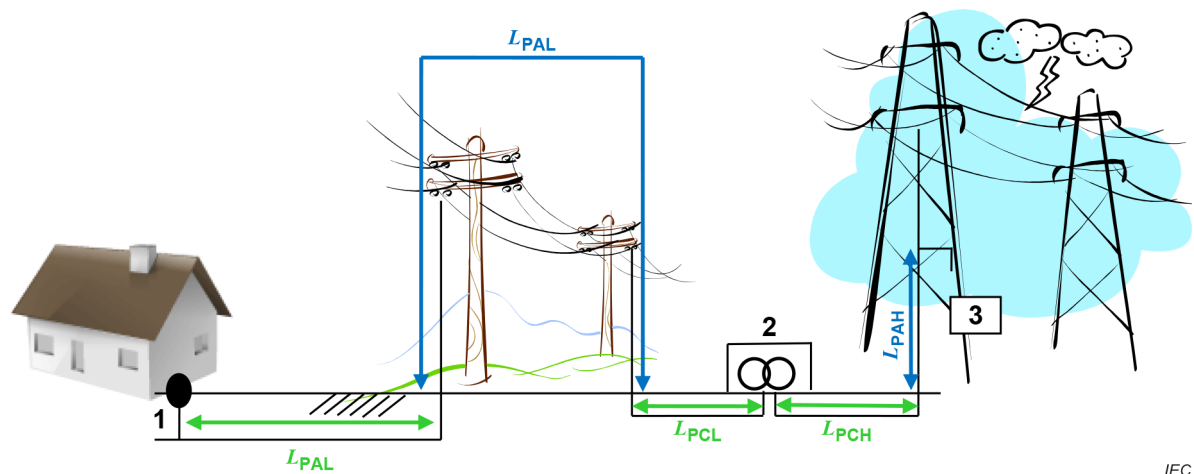
L_{PAH} is the length (km) of the high-voltage overhead line;

L_{PCH} is the length (km) of the high-voltage underground cable.

The total length ($L_{PAL} + L_{PCL} + L_{PAH} + L_{PCH}$) is limited to 1 km or by the distance from the first overvoltage protective device installed in the power network to the entrance of the installation, whichever is smaller.

If the distribution networks lengths are totally or partially unknown then L_{PAL} shall be taken equal to the remaining distance to reach a total length of 1 km.

For example, if only the distance of the underground cable is known (e.g. 100 m), then the L_{PAL} shall be taken equal to 90 m. An illustration of an installation showing the lengths to consider is given in Figure 3.



Key

- 1 origin of the installation
- 2 LV/HV transformer
- 3 surge arrester (overvoltage protective device)

Figure 3 – Illustration of an installation showing the lengths to consider

If $CRL \geq 1\,000$, no protection against transient overvoltages of atmospheric origin is ~~needed~~ required;

If $CRL < 1\,000$, protection against transient overvoltages of atmospheric origin is required.

NOTE 3 Examples of calculations of CRL are given in Annex A.

443.6 Classification of rated impulse voltages (overvoltage categories)

443.6.1 Purpose of classification of rated impulse voltages (overvoltage categories)

Subclause 443.6 gives information on the overvoltage category of the equipment.

NOTE Overvoltage categories are defined within electrical installations for the purpose of insulation coordination and a related classification of equipment with rated impulse voltages is provided in Table 4.

The rated impulse voltage is used to classify equipment energized directly from the low-voltage electrical installation into overvoltage category.

Rated impulse voltages for equipment selected according to the nominal voltage are provided to distinguish different levels of availability of equipment with regard to continuity of service and an acceptable risk of failure.

It is possible that inherent overvoltage control based only on the impulse voltage withstand of the equipment in accordance with IEC 60664-1 ~~might~~ is not ~~be~~ sufficient, because:

- transient overvoltages transmitted by the supply distribution system are not significantly attenuated downstream in most installations. Insulation coordination can be achieved in the whole installation, by transient overvoltage protection of the equipment corresponding to the classified rated impulse voltage, reducing the risk of failure to an acceptable level;
- in installations supplied by a completely buried low-voltage system not including overhead lines, surge currents and partial lightning currents are distributed via the underground cables;
- equipment is often connected to two different services, e.g. power line and data line. Field experience shows that much surge related damage is experienced on this kind of equipment.

It is necessary to consider the rated impulse voltage U_W (see IEC 60664-1) of the most sensitive equipment to be protected in the system or, in cases where a temporary loss of function of equipment is critical, the equipment level immunity (see IEC 61000-4-5).

443.6.2 Rated impulse voltages of equipment and overvoltage categories

The following points shall be noted:

- a) Equipment with a rated impulse voltage corresponding to overvoltage category IV is suitable for use at, or in the proximity of, the ~~origin of~~ point where the electrical installation ~~is connected to an external electric power network (either public or private), for example upstream of the main distribution board.~~ Equipment of category IV has a very high impulse withstand capability providing the required high degree of reliability, and shall have a rated ~~a rated~~ impulse voltage not less than the value specified in Table 4.

NOTE 1 Examples of such equipment include ~~electricity~~ energy meters, ~~primary overcurrent~~ protective devices and ripple control units, ~~telecontrol~~ systems.

- b) Equipment with a rated impulse voltage corresponding to overvoltage category III is suitable for use in the ~~fixed~~ electrical installation downstream of and including the main distribution board, providing a high degree of availability, and shall have a rated impulse voltage not less than the value specified in Table 4.

NOTE 2 Examples of such equipment include distribution boards, ~~local~~ generation, circuit-breakers, wiring systems including cables, busbars, junction boxes, switches, socket-outlets ~~in the fixed installation~~ (see IEC 60050-826:2022, 826-15-01), and equipment for industrial use and some other equipment, e.g. stationary motors ~~with permanent connection to the fixed installation.~~

- c) Equipment with a rated impulse voltage corresponding to overvoltage category II is suitable for connection to the ~~fixed~~ electrical installation, providing a degree of availability normally required for current-using equipment, and shall have a rated impulse voltage not less than the value specified in Table 4.

