

INTERNATIONAL STANDARD

NORME INTERNATIONALE



**Protection against lightning –
Part 3: Physical damage to structures and life hazard**

**Protection contre la foudre –
Partie 3: Dommages physiques sur les structures et risques humains**



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INTERNATIONAL ELECTROTECHNICAL COMMISSION

PROTECTION AGAINST LIGHTNING –

Part 3: Physical damage to structures and life hazard

FOREWORD

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IEC 62305-3 has been prepared by IEC technical committee 81: Lightning protection. It is an International Standard.

This third edition cancels and replaces the second edition published in 2010. This edition constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition:

- a) Minimum thicknesses of metal sheets or metal pipes are given in Table 4 for air-termination systems where it is necessary to prevent hot-spot problems. Maximum temperature rises ΔT (K) and time duration t_{50} (s) for different thicknesses and long strokes are also given.
- b) Cross-reference to the IEC 62561 series is made for the use of reliable, stable, safe and appropriate LPS components.

- c) The application of two methods – general and simplified – for separation distance calculation is clarified.
- d) Some changes to the requirements for continuity of steel reinforcement are made.
- e) Annex C is revised to address comments from IEC subcommittee 31J.
- f) Revision of positioning of air-termination conductors are modified according to the three accepted methods. A more precise description of the methods for positioning of the air-termination systems is made according to the complexity of structures to be protected. The main text has been simplified, Annex A has been deleted and all detailed information has been moved to Annex D.
- g) Information on the protection of green roofs is introduced in Annex D.
- h) Information on the protection of protruding parts on facades of tall buildings is introduced in Annex D;
- i) a new definition of “electrically insulated LPS” has been introduced to distinguish it from an LPS both electrically and physically isolated from the structure, with a slight modification of the other LPS definitions.

The text of this International Standard is based on the following documents:

Draft	Report on voting
81/764/FDIS	81/767/RVD

Full information on the voting for its approval can be found in the report on voting indicated in the above table.

The language used for the development of this International Standard is English.

This document was drafted in accordance with ISO/IEC Directives, Part 2, and developed in accordance with ISO/IEC Directives, Part 1 and ISO/IEC Directives, IEC Supplement, available at www.iec.ch/members_experts/refdocs. The main document types developed by IEC are described in greater detail at www.iec.ch/publications.

A list of all parts in the IEC 62305 series, published under the general title *Protection against lightning*, can be found on the IEC website.

The following differing practices of a less permanent nature exist in the countries indicated below.

In Austria, Annex C shall not be applied and is replaced by the National standard ÖVE/ÖNORM EN 62305-3 Beiblatt 1:2013-11-01 Blitzschutz – Teil 3: Schutz von baulichen Anlagen und Personen – Beiblatt 1: Zusätzliche Informationen für bauliche Anlagen mit explosionsgefährdeten Bereichen. In Austria, Annex C shall be classified as "Informative".

In Germany, the need for lightning protection is determined by, and the class of required LPS shall be selected according to, a national annex to the third edition of IEC 62305-1 (including an option for a risk assessment following the third edition of IEC 62305-2).

In Germany, for a metallic or electrically-continuous connected reinforced concrete framework, in addition, DIN EN 62305-3 Beiblatt 1 shall be applied.

In Germany, 8.1 condition b) is not applied – see DIN EN 62305-3 Beiblatt 1. Instead, the alternate measures, as described in DIN EN 62305-3 Beiblatt 1, shall be applied.

In Germany, for 8.2, the alternate measures, as described in DIN EN 62305-3 Beiblatt 1, shall be applied.

In Japan, when using country-specific lightning protection components, the manufacturer and/or lightning protection designer shall explain that the component will withstand the electromagnetic effects of lightning currents and possible accidental stresses without damage.

In Italy, a separation distance is not required in structures with metallic or electrically-continuous connected reinforced concrete framework according to 5.3.5.

In Italy, in reinforced concrete structures, the reinforcement may be used for equipotential bonding. In this case, if a ring electrode is not yet installed and connected to the reinforcement steels, a ring conductor welded or bolted to the steel reinforcement will be installed, to which the bonding bars should be connected via welded conductors.

In the Netherlands, in some situations, special fasteners which are necessary and which are not available on the commercial market and are not tested according to IEC 62561-4 (because of a small number of required special fasteners), must comply with the lateral and axial test mentioned in IEC 62561-4. A written statement of passing these lateral and axial tests must be issued by the designer and/or the installer of the LPS and must be a part of the commissioning documents.

In South Africa, the class of required LPS shall be selected on the basis of a risk assessment of either the second edition of IEC 62305-2 or the third edition of IEC 62305-2 . This note applies also for D.4.1 and D.4.2.1.

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INTRODUCTION

This part of IEC 62305 deals with the protection, in and around a structure, against physical damage and injury to human beings due to touch and step voltages.

The main and most effective measure for protection of structures and its content against physical damage is considered to be a lightning protection system (LPS). It usually consists of both external and internal lightning protection measures.

An external LPS is intended to

- a) intercept a lightning flash to the structure (with an air-termination system),
- b) conduct the lightning current safely towards earth (using a down-conductor system),
- c) disperse the lightning current into the earth (using an earth-termination system).

NOTE The purpose of the external LPS is to protect the structure from a direct lightning strike by providing the preferred attachment points, conducting and dispersing the lightning current. It will not significantly influence the attachment process between the structure and the lightning to increase or reduce the number of direct lightning strikes (S1) to the structure.

An internal LPS prevents dangerous sparking within the structure using either equipotential bonding or a separation distance (and hence isolation) between the external LPS (as defined in 3.2) and other electrically conducting elements internal to the structure.

Main protection measures against injury to human beings due to touch and step voltages are intended to:

- 1) reduce dangerous current flowing through bodies by either insulating exposed conductive parts, or by increasing the surface soil resistivity, or both,
- 2) reduce the occurrence of dangerous touch and step voltages by either physical restrictions or warning notices, or both.

The type and location of an LPS should be carefully considered in the initial design of a new structure, thereby enabling maximum advantage to be taken of the electrically conductive parts of the structure. By so doing, design and construction of an integrated installation is made easier, the overall aesthetic aspects can be improved, and the effectiveness of the LPS can be increased at minimum cost and effort.

Access to the ground and the proper use of foundation steelwork for the purpose of forming an effective earth termination may well be impossible once construction work on a site has commenced. Therefore, soil resistivity and the nature of the earth should be considered at the earliest possible stage of a project. This information is fundamental to the design of an earth-termination system and can influence the foundation design work for the structure.

Regular consultation between LPS designers and installers, architects and builders is essential in order to achieve the best result at minimum cost.

If lightning protection is to be added to an existing structure, every effort should be made to ensure that it conforms to the principles of this document. The design of the type and location of an LPS should take into account the features of the existing structure.

When safety is involved and significant changes are made to the structure or its use changes, consideration of updating the lightning protection installation to the present edition of this document is recommended.

National or local laws and regulations can provide guidance or minimum requirements on the application of this document. This includes specifying the class of a required LPS for specific applications without a risk assessment, the conditions of separation and bonding of other earth-termination systems, the additional information given in Annex C for LPSs in case of structures with a risk of explosion, and the mandatory requirements for inspection, testing and maintenance of LPSs given in Clause 7.

PROTECTION AGAINST LIGHTNING –

Part 3: Physical damage to structures and life hazard

1 Scope

This part of IEC 62305 provides the requirements for protection of a structure against physical damage by means of a lightning protection system (LPS), and for protection against injury to human beings due to touch and step voltages in the vicinity of an LPS (see IEC 62305-1).

This document is applicable to the:

- a) design, installation, inspection and maintenance of an LPS for structures without limitation of their height,
- b) establishment of measures for protection against injury to human beings primarily due to touch and step voltages.

NOTE 1 Specific requirements for an LPS in structures dangerous to their surroundings due to the risk of explosion are provided in Annex C.

NOTE 2 This document is not intended to provide protection against failures of electrical and electronic systems due to overvoltages. Specific requirements for such cases are provided in IEC 62305-4.

NOTE 3 Specific requirements for the protection against lightning of wind turbines are reported in IEC 61400-24 [1]¹.

NOTE 4 Specific requirements for the protection against overvoltage of photovoltaic systems are reported in IEC 61643-32 [2] and in IEC 62305-4:2024, Annex F.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60079-10-1:2020, *Explosive atmospheres – Part 10-1: Classification of areas – Explosive gas atmospheres*

IEC 60079-10-2:2015, *Explosive atmospheres – Part 10-2: Classification of areas – Explosive dust atmospheres*

IEC 60079-14, *Explosive atmospheres – Part 14: Electrical installations design, selection and erection*

IEC 60364-5-53, *Low-voltage electrical installations – Part 5-53: Selection and erection of electrical equipment – Devices for protection for safety, isolation, switching, control and monitoring*

IEC 61643-11, *Low-voltage surge protective devices – Part 11: Surge protective devices connected to low-voltage power systems – Requirements and test methods*

¹ Numbers in square brackets refer to the Bibliography.