NOTE 3 Examples of such equipment include tools, household appliances and similar loads.

- d) ~~Equipment with a rated impulse voltage corresponding to overvoltage category I is only suitable for use in the fixed installation where SPDs are installed outside the equipment to limit transient overvoltages to the specified level, and shall have a rated impulse voltage not less than the value specified in Table 443.2. Therefore, equipment with a rated impulse voltage corresponding to overvoltage category I should preferably not be installed at or near the origin of installation.~~

NOTE 4 ~~Examples of such equipment include those containing electronic circuits like computers, home electronics, etc.~~

Equipment with a rated impulse voltage corresponding to overvoltage category I is only suitable for use where measures are taken to reduce transient overvoltages and temporary overvoltages to not exceed the value specified in Table 4.

Table 4 – Required rated impulse voltage of equipment U_W

Nominal voltage of the installation ^a V	Voltage line to neutral derived from nominal voltages a.c. or d.c. up to and including V	Required rated impulse voltage of equipment ^c kV			
		Overvoltage category IV (equipment with very high rated impulse voltage)	Overvoltage category III (equipment with high rated impulse voltage)	Overvoltage category II (equipment with normal rated impulse voltage)	Overvoltage category I (equipment with reduced rated impulse voltage)
		For example, energy meter, telecontrol systems	For example, distribution boards, switches, socket-outlets	For example, distribution domestic appliances, tools	For example, sensitive electronic equipment
120/208	150	4	2,5	1,5	0,8
230/400 ^{b, d} 277/480 ^b	300	6	4	2,5	1,5
400/690	600	8	6	4	2,5
1 000	1 000	12	8	6	4
1 500 d.c.	1 500 d.c.			8	6
^a —According to IEC 60038:2009. ^b —In Canada and USA, for voltages to earth higher than 300 V, the rated impulse voltage corresponding to the next highest voltage in this column applies. ^c —This rated impulse voltage is applied between live conductors and PE. ^d —For IT systems operations at 220–240 V, the 230/400 row shall be used, due to the voltage to earth at the earth fault on one line.					

Nominal voltage of the installation V	Voltage line to neutral or mid-point derived from nominal voltages AC or DC up to and including V	Required rated impulse voltage of equipment ^a kV			
		Overvoltage category IV (equipment with very high rated impulse voltage)	Overvoltage category III (equipment with high rated impulse voltage)	Overvoltage category II (equipment with normal rated impulse voltage)	Overvoltage category I (equipment with reduced rated impulse voltage)
120/208	150	4	2,5	1,5	0,8
230/400 ^{b c} 277/480 ^c	300	6	4	2,5	1,5
400/690	600	8	6	4	2,5
1 000	1 000	12	8	6	4
1 250 (for DC only)	1 250 (for DC only)	12	8	6	4
1 500 (for DC only)	1 500 (for DC only)	15	10	8	6
^a This rated impulse voltage is applied between live conductors and PE. ^b For IT systems having line-to-line voltage from 220 V to 240 V, the 230/400 row shall be used, due to the voltage to earth at the earth fault on one line. ^c In Canada and the USA, for voltages to earth higher than 300 V, the rated impulse voltage corresponding to the next highest voltage in this column applies.					

444 Measures against electromagnetic influences

444.1 General

Clause 444 provides basic recommendations for the mitigation of electromagnetic disturbances. Electromagnetic interference (EMI) ~~may~~ can disturb or damage information technology systems or information technology equipment as well as equipment with electronic components or circuits. Currents due to lightning, switching operations, short-circuits and other electromagnetic phenomena ~~may~~ can cause overvoltages and electromagnetic interference.

These effects are most severe

- where large metal loops exist; and
- where different electrical wiring systems are installed in common routes, e.g. for power supply and for signalling information technology equipment within a building.

The value of the induced voltage depends on the rate of rise (di/dt) of the interference current, and on the size of the loop.

Power cables carrying large currents with a high rate of rise of current (di/dt) (e.g. the starting current of lifts or currents controlled by rectifiers) can induce overvoltages in cables of information technology systems, which can influence or damage information technology equipment or similar electrical equipment.

In or near rooms for medical use, electric or magnetic fields associated with electrical installations can interfere with medical electrical equipment.

This Clause 444 provides information for architects of buildings and for designers and installers of electrical installations of buildings on some installation concepts that limit electromagnetic influences. Basic considerations are given here to mitigate such influences that ~~may~~ can result in disturbance.

444.2 Void

NOTE This clause is reserved for future input.

444.3 Void

444.4 Mitigation of electromagnetic interference (EMI)

444.4.1 General

Consideration shall be given by the designer and installer of the electrical installation to the measures described below for reducing the electric and magnetic influences on electrical equipment.

Only electrical equipment, which meets the requirements in the appropriate EMC standards or the EMC requirements of the relevant product standard, shall be used.

444.4.2 Sources of EMI

Electrical equipment sensitive to electromagnetic influences should not be located close to potential sources of electromagnetic emission such as

- switching devices for inductive loads,
- electric motors,
- fluorescent lighting,
- welding machines,
- computers,
- rectifiers,
- choppers,
- frequency converters ~~or~~ regulators,
- lifts,
- transformers,
- switchgear,
- power distribution busbars.

444.4.3 Measures to reduce EMI

The following measures reduce electromagnetic interference.

- a) For electrical equipment sensitive to electromagnetic influences, surge protection devices ~~and~~ or filters, ~~or both~~, are recommended to improve electromagnetic compatibility with regard to conducted electromagnetic phenomena.
- b) Metal sheaths of cables should be bonded to the CBN.
- c) Inductive loops should be avoided by selection of a common route for power, signal and data circuits wiring.
- d) Power and signal cables should be kept separate and should, wherever practical, cross each other at right-angles (see 444.6.3).
- e) Use of cables with concentric conductors to reduce currents induced into the protective conductor.

- f) Use of symmetrical multicore cables (e.g. screened cables containing separate protective conductors) for the electrical connections between convertors and motors, which have frequency controlled motor-drives.
- g) Use of signal and data cables according to the EMC requirements of the manufacturer's instructions.
- h) Where a lightning protection system is installed,
 - power and signal cables shall be separated from the down conductors of lightning protection systems (LPS) by either a minimum distance or by use of screening. The minimum distance shall be determined by the designer of the LPS in accordance with IEC 62305-3;
 - metallic sheaths or shields of power and signal cables should be bonded in accordance with the requirements for lightning protection ~~given in IEC 62305-3 and IEC 62305-4.~~
- i) Where screened signal or data cables are used, care should be taken to limit the fault current from power systems flowing through the screens and cores of signal cables, or data cables, which are earthed. Additional conductors ~~may~~ **can** be necessary, e.g. a by-pass equipotential bonding conductor for screen reinforcement; see Figure 4.

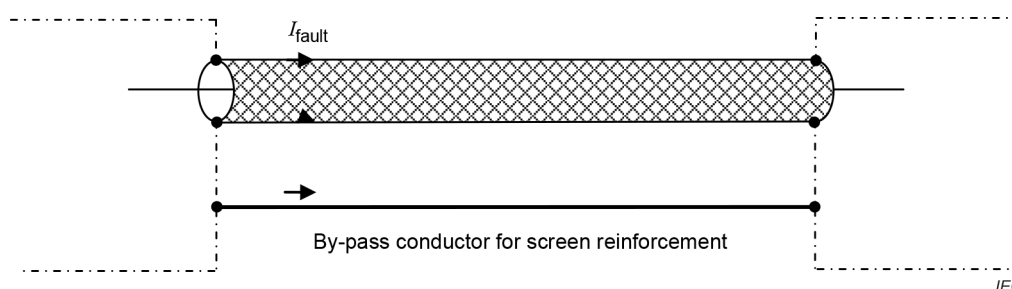


Figure 4 – By-pass conductor for screen reinforcement to provide a common equipotential bonding system

NOTE 1 The provision of a by-pass conductor in proximity to a signal, or data, cable sheath also reduces the area of the loop associated with equipment, which is only connected by a protective conductor to earth. This practice considerably reduces the EMC effects of lightning electromagnetic pulse (LEMP).

- j) Where screened signal cables or data cables are common to several buildings supplied from a TT-system, a by-pass equipotential bonding conductor should be used; see Figure 5. The by-pass conductor shall have a minimum cross-sectional area of 16 mm² Cu or equivalent. The equivalent cross-sectional area shall be dimensioned in accordance with IEC 60364-5-54:2011, 544.1.

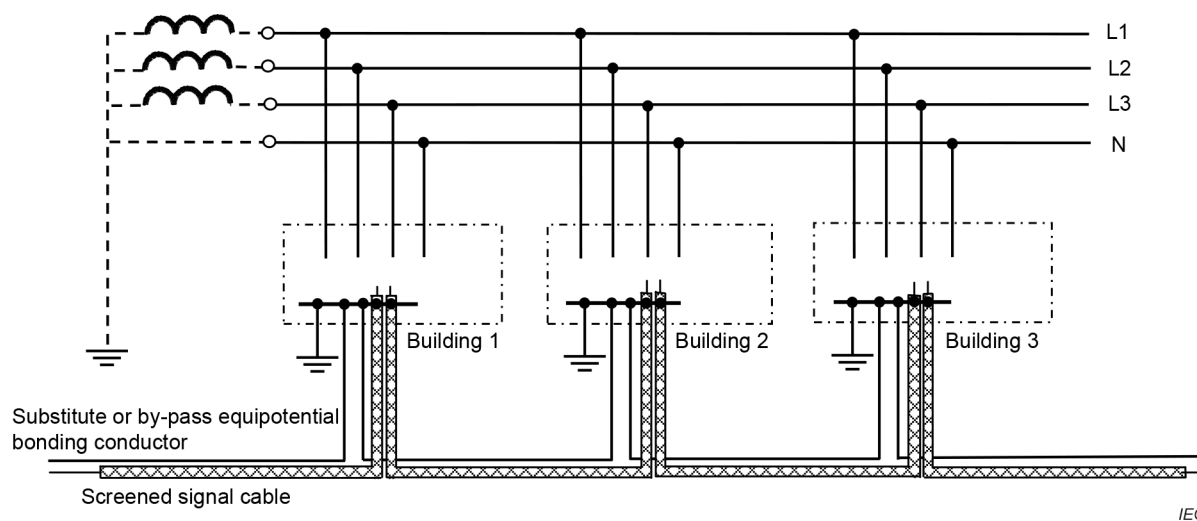


Figure 5 – Example of a substitute or by-pass equipotential bonding conductor in a TT-system

NOTE 2 Where the earthed shield is used as a signal return path, a double-coaxial cable ~~may~~ can be used.

NOTE 3 It is recalled that if the consent according to IEC 60364-4-41:2005, 411.3.1.2 and IEC 60364-4-41:2005/AMD1:2017, 411.3.1.2 cannot be obtained, it is the responsibility of the owners or operators to avoid any danger due to the exclusion of those cables from the connection to the main equipotential bonding.

NOTE 4 The problems of earth differential voltages on large public telecommunication networks are the responsibility of the network operator, who ~~may~~ can employ other methods.

NOTE 5 In the Netherlands, a by-pass equipotential bonding conductor, connecting the earthing systems of several TT installations together, is permitted only if fault protection, in accordance with IEC 60364-4-41:2005, 411.3.1.2 and IEC 60364-4-41:2005/AMD1:2017, 411.3.1.2, remains effective in the case of failure of any single RCD.

- k) Equipotential bonding connections should have an impedance as low as possible
 - by being as short as possible,
 - by having a cross-section shape that results in low inductive reactance and impedance per metre of route, e.g. a bonding braid with a width to thickness ratio of five to one.
- l) Where an earthing busbar is intended (according to 444.5.7) to support the equipotential bonding system of a significant information technology installation in a building, it may be installed as a closed ring.