IEC 61643-21, *Low-voltage surge protective devices – Part 21: Surge protective devices connected to telecommunications and signalling networks – Performance requirements and testing methods*

IEC 62305-1:2024, *Protection against lightning – Part 1: General principles*

IEC 62305-2:—², *Protection against lightning – Part 2: Risk management*

IEC 62305-4:2024, *Protection against lightning – Part 4: Electrical and electronic systems within structures*

IEC 62561 (all parts), *Lightning protection system components (LPSC)*

IEC 62561-1:2017³, *Lightning protection system components (LPSC) – Part 1: Requirements for connection components*

IEC TS 62561-8:2018, *Lightning protection system components (LPSC) – Part 8: Requirements for components for isolated LPS*

ISO 3864-1, *Graphical symbols – Safety colours and safety signs – Part 1: Design principles for safety signs and safety markings*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in IEC 62305-1, IEC 62305-2, IEC 62305-4 and IEC 60079-14 and the following apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- IEC Electropedia: available at <https://www.electropedia.org/>
- ISO Online browsing platform: available at <https://www.iso.org/obp>

3.1

lightning protection system

LPS

complete system used to reduce injury to human beings and physical damage due to lightning flashes to a structure and its contents

Note 1 to entry: A lightning protection system usually consists of external and internal lightning protection systems. To protect internal systems against the effects of LEMP, measures according to IEC 62305-4 are necessary.

3.2

external lightning protection system

part of the LPS consisting of an air-termination system, a down-conductor system and an earth-termination system

² Third edition under preparation. Stage at the time of publication IEC FDIS 62305-2:2024.

³ Withdrawn.

3.3

isolated LPS

LPS with an air-termination system and down-conductor system positioned in such a way that the LPS has no electrical and no physical contact with the structure to be protected except at ground level for equipotential bonding and that along the complete path of the lightning current the separation distance is respected

Note 1 to entry: In an isolated LPS, dangerous sparks between the LPS and the structure are avoided.

3.4

attached LPS

LPS with an air-termination system and down-conductor system and earth-termination system positioned in such a way that the path of the lightning current can be in contact with the structure to be protected

3.5

electrically insulated LPS

LPS with an air-termination system and down-conductor system attached to the structure but positioned in such a way that the LPS has no electrical contact with the structure to be protected except at ground level for equipotential bonding and that along the complete path of the lightning current the separation distance is maintained

Note 1 to entry: In an electrically insulated LPS dangerous sparks between the LPS and the structure and partial lightning currents are avoided.

Note 2 to entry: An insulating down conductor or insulating stand-offs that meet the requirements of IEC TS 62561-8 ensure that the LPS has no direct electrical contact with the structure to be protected and ensure an adequate equivalent separation distance to avoid flashover.

3.6

internal lightning protection system

part of the LPS consisting of either lightning equipotential bonding or electrical separation from an external LPS, or both

3.7

air-termination system

part of an external LPS using metallic elements such as rods, masts, mesh conductors or catenary wires intended to intercept lightning flashes

3.8

down-conductor system

part of an external LPS intended to conduct lightning current between the air-termination system and the earth-termination system

3.9

ring conductor

conductor forming a loop around the structure and interconnecting the down conductors for distribution of lightning current among them

3.10

earth-termination system

part of an external LPS which is intended to conduct and disperse lightning current into the earth

3.11

earth electrode

part or a group of parts of the earth-termination system which provides direct electrical contact with the earth and disperses lightning current into the earth

3.12**ring earth electrode**

earth electrode forming a closed loop around the structure below or on the surface of the earth

3.13**foundation earth electrode**

conductive part buried in the soil under a building foundation or, preferably, embedded in concrete of a building foundation, generally in the form of a closed loop or mesh

[SOURCE: IEC 60050-826:2022 [3], 826-13-08, modified – "or mesh" has been added.]

3.14**equipotential earth grid**

mat consisting of an array of conductors intended for potential equalization

3.15**natural component**

conductive part of a structure not installed specifically for lightning protection but that can perform the function of one or more parts of the LPS

3.16**connection component**

part of an LPS used to interconnect conductors or connect conductors to other items

Note 1 to entry: Connection components also include bridging components and expansion pieces.

Note 2 to entry: A connection component is also referred to as a connector in some countries.

3.17**fixing component**

part of an LPS which is used to fix the elements of the LPS to the structure to be protected

3.18**metal installation**

extensive metal item in the structure to be protected that can form a path for lightning current

EXAMPLE Pipework, staircases, elevator guide rails, ventilation, heating and air-conditioning ducts, interconnected reinforcing steel, and structural metal parts.

3.19**external conductive part**

metal item entering or leaving the structure to be protected and which can carry a part of the lightning current

EXAMPLE Pipework, metallic cable elements, metal ducts.

3.20**electrical system**

system incorporating low-voltage power supply components

3.21**electronic system**

system incorporating sensitive electronic components such as telecommunication equipment, computer, control and instrumentation systems, and power electronic installations

3.22**internal system**

electrical and electronic systems within a structure

3.23

lightning equipotential bonding

EB

bonding to the LPS of separated conductive parts, by direct connections or via surge protective devices, to reduce potential differences caused by lightning current

3.24

bonding bar

metal bar on which metal installations, external conductive parts, electric power and telecommunication lines and other cables can be bonded to an LPS

3.25

bonding conductor

conductor connecting separated conductive parts to an LPS

3.26

interconnected reinforcing steel

steelwork within a concrete structure which is considered electrically continuous

3.27

dangerous sparking

electrical discharge due to lightning which causes physical damage in the structure to be protected

3.28

separation distance

^s
necessary distance between a conductor carrying partial lightning current and other conductive parts to avoid dangerous sparking

3.29

surge protective device

SPD

device containing at least one non-linear component, intended to limit transient overvoltages and divert surge currents

3.30

test joint

detachable bonding between down conductor and earth lead-in conductor for the measurement of earthing resistance

3.31

test point

point for the measurement of either total earthing resistance or continuity, or both, by electrical connection to a down conductor installed in an inaccessible location

3.32

class of LPS

number denoting the classification of an LPS according to the lightning protection level for which it is designed

3.33

lightning protection designer

specialist competent and skilled in the design of the LPS

3.34

LPS installer

person competent and skilled in the installation of the LPS

3.35**structure with a risk of explosion**

structure with hazardous areas as determined in accordance with IEC 60079-10-1 and IEC 60079-10-2 or containing explosive materials

3.36**isolating spark gap****ISG**

component designed to interconnect electrically-isolated conductive sections when the potential difference between the sections exceeds the rated breakdown voltage

3.37**solid explosive material**

solid chemical compound, mixture, or device with explosion as its primary or common purpose

3.38**Zone 0**

area in which an explosive gas atmosphere is present continuously, or for long periods, or frequently

[SOURCE: IEC 60079-10-1:2020, 3.3.4]

3.39**Zone 1**

area in which an explosive gas atmosphere is likely to occur occasionally in normal operation

[SOURCE: IEC 60079-10-1:2020, 3.3.5]

3.40**Zone 2**

area in which an explosive gas atmosphere is not likely to occur in normal operation, but, if it does occur, will exist for a short period only

[SOURCE: IEC 60079-10-1:2020, 3.3.6]

3.41**Zone 20**

place in which an explosive atmosphere, in the form of a cloud of combustible dust in air, is present continuously, or for long periods or frequently

[SOURCE: IEC 60079-10-2:2015, 3.25.1, modified – "explosive dust atmosphere" has been replaced with "explosive atmosphere" and "a cloud of dust in air" has been replaced with "a cloud of combustible dust in air".]

3.42**Zone 21**

place in which an explosive atmosphere, in the form of a cloud of combustible dust in air, is likely to occur in normal operation occasionally

[SOURCE: IEC 60079-10-2:2015, 3.25.2, modified – "explosive dust atmosphere" has been replaced with "explosive atmosphere" and "a cloud of dust in air" has been replaced with "a cloud of combustible dust in air".]

3.43

Zone 22

place in which an explosive atmosphere, in the form of a cloud of combustible dust in air, is not likely to occur in normal operation but, if it does occur, will persist for a short period only

[SOURCE: IEC 60079-10-2:2015, 3.25.3, modified – "area" has been replaced with "place", "explosive dust atmosphere" has been replaced with "explosive atmosphere" and the Note to entry has been deleted.]