NOTE 6 This measure is preferably applied in buildings of the telecommunications industry.

444.4.4 TN-system

444.4.4.1 To minimize electromagnetic influences, the following Subclauses 444.4.4.2 to 444.4.4.5 apply.

444.4.4.2 It is recommended that TN-C systems should not be maintained in existing buildings containing, or likely to contain, significant amounts of information technology equipment.

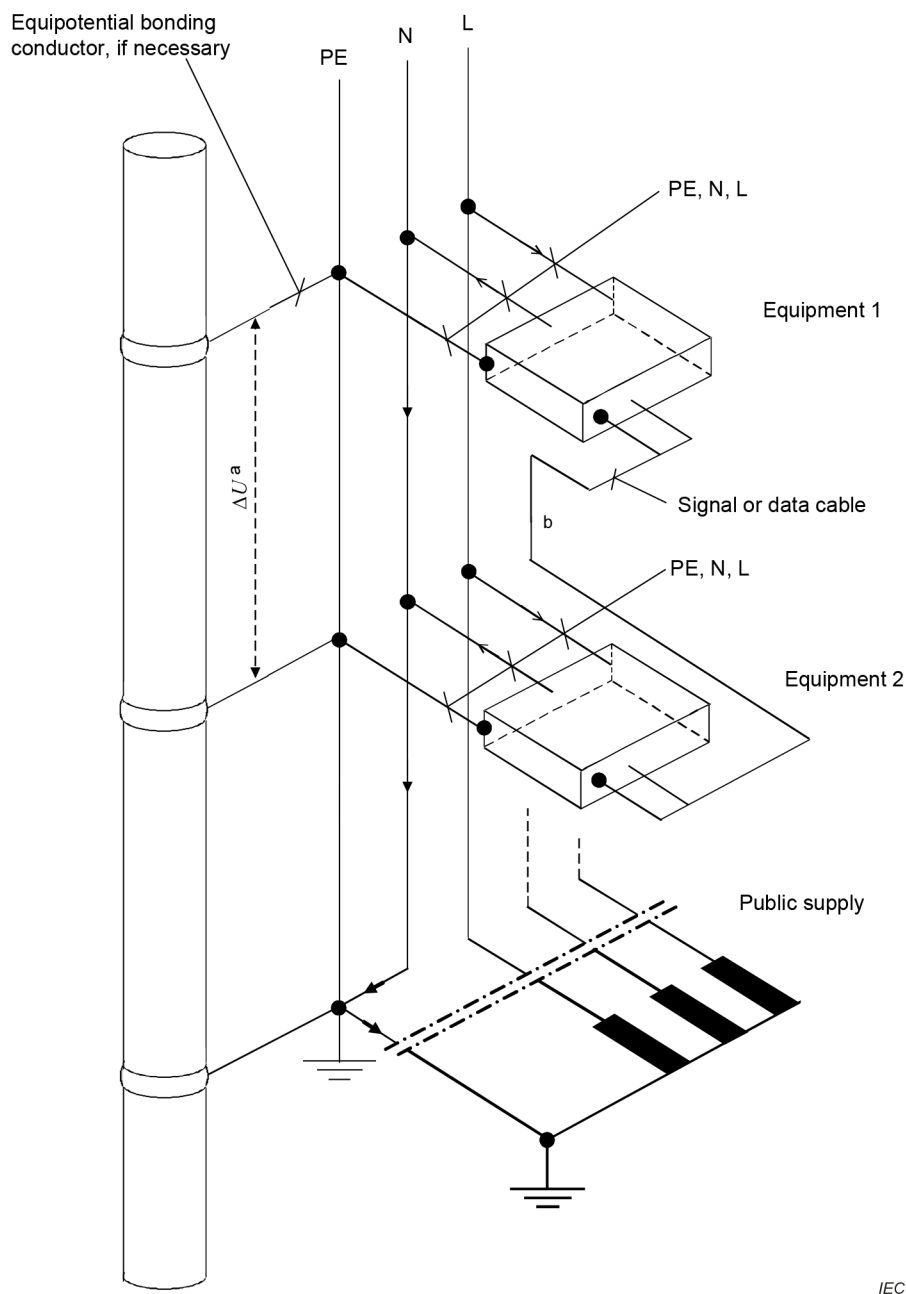
TN-C-systems shall not be used in newly constructed buildings containing, or likely to contain, significant amounts of information technology equipment.

NOTE Any TN-C installation is likely to have load or fault current diverted via equipotential bonding into metallic services and structures within a building.

444.4.4.3 In existing buildings supplied from public low-voltage networks and which contain, or are likely to contain, significant amounts of information technology equipment, a TN-S system should be installed downstream of the origin of the installation; see Figure 6.

In newly constructed buildings, TN-S systems shall be installed downstream of the origin of the installation; see Figure 6.

NOTE—The effectiveness of a TN-S-system may be enhanced by use of a residual current monitoring device, RCM, complying with IEC 62020-1:2020.