3.44

sliding contact

<for floating roof tank> device that moves up and down with the floating roof for the purpose of making contact between the roof and tank shell to conduct the short and intermediate components of a lightning strike

Note 1 to entry: Common types of sliding contacts are shunts and shoes.

3.45

fixed contact

<for floating roof tank> device providing a contact between a floating roof and the tank shell installed to conduct the intermediate and long-duration current component of a lightning strike

Note 1 to entry: The most common type of fixed contact for floating roofs is a bypass conductor.

4 Lightning protection system (LPS)

4.1 Class of LPS

The characteristics of an LPS are determined by the characteristics of the structure to be protected and by the considered lightning protection level.

Four classes of LPS (I to IV), as shown in Table 1, are defined in this document, corresponding to lightning protection levels defined in IEC 62305-1.

Table 1 – Relation between lightning protection levels (LPL) and class of LPS (see IEC 62305-1)

LPL	Class of LPS
I	I
II	II
III	III
IV	IV

Each class of LPS is characterized by the following:

a) Data dependent upon the class of LPS:

- lightning parameters (see IEC 62305-1:2024, Table 3 and Table 4);
- rolling sphere radius, mesh size and protection angle (see 5.2.2);
- distances between down conductors (see 5.3.3);
- separation distance against dangerous sparking (see 6.3);
- minimum length of earth electrodes (see 5.4.2);
- connection components (see 5.5.3);
- selection of SPD or ISG for lightning equipotential bonding (see 6.2).

b) Factors not dependent upon the class of LPS:

- minimum thickness of metal sheets or metal pipes in air-termination systems (see 5.2.5);
- LPS materials and conditions of use (see 5.5);
- material, configuration and minimum dimensions for air terminations, down conductors and earth terminations (see 5.6) and equipotential bonding conductors connecting different bonding bars or connecting bonding bars to the earth-termination system (see Table 9);
- conductors connecting internal metal installations to the bonding bar (see Table 10);
- lightning equipotential bonding via metallic conductors.

The class of the required LPS should be selected on the basis of a risk assessment (see IEC 62305-2).

The probability of the performance of each class of LPS is given in IEC 62305-2:—, Annex B.

4.2 Design of the LPS

A technically and economically optimized design of an LPS is possible, especially if the steps in the design and construction of the LPS are coordinated with the steps in the design and construction of the structure to be protected. In particular, the design of the structure itself should utilize the natural components of the structure as parts of the LPS.

The design documentation of an LPS shall contain all the information necessary to ensure a correct and complete installation. For detailed information, see Annex D.

The LPS should be designed and installed by well-trained and expert (or certified) LPS designers and installers (see D.4.1).

The design of the class and location of the LPS for existing structures shall take into account the constraints of the existing situation.

5 External lightning protection system

5.1 General

5.1.1 Application of an external LPS

The external LPS is intended to intercept direct lightning flashes to the structure, including flashes to the side of the structure, and conduct the lightning current from the point of strike to ground. The external LPS is also intended to disperse this current into the earth without causing thermal or mechanical damage, or dangerous sparking which can trigger fire or explosions.

5.1.2 Application of an isolated LPS or an electrically insulated LPS

In most cases, the external LPS can be attached to the structure to be protected.

An isolated LPS or an electrically insulated LPS should be considered when the thermal and explosive effects at the point of strike, or on the conductors carrying the lightning current, can cause damage to the structure or to its contents (see Annex D). Typical examples include structures with combustible coverings, structures with combustible walls and areas at risk of explosion and fire.

NOTE 1 The use of an isolated LPS can be convenient where it is expected that future changes in the structure, its contents or its use will require modifications to the LPS.

An isolated LPS should also be considered when the susceptibility of the contents warrants the reduction of the radiated electromagnetic field associated with the lightning current pulse in the down conductor.

An isolated LPS or an electrically insulated LPS should also be considered if partial lightning currents entering the structure can interfere with or destroy sensitive electrical or electronic equipment.

NOTE 2 See more information in IEC 62305-4.

5.1.3 Use of natural components

Natural components made of conductive materials, which will always remain in or on the structure and will not be modified (e.g. interconnected steel-reinforcement, metal framework of the structure and metal sheets) can be used as parts of an LPS. When using natural components as part of an LPS, the risk of damage to the natural components shall be considered.

Other natural components can only be considered as being additional to an LPS.

NOTE For further information, see Annex D.

5.2 Air-termination systems

5.2.1 General

The probability of lightning current penetrating a structure is decreased considerably by the presence of a properly designed air-termination system.

Air-termination systems can be composed of any combination of the following elements:

- a) rods (including free-standing masts);
- b) catenary wires;
- c) meshed conductors.

To conform to this document, all types of air-termination systems shall be positioned in accordance with 5.2.2 and 5.2.3. All types of air terminals shall comply in full with this document.

For all types of air terminals only the real physical dimensions of the metal air-termination systems shall be used for the determination of the volume protected.

The individual air-termination rods should be connected together at roof level to ensure current division.

Radioactive air terminals are not allowed.

5.2.2 Positioning

5.2.2.1 General methods

Air-termination components installed on a structure shall be located at roof level on corners, exposed points and edges and the structure's horizontal and vertical protrusions in accordance with one or more of the following methods.

NOTE Research indicates that the probability of strikes to the vertical side of a structure of less than 60 m in height is low enough that taking it into consideration is not necessary.

Acceptable methods to be used in determining the position of the air-termination system include:

- the rolling sphere method;
- the protection angle method;
- the mesh method.

The rolling sphere method is the general procedure suitable in all cases.

The protection angle method is a supplementary procedure to the rolling sphere method suitable for simple-shaped parts of buildings but it is subject to limits of air-termination height indicated in Figure 1.

The mesh method is a suitable procedure of protection where plane surfaces shall be protected.

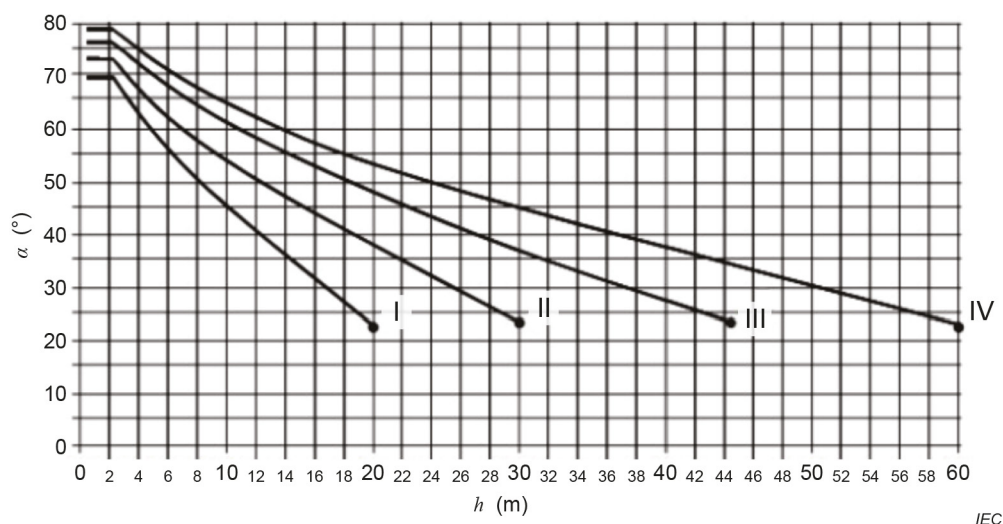
The values for the rolling sphere radius, mesh size and protection angle for each class of LPS are given in Table 2 and Figure 1.

Detailed information on the positioning of the air-termination system is given in Annex D.

Table 2 – Values of rolling sphere radius, mesh size and protection angle corresponding to the class of LPS

Class of LPS	Protection method		
	Rolling sphere radius r m	Mesh cell size w_m m	Protection angle α °
I	20	5 × 5	See Figure 1 below.
II	30	10 × 10	
III	45	15 × 15	
IV	60	20 × 20	

One dimension of the mesh cell given in Table 2 can be increased by a maximum of +25 %, provided the mesh cell perimeter is not increased.



NOTE 1 The protection angle method is not applicable beyond the values marked with • in this Figure 1. Only the rolling sphere and mesh methods apply in these cases.

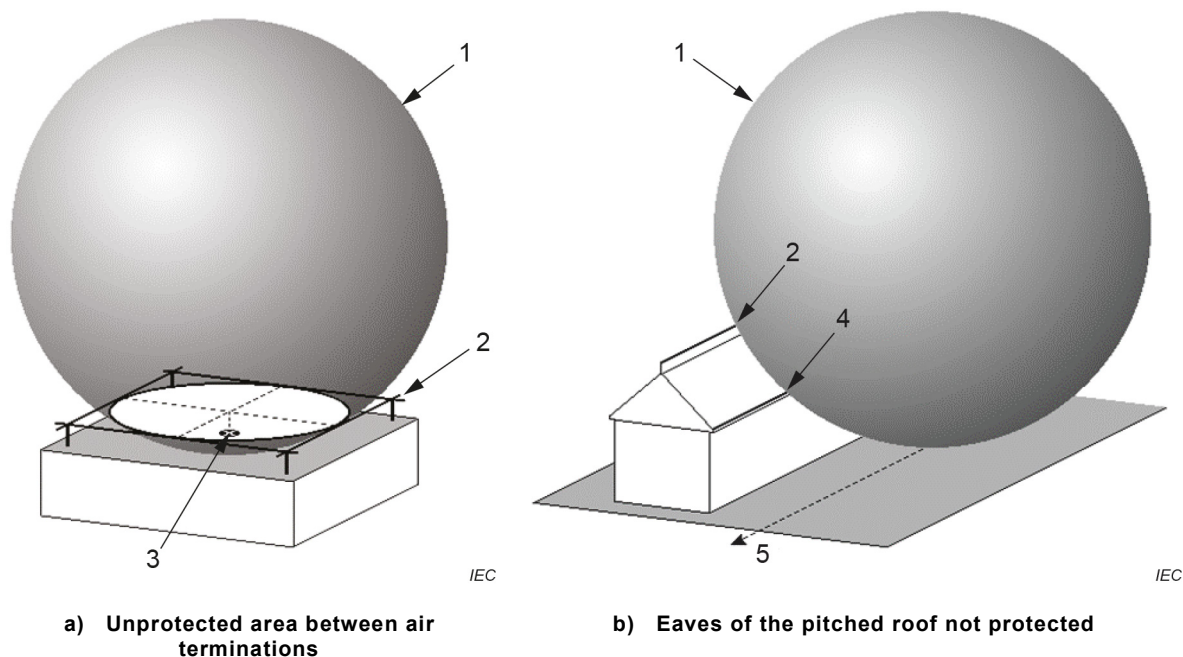
NOTE 2 h is the reference height of an air termination above the reference plane of the area to be protected.

NOTE 3 The angle will not change for values of h below 2 m.

Figure 1 – Protection angle corresponding to the class of LPS

5.2.2.2 Positioning of the air-termination system utilizing the rolling sphere method

Applying this method, the positioning of the air-termination system is adequate if it can prevent a fictive sphere from touching the structure to be protected when the sphere approaches from any possible direction (see Figure 2 a) and Figure 2 b)). Figure 2 a) shows the unprotected area between four air-termination points while Figure 2 b) shows the eaves of the pitched roof are not protected by the air termination on the ridge of the structure.



Key

- 1 rolling sphere
- 2 air termination
- 3 contact point (shall be avoided)
- 4 contact line (shall be avoided)
- 5 rolling direction

Figure 2 – Contacting the rolling sphere with the structure to be protected

5.2.2.3 Positioning the air-termination system when utilizing the protection angle method

5.2.2.3.1 General

The position of the air-termination system is considered to be adequate if the considered part of the structure to be protected is fully situated within the protected volume provided by the air-termination system.

The protection angle depends on the class of LPS and on the reference height of the air termination as given in Table 2.

The reference height is the height between the reference plane and the top of the air termination.

The reference plane can be:

- the ground level which can be considered as the reference plane in all cases, or
- any other horizontal plane surface which is protected.

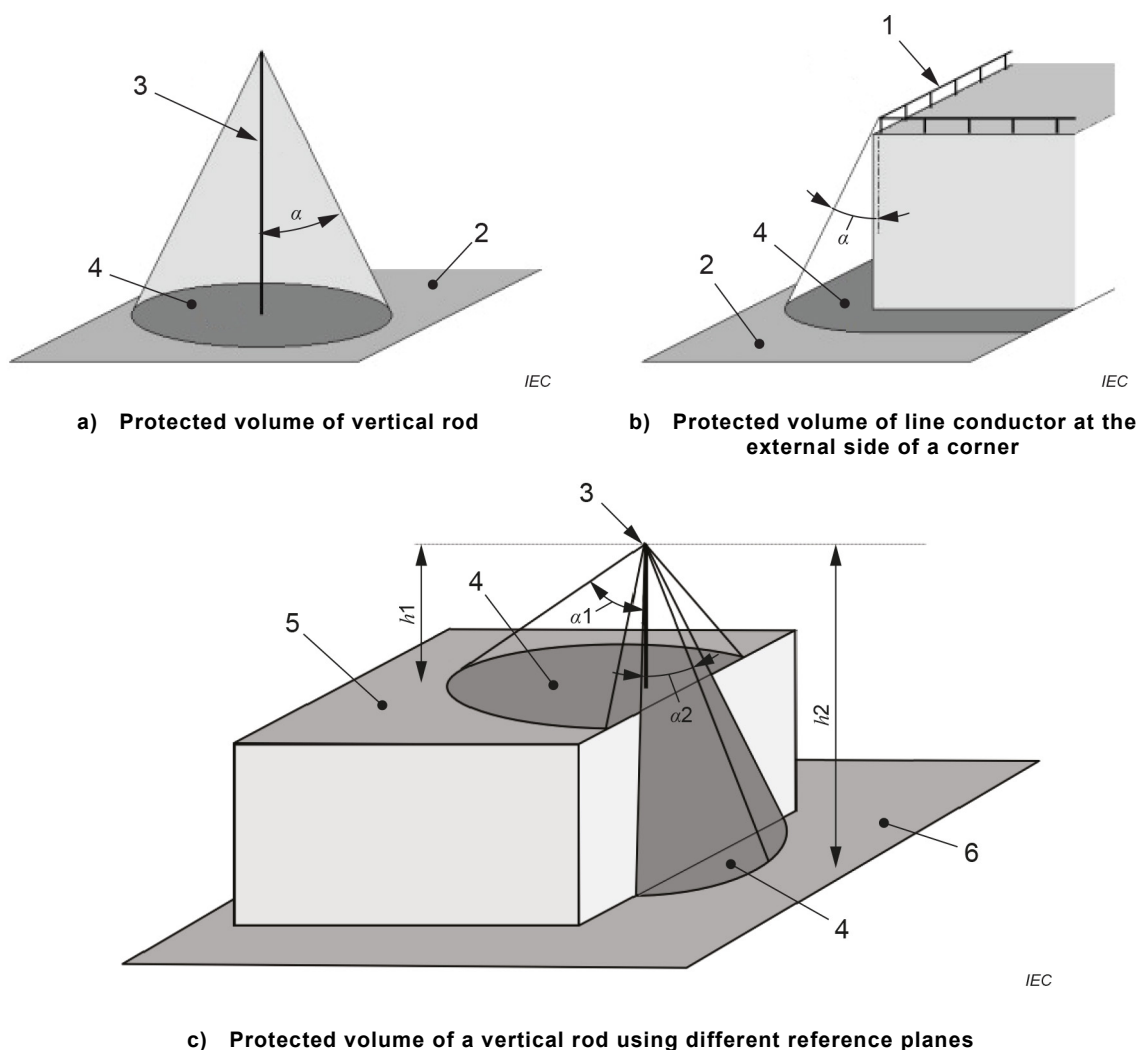
The protection angle is applicable up to, but excluding, the physical edges of an elevated reference plane, such as a roof. At the edges the protection angle appropriate to a lower reference plane such as another protected horizontal plane or the ground shall be used.

The application of the protection angle method is reported in 5.2.2.3.2.

NOTE The hypotenuse associated with the protection angle is a line approximating the appropriate curve of a rolling sphere. The reference plane is the surface on which the rolling sphere would rest.

5.2.2.3.2 Volume protected by rod-type air termination

The volume protected by a vertical or near vertical rod is represented by a straight line rotating from the tip of the air termination around an axis perpendicular to the reference plane at an angle from this axis equal to the protection angle. The shape of the protected volume in the simple case shown in Figure 3 a) is a vertical cone or in the case involving two reference planes, two segments of cones, as shown in Figure 3 c).