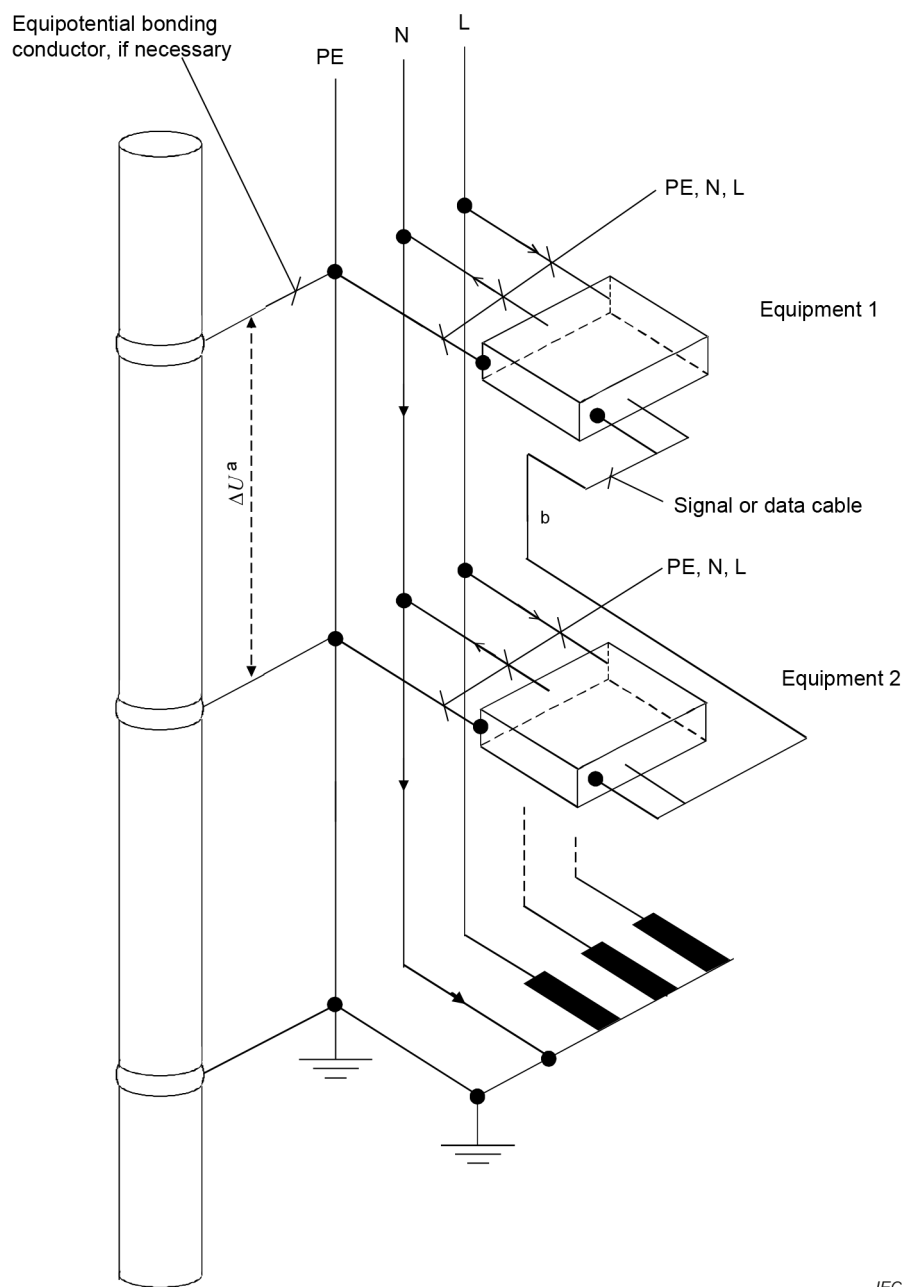


^a No voltage drop ΔU along the PE conductor under normal operation conditions.

^b Loops of limited area formed by signal or data cables.

Figure 6 – Avoidance of neutral conductor currents in a bonded structure by using the TN-S system from the origin of the public supply up to and including the final circuit within a building

444.4.4.4 In existing buildings where the complete low-voltage installation including the transformer is operated only by the user and which contain, or are likely to contain, significant amounts of information technology equipment, TN-S systems should be installed; see Figure 7.



IEC

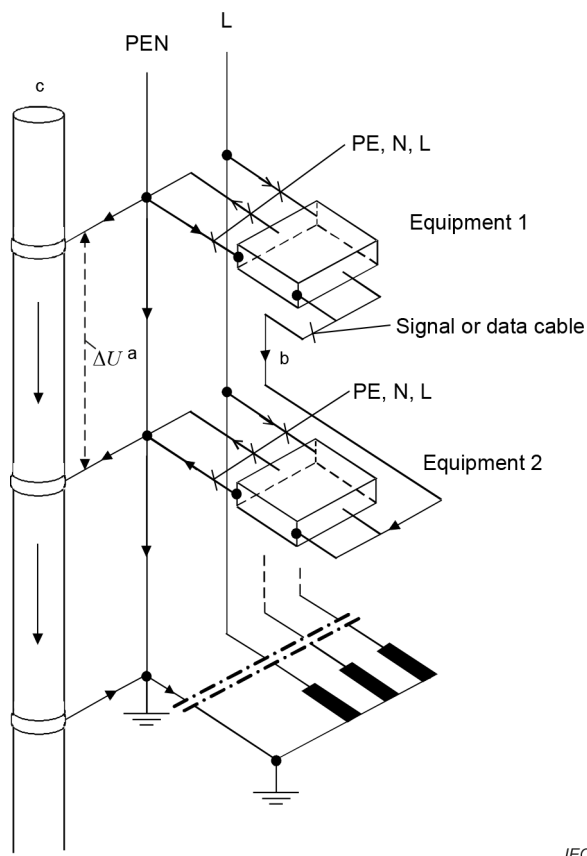
^a No voltage drop ΔU along the PE conductor under normal operation conditions.

^b Loops of limited area formed by signal or data cables.

Figure 7 – Avoidance of neutral conductor currents in a bonded structure by using a TN-S system downstream of a consumer's private supply transformer

444.4.4.5 Where an existing installation is a TN-C-S system (see Figure 8), signal and data cable loops should be avoided by

- changing all TN-C parts of the installation shown in Figure 8 into TN-S, as shown in Figure 6, or
- where this change is not possible, by avoiding signal and data cable interconnections between different parts of the TN-S installation.