Key

- 1 air-termination conductor
- 2 reference plane (α)
- 3 air-termination rod
- 4 protected area
- 5 reference plane for h_1 (α_1)
- 6 reference plane for h_2 (α_2)

Figure 3 – Application of the protection angle method

5.2.2.3.3 Volume protected by line-type air termination

A horizontal line air termination provides a protected volume described in two parts. Along the side of a regular structure the protected volume is represented by a straight line in the plane of the protection angle, moving along the horizontal air-termination conductors, and containing the protection angle. At a corner it is represented by a quarter of a cone with the semi-angle equal to the protection angle, having its base in the reference plane. An example of the protected volume is given in Figure 3 b).

5.2.2.4 Positioning of the air-termination system utilizing the mesh method

For the purposes of protecting flat surfaces, a mesh system is considered to protect the whole surface provided all of the following conditions are fulfilled:

- a) Air-termination conductors are positioned
- on roof edge lines,
 - on roof overhangs,
 - on roof ridge lines, if the slope of the roof exceeds 1/10.

NOTE 1 The mesh method is suitable for horizontal and inclined roofs.

NOTE 2 The mesh method is suitable for lateral surfaces to protect against flashes to the side of the structure.

- b) The mesh dimensions meet the values given in Table 2.

NOTE 3 Damage to a mesh air termination due to snow slabs on roofs with a slope exceeding 1/10 is minimized by the use of parallel air-termination conductors instead of a mesh with a spacing between the conductors not greater than the required mesh width. Subclause 6.3.1 provides a general approach to calculate the separation distance. See a more detailed explanation in D.5.2.2.4.

- c) The network of the air-termination system is constructed in such a way that the lightning current will always encounter at least two distinct metal routes to the earth termination.
- d) No installation protrudes outside the volume protected by air-termination systems.

NOTE 4 Further information can be found in Annex D.

- e) Metal installations at earth potential on the surface of the roof are required to be protected by an air termination if they do not meet the requirements for a natural air termination.
- f) The air-termination conductors follow, as far as possible, the shortest and most direct route.

NOTE 5 Air terminations installed below the highest probable water level can cause damages.

5.2.3 Air terminations against flashes to the side of tall structures

Lateral impacts of flashes to the side of tall structures are considered as negligible for structures up to 60 m in height measured from ground level. However, elements significantly protruding the facade can be endangered (e.g. balconies, cameras, antennas).

On structures taller than 60 m, flashes to the side can occur, especially to protruding parts, and to corners and edges of facades.

NOTE 1 In general, the risk due to these flashes is low because only a few per cent of all flashes to tall structures will be to the side and their parameters are significantly lower than those of flashes to the top of structures. However, electrical and electronic equipment on walls outside structures can be destroyed even by lightning flashes with low current peak values.

An air-termination system shall be installed to protect significant protrusions (such as balconies, viewing platforms) on vertical surfaces on the upper part of tall structures (i.e. typically the topmost 20 % of the height of the structure), as well as the equipment installed on them (see Annex D). For parts of the upper 20 % that do not exceed 60 m above ground level, protection of the vertical surface is optional.

NOTE 2 Elements protruding through the facade of structures up to 60 m in height are rarely endangered.

NOTE 3 In the United States ground level is also called local grade.

NOTE 4 More information on the protection of protruding parts on tall structures is given in Annex D.

5.2.4 Construction

The air terminations of an attached LPS shall be installed as follows.

- If the roof is made of non-combustible material, the air-termination conductors can be positioned on the surface of the roof.

NOTE 1 Criteria for non-combustible material is given in ISO 1182 [4] as class A1, A2.

NOTE 2 Examples of non-combustible building elements are steel frame walls with masonry in-fill, brickwork, blockwork, ceramic tiles, metal sheathing, built-up roof with gravel, seamed metal panels, concrete slabs, steel and glass.

- If the roof is made of normal-flammable material, the air-termination conductors can be positioned on the surface of the roof, provided their temperature rise due to the passage of lightning current is not dangerous for the material of the roof.

NOTE 3 Criteria for normal-flammable material, class B through class E follow ISO 11925-2 [5], with reference for classification to EN 13501-1 [6].

NOTE 4 Examples of normal-flammable building elements are wooden rafters, wooden-framed walls, floors, roof deck, wooden sheets and single-ply plastic membranes.

NOTE 5 For temperature rise see IEC 62305-1:2024, Table D.3.

- Adequate distance shall be maintained between the roof made of easily-flammable material and the air-termination conductors. For thatched roofs, where no steel bars are used for mounting of the reed, a distance of at least 0,15 m is adequate. For other easily-flammable materials, a distance not lower than 0,10 m is considered adequate.
- Easily-flammable parts of the structure to be protected shall not remain in direct contact with the conductors of an external LPS and shall not remain directly under any metallic roofing membrane that can be punctured by a lightning flash (see 5.2.5).

NOTE 6 Criteria for easily-flammable material, class F, follow ISO 11925-2, with reference for classification to EN 13501-1.

NOTE 7 Examples of easily-flammable parts of the structure are those made of textile materials, wood (thinner than 3 mm) or paper.

NOTE 8 National rules regulating construction work and the erection of structures are sometimes used as other criteria to describe non-, normal- and easily-flammable materials.

Account shall also be taken of less flammable membranes such as wooden sheets (see also D.5.2.4).

5.2.5 Natural components

Natural components can be of high technical benefit for lightning protection, for example by reducing induction effects and reducing the necessary separation distance.

The use of natural components can give rise to damage, hot spot or ignition problems. The suitability of natural components as LPS shall be considered if the temperature rise of the inner surface at the point of strike does not constitute a danger. Hot spot or ignition problems can be less likely to occur when the metal sheets lie inside an LPZ 0_B or higher. For the LPZ concept refer to IEC 62305-1.

The following parts of a structure should be considered and can be used as natural air-termination components in accordance with 5.1.3.

- a) Metal sheets covering the structure to be protected provided that the electrical current path has been made durable for transferring the lightning current (e.g. by means of brazing, welding, crimping, seaming, screwing or bolting). Any connection not tested on the basis of IEC 62561-1 shall be evaluated by the designer and the installer of the LPS for its ability to perform as a natural air-termination. This risk can be evaluated and assessed by analysing the physical effects of lightning, described in IEC 62305-1.

A type test based on IEC 62561-1:2017⁴ shall include at least:

- i) a reference to IEC 62561-1:2017, 6.3 relating to ageing (exceptions can be insulated coated material as well as the usage in concrete or material indoors);
- ii) a reference to IEC 62561-1:2017, 6.4 relating to lightning impulse current criteria a) and b);
- iii) description of the method and the connection configuration in which it is necessary for the connection to be made at the construction site;
- iv) description of the required qualification (if any is required). The installer on site shall have the qualification to repeat the quality of the test sample;
- v) description of all materials and dimensions of the connection including the natural conductors;
 - the thickness of the metal sheet is not less than the value t' given in Table 3 if it is not important to prevent puncture of the sheeting or to consider ignition of any readily- combustible materials or explosive atmosphere underneath;
 - the thickness of the metal sheet is not less than the value t given in Table 3 if it is necessary to take precautions against puncture;
 - the thickness of the metal sheet is not less than the value t'' given in Table 4 if it is necessary to take precautions against puncture and to consider hot spot problems;
 - they are not coated with insulating material;
 - for interception purposes, a thin coating of protective paint (max. 0,2 mm) or thin coating of PVC (max. 0,5 mm), or asphalt (max. 1 mm) is not regarded as insulator – it will be penetrated at the point of strike;
 - for electrical continuity purposes a thin coating of protective paint (max. 0,2 mm) is not regarded as insulator – it will be penetrated at the contact area of the connection. However, such a thin coating may cause arcing.

**Table 3 – Minimum thickness of metal sheets or metal pipes
in air-termination systems**

Class of LPS	Material	Thickness ^a t mm	Thickness ^b t' mm
I to IV	Lead	–	2,0
	Steel (stainless, galvanized)	4	0,5
	Titanium	4	0,5
	Copper	5	0,5
	Aluminium	7	0,65
	Zinc	–	0,7
^a t prevents puncture.			
^b t' applies if it is not important to prevent puncture, hot spot or ignition problems.			

⁴ Withdrawn.

Table 4 – Maximum temperature rises ΔT (K) of inner surface and time duration t_{50} (s) for different thickness t'' (mm) and long strokes according to LPL I ($Q_{\text{LONG}} = 200 \text{ C}$)

Metal	Maximum temperature rises ΔT					t_{50}^a s
	For thickness t'' of 3 mm	For thickness t'' of 4 mm	For thickness t'' of 5 mm	For thickness t'' of 6 mm	For thickness t'' of 7 mm	
Copper	1 050	890	670	520	430	0,65
Brass	860	730	550	400	290	0,80
Aluminium	640	630	590	520	440	0,95
Steel (St37)	1 430	1 080	830	660	520	3,6
Stainless steel (V2A)	1 360	940	620	410	290	8,0

NOTE 1 The values given in this table are only valid to process equipment operating near atmospheric pressure. In practice this precludes application to items other than tanks.