IEC

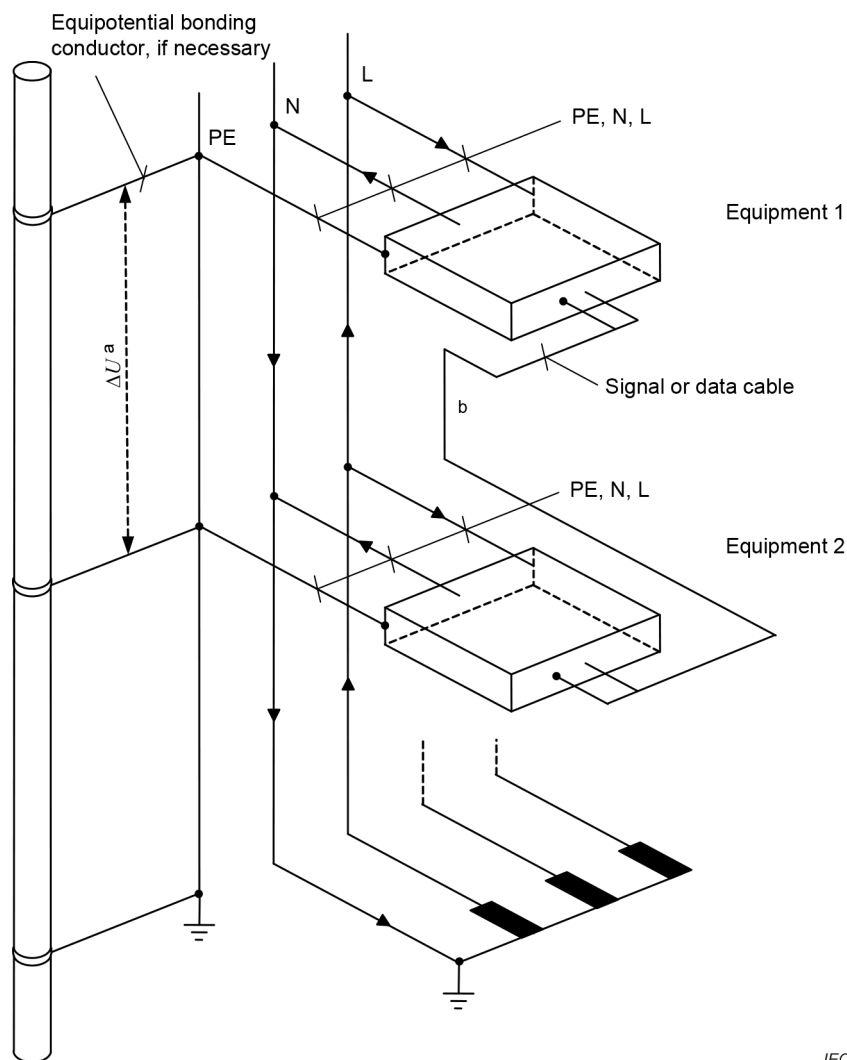
- a Voltage drop ΔU along PEN in normal operation.
- b Loop of limited area formed from signal or data cables.
- c Extraneous-conductive-part.

NOTE In a TN-C-S system, the current, which in a TN-S system would flow only through the neutral conductor, flows also through the screens or reference conductors of signal cables, exposed-conductive-parts, and extraneous-conductive-parts such as structural metalwork.

Figure 8 – TN-C-S system within an existing building installation

444.4.5 TT system

In a TT system, such as that shown in Figure 9, consideration should be given to overvoltages which ~~may~~ can exist between live parts and exposed-conductive-parts when the exposed-conductive-parts of different buildings are connected to different earth electrodes.



IEC

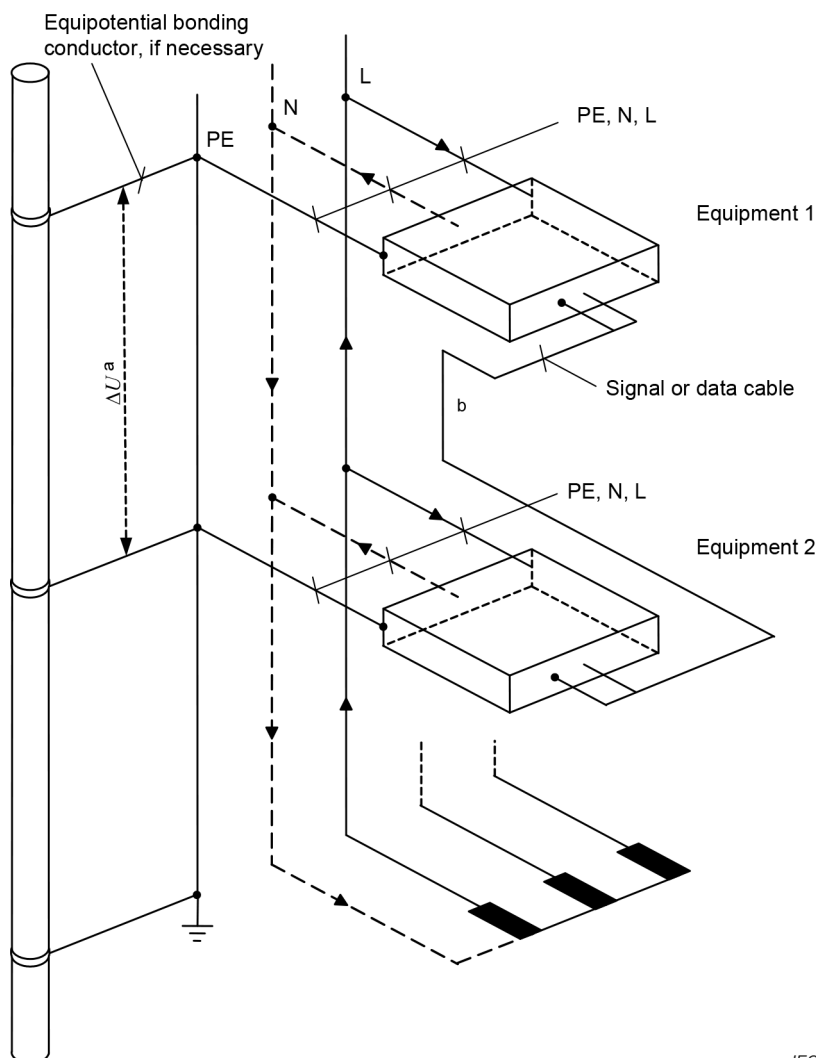
- ^a Voltage drop ΔU along PEN in normal operation.
- ^b Loop of limited area formed from signal or data cables.

Figure 9 – TT system within a building installation

444.4.6 IT system

In a three-phase IT system (see Figure 10), the voltage between a healthy line-conductor and an exposed-conductive-part can rise to the level of the line-to-line voltage when there is a single insulation fault between a line conductor and an exposed-conductive-part; this condition should be considered.

NOTE—Electronic equipment directly supplied between the line conductor and neutral should be designed to withstand such a voltage between the line conductor and exposed-conductive-parts; see corresponding requirement from ~~IEC 60950-1~~ IEC 62368-1:2023 for information technology equipment.



IEC

^a Voltage drop ΔU along PEN in normal operation.

^b Loop of limited area formed from signal or data cables.

Figure 10 – IT system within a building installation

444.4.7 Multiple-source supply

444.4.7.1 General

For multiple-source power supplies, the provisions in 444.4.7.2 and 444.4.7.3 shall be applied.

NOTE Where multiple earthing of the star points of the sources of supplies is applied, neutral conductor currents **may** can flow back to the relevant star point, not only via the neutral conductor, but also via the protective conductor as shown in Figure 11. For this reason, the sum of the partial currents flowing in the installation is no longer zero and a magnetic stray field is created, similar to that of a single conductor cable.

In the case of single conductor cables, which carry AC current, a circular electromagnetic field is generated around the core conductor that **may** can interfere with electronic equipment. Harmonic currents produce similar electromagnetic fields but they attenuate more rapidly than those produced by fundamental currents.

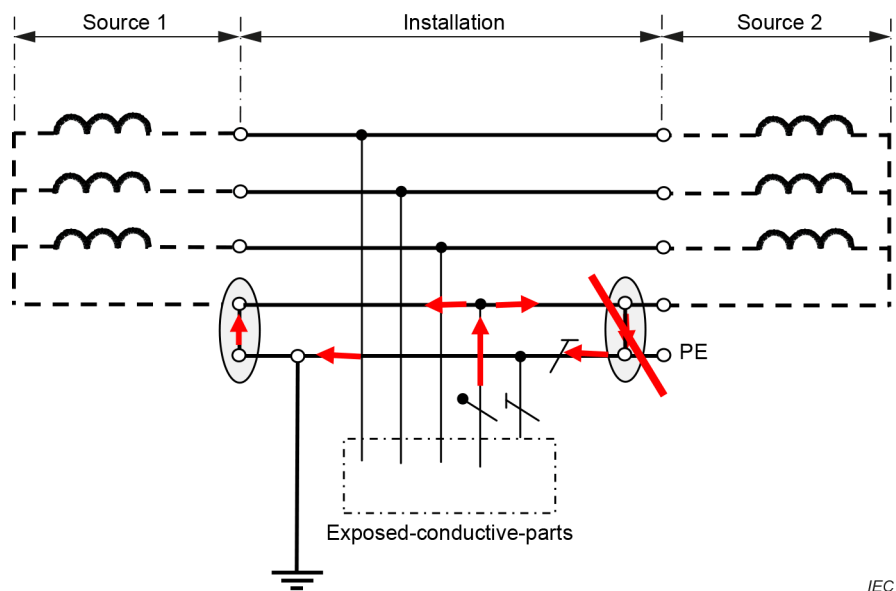
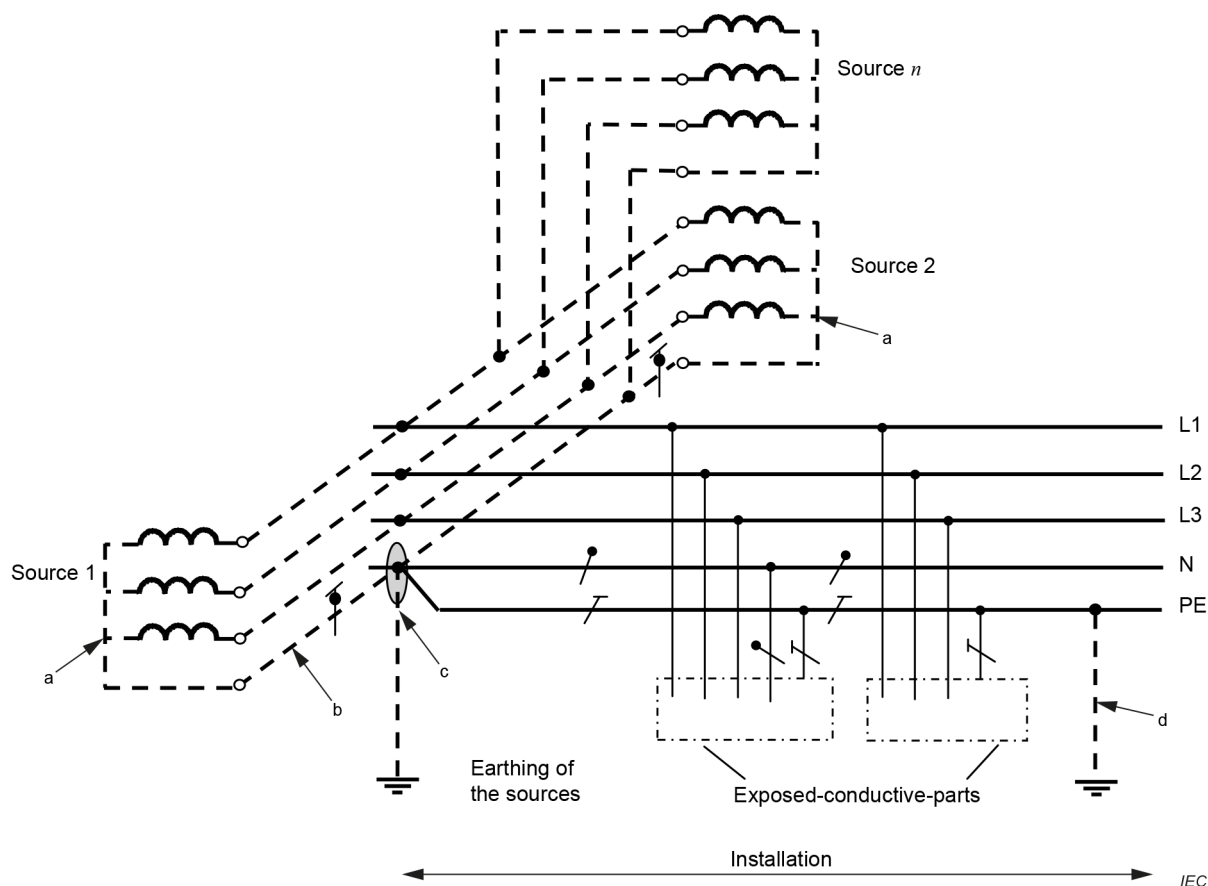