NOTE 2 If the metals are coated with a thermally insulating material at the inner surface, the temperatures do not exceed 200 °C for sheets with at least 4 mm thickness and 260 °C for sheets with 3 mm thickness. The coating can consist of polytetrafluoroethylene (PTFE) or rubber with 2 mm thickness.

^a t_{50} indicates that a value of 50 % of the given maximum temperature rise is exceeded for the given time. The given time is a typical time valid for all thicknesses of the sheets.

- b) Metal components of roof construction (trusses, interconnected reinforcing steel, etc.), underneath non-metallic roofing, provided any damage to this non-metallic roofing is acceptable.
- c) Metal parts such as ornamentation, railings, coverings of parapets, with cross-sections not less than that specified for standard air-termination components.
- d) Metal pipes and tanks on the roof, provided that they are constructed of material with thicknesses and cross-sections in accordance with Table 7.
- e) Metal pipes and tanks carrying readily-combustible or explosive mixtures, provided that they are constructed of material with a thickness not less than the appropriate value of t given in Table 3 and that the temperature rise of the inner surface at the point of strike (see Table 4) does not constitute a danger (for detailed information, see Annex C).

If the conditions for thickness are not fulfilled, the pipes and tanks shall be included in the protected volume.

Piping and tanks carrying readily-combustible or explosive mixtures (e.g. pipes or ducts of exhaust or extraction systems) shall not be considered as an air-termination natural component if the gasket in the flange sides is neither metallic nor otherwise properly bonded.

The possibility of puncture and material loss caused by a direct strike should be considered because of reduction in the compressive strength of the pipe.

NOTE CLC/TS 50703-1 [7] includes requirements for metal sheet joint tests in Europe.

5.3 Down-conductor systems

5.3.1 General

To reduce the probability of damage due to lightning current flowing in the LPS, the down conductors shall be arranged in such a way that from the point of strike to earth:

- a) several parallel current paths exist;
- b) the length of the current paths is kept to a minimum;
- c) equipotential bonding to conducting parts of the structure is performed according to the requirements of 6.2.

NOTE 1 Lateral connection of down conductors is considered good practice.

The geometry of the down conductors and of the ring conductors affects the separation distance (see 6.3).

NOTE 2 The installation of as many down conductors as possible, at equal spacing around the perimeter interconnected by ring conductors, reduces the probability of dangerous sparking and facilitates the protection of internal installations (see IEC 62305-4). This condition is fulfilled in metal framework structures and in reinforced concrete structures in which the interconnected steel is electrically continuous.

Preferred values of the distance between down conductors are given in Table 5.

More information on partitioning of the lightning current amongst down conductors is given in Annex B.

5.3.2 Positioning of an isolated LPS

When positioning an isolated LPS system, the separation distance shall always be kept. The positioning of down conductors meets the minimum location requirements under the following conditions:

- a) If the air termination consists of rods on a separated mast(s) not made of metal or steel reinforced concrete, at least one down conductor is required for each mast. Where masts are made of metal or steel reinforced concrete, the mast can be used as the down conductor and no additional down conductors are required.
- b) If the air termination consists of catenary wires (or one wire), at least one down conductor is necessary at each supporting structure.
- c) If the air termination forms a network of conductors, at least one down conductor is necessary at each supporting wire end.

5.3.3 Positioning of an attached LPS

For each attached LPS the number of down conductors shall be not less than two and should be distributed around the perimeter of the structure to be protected, subject to architectural and practical constraints.

NOTE 1 Planning of the down-conductor layout is important for structures with complex geometry.

Equal spacing of the down conductors is preferred around the perimeter of an air-termination system. Preferred values of the distance between down conductors are given in Table 5.

**Table 5 – Preferred values of the distance between down conductors
by LPS according to the class of LPS**

Class of LPS	Distances m
I	10
II	10
III	15
IV	20

A down conductor should be installed at each exposed corner of the structure, where this is possible.

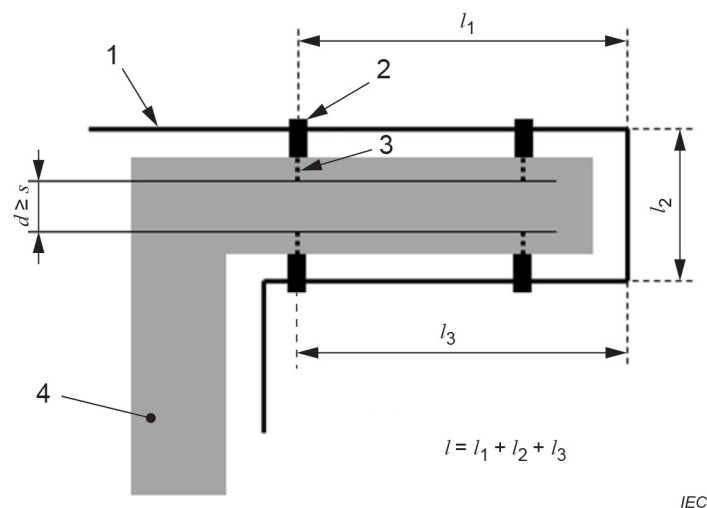
NOTE 2 Further information on the application of an electrically insulated LPS, with respect to the equivalent separation distance, is under consideration. A future International standard is being developed: IEC 62561-8 [8]⁵.

5.3.4 Construction

The down conductors shall be installed such that, as far as practicable, they form a direct continuation of the air-termination conductors.

Down conductors shall be installed as straight and vertical as practicable, to provide the shortest and most direct path to earth; but where this is not possible, the minimum distance between any two points of a down conductor loop (1) including its fixing components (2 and 3) shall not be less than the separation distance ' s ' (from 6.3, using conductor length ' l ' between the points). See Figure 4.

⁵ Under consideration.

**Key**

1 down conductor

2 fastener

3 metal screw to fix fastener

4 structure

 s separation distance d shortest distance between conducting parts at the point of consideration

NOTE In the case of reinforced concrete the separation distance can be calculated differently.

Figure 4 – Loop in a down conductor

NOTE 1 In the United States, no bend of an LPS conductor shall form an included angle of less than 90°, nor have a bend radius less than 200 mm.

Down conductors, even if covered in insulating material, shall not be installed in gutters or down spouts.

NOTE 2 The effects of moisture in the gutters lead to intensive corrosion of the down conductor.

It is recommended that the down conductors be positioned such that a separation distance in accordance with 6.3 is provided between them and any doors and windows.

Down conductors of an LPS attached to the structure to be protected shall be installed as follows:

- if the wall is made of non-combustible material, the down conductors can be positioned on the surface or in the wall;
- if the wall is made of normal-flammable material the down conductors can be positioned on the surface of the wall, provided that their temperature rise due to the passage of lightning current is not dangerous for the material of the wall;

NOTE 3 For classification of non-combustible, normal-flammable and easily-flammable materials see 5.2.4.

NOTE 4 For temperature rise see also IEC 62305-1:2024, Table D.3

- if the wall is made of easily-flammable material and the temperature rise of down conductors is dangerous, the down conductors shall be placed in such a way that the distance between them and the wall is always greater than 0,1 m. Mounting brackets can be in contact with the wall.

When the distance from the down conductor to an easily-flammable material cannot be ensured, the cross-section of steel (regular steel and stainless steel) or thermal equivalent conductor shall be not less than 100 mm².

5.3.5 Natural components

The following parts of the structure can be used as natural down conductors:

a) the metal installations, provided that all following conditions are fulfilled:

- the electrical current path shall be made durable against mechanical and environmental stresses, and be capable of withstanding the lightning current (e.g. by means of brazing, welding, crimping, seaming, screwing or bolting). Any natural down conductor and connections not tested according to 5.2.5 a) shall be evaluated by the designer and the installer of the LPS to assess the probability that the natural component and associated connections can withstand lightning currents at the point of installation;
- their dimensions are at least equal to that specified in Table 7 for standard down conductors.

Piping carrying readily-combustible or explosive mixtures (e.g. pipes or ducts of exhaust or extraction systems) shall not be considered as a down-conductor natural component if the gasket in the flange sides is neither metallic nor otherwise properly bonded.

NOTE 1 Metal installations can be clad with insulating material or anti-corrosion coating.

NOTE 2 In the United States, connections to metal framework used as a natural down conductor are made using bonding plates having a surface contact area of not less than 5 200 mm² or by welding or brazing.

b) the metal of the electrically-continuous reinforced concrete framework of the structure, provided that at least one of the following conditions is fulfilled:

- the steelwork within reinforced concrete structures is electrically continuous, which is valid if the major interconnections of vertical and horizontal bars are welded, clamped, connected using lightning protection system components (LPSC) or overlapped and bound for a minimum length of 20 times their diameter; or otherwise securely connected (see Figure D.23);
- the connections between reinforcement elements are specified by the designer or installer, in cooperation with the builder and the civil engineer;
- the electrical continuity of the reinforcing bars is verified by an electrical test for structures utilizing steel-reinforced concrete (including pre-cast, pre-stressed reinforced units), where the designer or installer has not specified the connections between reinforcement elements. If it is not practical to conduct such testing, the reinforcing steel shall not be used as a natural down conductor (see D.5.3.5.2). In this case a dedicated down-conductor system shall be installed and bonded to the steel-reinforcement bars in the concrete at the top and bottom levels;

NOTE 4 More information is given in Annex D.

- the electrical continuity of the reinforcing steel in structures made of pre-cast reinforced concrete is ensured between individual adjacent pre-cast concrete units;
- clamps and other connectors used to form the continuity of steelwork in reinforced concrete comply with IEC 62561-1;

NOTE 5 For further information on the continuity of steelwork in reinforced concrete structures, see Annex D.

With prefabricated reinforced concrete, it is important to establish interconnection points between the reinforcing elements. It is also important that reinforced concrete contains a conductive connection between the interconnection points. The individual parts should be connected on-site during assembly (see Annex D).

NOTE 6 In the case of pre-stressed concrete, the risk of causing unacceptable mechanical consequences is present, due either to lightning current or as a result of the connection to the lightning protection system.

c) the interconnected steel framework of the structure;

NOTE 7 Ring conductors are not necessary if the metal framework of steel structures or interconnected reinforcing steel of the structure is used as down conductors.

- d) the facade elements, profile rails and metallic sub-constructions of facades, provided that all following conditions are fulfilled:
- their dimensions conform to the requirements for down conductors (see 5.6.2) and that for metal sheets or metal pipes thicknesses are not less than 0,5 mm;
 - their electrical continuity in a vertical direction conforms to the requirements of 5.5.3. Any connection not tested according to 5.2.5 a) can be used upon accepting the risk of being damaged due to lightning current and shall be evaluated by the designer and installer of the LPS.

NOTE 8 For more information, see Annex D.

5.3.6 Test joints and test points

At the connection of the earth termination, a test joint should be fitted on each down conductor, except in the case of embedded components used as down conductors combined with foundation earth electrodes.

For down conductors embedded in concrete or using other natural components only a test point is required.

For measuring purposes, the joint shall be capable of being opened with the aid of a tool. In normal use, it shall remain closed.

Test joints shall be able to conduct lightning current and to withstand the electrodynamic forces produced by the lightning current.

To fulfil the above requirements the test joints shall be tested according to 5.5.

5.4 Earth-termination system

5.4.1 General

When dealing with the dispersion of lightning current (high frequency behaviour) into the ground, whilst minimizing any potentially dangerous overvoltages, the shape and dimensions of the earth-termination system are important criteria. In general, a low earthing resistance (if possible lower than 10 Ω when measured at low frequency) of the LPS earth-termination system is recommended.

NOTE 1 Adding additional earthing electrodes or using earthing enhancing compounds according to IEC 62561-7 are methods available to reduce the earthing resistance, if necessary.

For protection against lightning, a single integrated earth-termination system is necessary and is suitable for all purposes (i.e. lightning protection, power systems and telecommunication systems, electronic and computer systems).

Earth-termination systems shall be bonded in accordance with the requirements of 6.2.

NOTE 2 Lightning equipotential bonding between the LPS earth-termination system and other earthing systems can be achieved via natural components in accordance with 5.3.5 and 5.5.3.

NOTE 3 Serious corrosion problems can occur when earthing systems made of different materials are connected to each other.

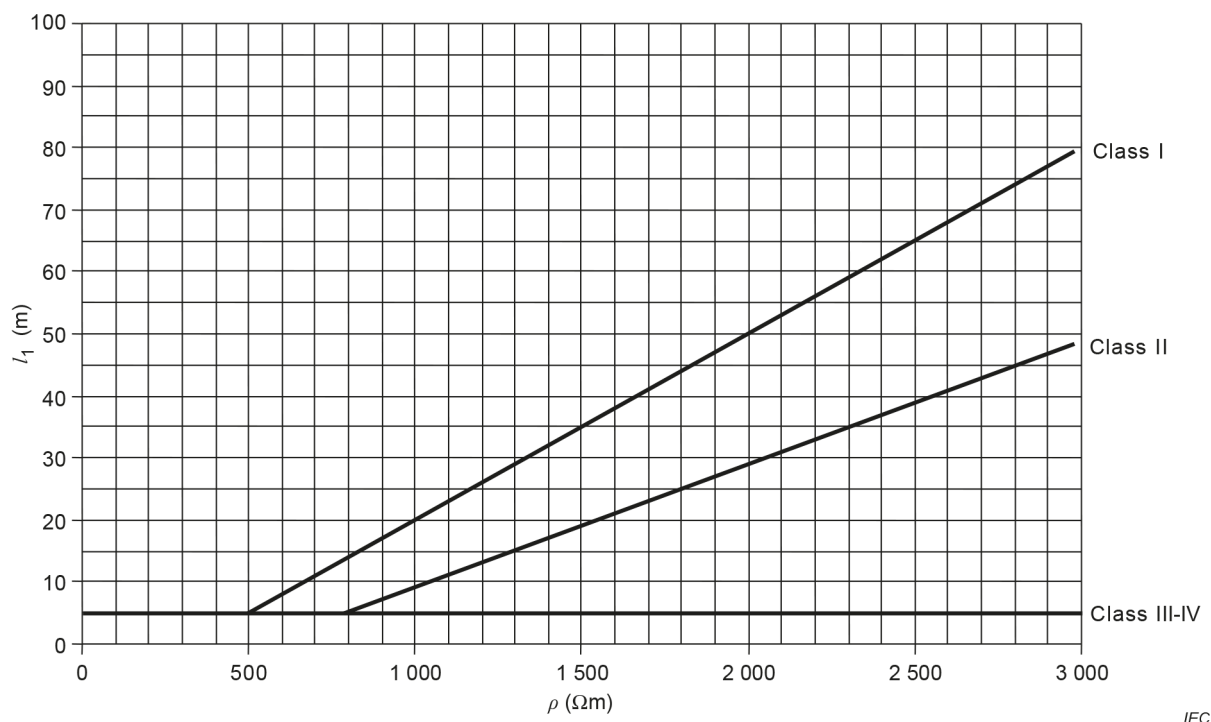
5.4.2 Earthing arrangement in general conditions

5.4.2.1 General

For the earth-termination arrangement, two basic types of earth electrode arrangements apply.

5.4.2.2 Type A arrangement

This type of arrangement comprises horizontal or vertical earth electrodes installed outside the structure to be protected, connected to each down conductor or foundation earth electrodes, not forming a closed loop. In Type A arrangements, the total number of earth electrodes shall be not less than two.



NOTE 1 Classes III and IV are independent of soil resistivity.

NOTE 2 The soil resistivity of interest is that measured to the depth to which the earth electrodes are buried.

Figure 5 – Minimum length l_1 of each earth electrode according to the class of LPS

The minimum length of each earth electrode at the base of each down conductor is

- l_1 for horizontal electrodes, or
- $0,5 l_1$ for vertical (or inclined) electrodes,

where l_1 is the minimum length of each earth electrode shown in the relevant part of Figure 5.

NOTE 1 In the United States, based on the requirements of NFPA 780: Standard for the Installation of Lightning Protection Systems [9] and practical experience in the use of horizontal earth electrodes, the minimum length of horizontal earth electrodes is not required to be twice that required for vertical electrodes.

For combined (vertical or horizontal) electrodes, the total length shall be considered.

The minimum lengths stated in Figure 5 can be disregarded provided that an earthing resistance of the Type A arrangement less than 10Ω (measured at a frequency different from the power frequency and its multiple to avoid possible interference) is achieved.

NOTE 2 When the above-mentioned requirements cannot be met, a Type B earth arrangement can be used.

NOTE 3 Reduction of earthing resistance by the extension of earth electrodes is practically convenient up to 60 m.

NOTE 4 In soil with resistivity higher than $3\,000 \Omega \cdot m$, Type B earth arrangements or earthing enhancing compounds are effective.

NOTE 5 In soil with resistivity less than $200 \Omega \cdot \text{m}$, earthing enhancing compounds are not effective.