**Figure 11 – TN multiple-source power supply
with a non-suitable multiple connection between PEN and earth**

444.4.7.2 TN multiple-source power supplies

In the case of TN multiple-source power supplies to an installation, the star points of the different sources shall, for EMC reasons, be interconnected by an insulated conductor that is connected to earth centrally at one and the same point; see Figure 12.

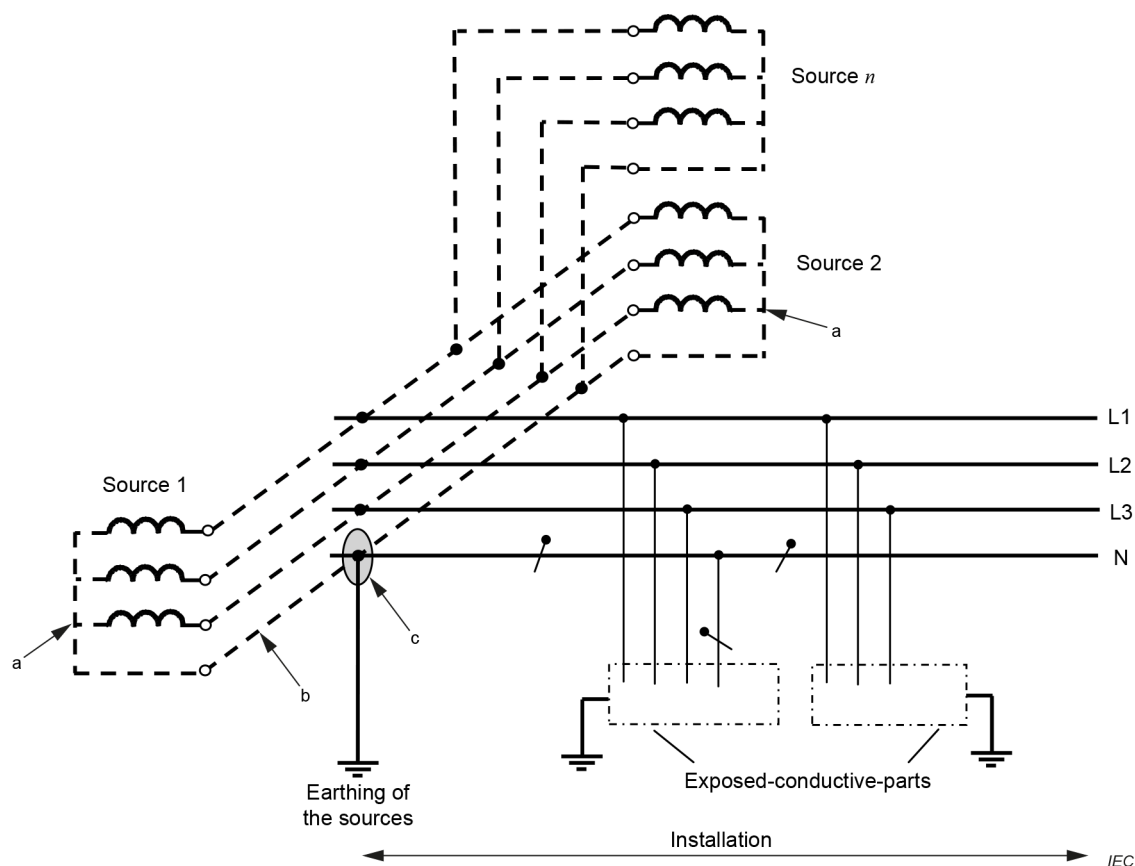


- a No direct connection from either transformer neutral points or generator star points to earth is permitted.
- b The conductor interconnecting either the neutral points of transformers, or the star-points of generators, shall be insulated. This conductor functions as a PEN conductor and it may be marked as such; however, it shall not be connected to current-using-equipment and a warning notice to that effect shall be attached to it, or placed adjacent to it.
- c Only one connection between the interconnected neutral points of the sources and the PE shall be provided. This connection shall be located inside the main switchgear assembly.
- d Additional earthing of the PE in the installation may be provided.

Figure 12 – TN multiple-source power supplies to an installation with connection to earth of the star points at one and the same point

444.4.7.3 TT multiple-source power supplies

In the case of TT multiple-source power supplies to an installation, it is recommended that the star points of the different sources are, for EMC reasons, interconnected and connected to earth centrally at only one point; see Figure 13.



- ^a No direct connection from either the transformer star points or the generator star points to earth is permitted.
- ^b The conductor interconnecting either the star points of transformers, or generator star points, shall be insulated. However, it shall not be connected to current-using-equipment and a warning notice to that effect shall be attached to it, or placed adjacent to it.
- ^c Only one connection between the interconnected star points of the sources and the PE shall be provided. This connection shall be located inside the main switchgear assembly.

Figure 13 – TT multiple-source power supplies to an installation with connection to earth of the star points at one and the same point

444.4.8 Transfer of supply

In TN systems the transfer from one supply to an alternative supply shall be by means of a switching device, which switches the line conductors and the neutral, if any; see Figure 14, Figure 15 and Figure 16.