NOTE 6 In soil with low resistivity, corrosion of the earth electrode can be considered. Refer to IEC 62561-7 for more information.

NOTE 7 For further information, refer to Annex D.

5.4.2.3 Type B arrangement

This type of arrangement comprises either a ring conductor external to the structure to be protected, in contact with the soil for at least 80 % of its total length, or a foundation earth electrode forming a closed loop. Such earth electrodes may also be meshed.

Although it is possible that 20 % of its total length is not in contact with the soil, the ring conductor shall always be completely connected throughout its total length.

For the ring earth electrode (or foundation earth electrode), the effective radius r_e of the area enclosed by the ring earth electrode (or foundation earth electrode) shall be not less than the value l_1 (see D.5.4.2.3.2 for details on the calculation of r_e):

$$r_e \geq l_1 \quad (1)$$

where l_1 is represented in Figure 5 according to LPS class I, II, III or IV.

When the required value of l_1 is larger than the convenient value of r_e , additional horizontal or vertical (or inclined) electrodes shall be added with individual lengths l_r (horizontal) and l_v (vertical) given by the following equations:

$$l_r = l_1 - r_e \quad (2)$$

and
$$l_v = (l_1 - r_e) / 2 \quad (3)$$

It is recommended that the number of additional electrodes should be not less than the number of the down conductors. A minimum of two additional electrodes is required.

The additional electrodes should be connected to the ring earth electrode at points where the down conductors are connected and, for as many as possible, equidistantly.

5.4.3 Installation of earth electrodes

The ring earth electrode (Type B arrangement) should preferably be buried at a depth of at least 0,5 m and at a distance of about 1 m away from the external walls.

The earth electrodes (Type A arrangement) shall be installed at a depth at least 0,5 m to the top of the electrode and distributed as uniformly as possible to minimize electrical coupling effects in the earth.

NOTE 1 If the top of a Type A earth electrode is positioned within an inspection housing, or is located below a high resistance material e.g. tarmac, then the 0,5 m requirement can be disregarded.

Earth electrodes shall be installed in such a way as to allow inspection during construction.

The embedded depth and the type of earth electrodes shall be such as to minimize the effects of corrosion, soil drying and freezing to stabilize the earth resistance. The upper part of a vertical earth electrode located in the depth of drying and freezing soil should not be regarded as being effective under dry and frosty conditions. For every vertical electrode, 0,5 m should be added to the value of the length l_1 , calculated in 5.4.2.2 and 5.4.2.3.

For bare solid rock, a ring-type electrode earthing arrangement is recommended.

For structures with extensive electronic systems or with high risk of fire, a Type B earthing arrangement is preferable.

In the case of a Type B arrangement foundation earthing system embedded in concrete, the earth electrode shall be correctly connected at least every 2 m with the reinforcement steel.

NOTE 2 Connection between the foundation electrode and the reinforcement steel is often made at intervals lower than 2 m for mechanical support.

NOTE 3 In Germany, foundation earthing systems are erected according to the National Standard DIN 18014 [10].

5.4.4 Natural earth electrodes

Interconnected reinforcing steel in concrete foundations in accordance with 5.6, or other suitable underground metal structures, should be used as an earth electrode. When the metallic reinforcement in concrete is used as an earth electrode, ensure the interconnections to prevent splitting of the concrete.

NOTE 1 In the case of pre-stressed concrete, the passage of lightning discharge currents can produce unacceptable mechanical stresses.

NOTE 2 If a foundation earth electrode inside waterproof concrete is used, a long-term increase in earthing resistance is possible.

NOTE 3 In the United States, reinforcing steel in concrete foundations is not the preferred electrode due to probable lack of ability to confirm interconnection quality and lack of sufficient access to the earthing system.

5.5 Components

5.5.1 General

Components of the LPS (air-termination rods, conductors, earth electrodes, connections components, isolating spark gaps, conductor fasteners, earth electrode inspection houses and electrode seals, lightning strike event counters, earthing enhancing compounds, components for isolated LPS) shall withstand the electromagnetic effects of lightning current and predictable stresses without being damaged. This shall be achieved by using components that have been successfully tested in accordance with the relevant part of the IEC 62561 series.

Components of an LPS shall be manufactured from the materials listed in Table 6 or from other materials with equivalent mechanical, electrical and chemical (corrosion) performance characteristics.

Mechanical and electrical characteristics as well as corrosion resistance properties shall meet the requirements of the IEC 62561 series.

NOTE 1 In the United States, components used shall be certified to Underwriters Laboratories Standard UL 96 [11].

NOTE 2 Components made of material other than metal can be used for fixing.

Table 6 – LPS materials and conditions of use^a

Material	Use			Corrosion		
	In open air	In earth	In concrete	Resistance	Increased by	Can be destroyed by galvanic coupling with
Copper	Solid Stranded	Solid Stranded As coating	Solid Stranded As coating	Good in many environments	Sulphur compounds Organic materials	-
Hot galvanized steel ^{c d e}	Solid Stranded ^b	Solid	Solid Stranded ^b	Acceptable in air, in concrete and in benign soil	High chlorides content	Copper
Steel with electro-deposited copper ^f	Solid	Solid	Solid	Good in many environments	Sulphur compounds	
Stainless steel	Solid Stranded	Solid Stranded	Solid Stranded	Good in many environments	High chlorides content	–
Aluminium ^h	Solid Stranded	Not allowed	Not allowed	Good in atmospheres containing low concentrations of sulphur and chloride	Alkaline solutions	Copper
Lead ^{f g}	Solid As coating	Solid As coating	Not allowed	Good in atmospheres with high concentration of sulphates	Acid soils	Copper Stainless steel
^a This table gives general guidance only. In special circumstances, more careful corrosion immunity considerations are required (see Annex D). ^b Stranded conductors are more vulnerable to corrosion than solid conductors. Stranded conductors are also vulnerable where they enter or exit concrete positions. This is the reason why stranded galvanized steel is not recommended in earth. ^c Galvanized steel can be corroded in clay soil or moist soil. ^d Galvanized steel in concrete should not extend into the soil due to possible corrosion of the steel just outside the concrete. ^e Galvanized steel in contact with reinforcement steel in concrete should not be used in coastal areas where there can be salt in the ground water. ^f Underground connections in soil which require removal of conductor coatings is not recommended without adequate post corrosion protection. ^g Use of lead in the earth is often banned or restricted due to environmental concerns. ^h To avoid corrosion, bare aluminium and aluminium alloy should not be used in direct contact with soil, gravel, limestone or lime mortar.						

5.5.2 Fixing

Air terminations and down conductors shall be firmly fixed so that the electrodynamic or accidental mechanical forces (for instance wind, vibrations, slipping of slabs of snow, thermal expansion) will not cause conductors to break or loosen (see Annex D).

The conductor fasteners shall comply with IEC 62561-4.

NOTE 1 Suggested distances between fixing components are reported in Table D.1.

NOTE 2 In the United States, conductors are fixed to the structure upon which they are placed at intervals not exceeding 1 m.

5.5.3 Connections

The number of connections along the conductors shall be kept to a minimum.

The classes N and H of IEC 62561-1 of connection components (LPSCs – components installed specifically for lightning protection) shall be selected as follows:

- class H tested components for LPS class I and class II;
All connections before current sharing should be performed with two connectors in parallel.
- class N tested components for LPS class III and class IV;
All connections before current sharing should be performed with two connectors in parallel or one connector tested to class H.

Detailed calculation may also be used.

NOTE If there is a clamp with parameters corresponding to the lightning current of the class of the LPS (200 kA, 150 kA, 100 kA) tested according to IEC 62561-1, it can be installed in an LPS with the equal class of the LPS.

5.5.4 Components of an electrically insulated LPS

Insulating components, such as insulating stand-offs and insulating down conductors shall meet the requirements of IEC TS 62561-8⁶.

5.6 Materials and dimensions

5.6.1 Materials

Material and its dimensions shall be chosen considering the effects of corrosion either of the structure to be protected or of the LPS and shall comply with the requirements and tests according to the IEC 62561 series.

5.6.2 Dimensions

Configurations and minimum cross-sectional areas of air-termination conductors, air-termination rods, down conductors and earth lead-in conductors are given in Table 7 and shall comply with the requirements and tests according to IEC 62561-2.

Configurations and minimum dimensions of earth electrodes are given in Table 8 and shall comply with the requirements and tests according to IEC 62561-2.

Assessment of environmental conditions (e.g. expected wind load) shall be considered during the dimensioning of air-termination rods.

⁶ IEC TS 62561-8 will be replaced by a future International standard IEC 62561-8.

Table 7 – Material, configuration and minimum cross-sectional area of air-termination conductors, air-termination rods, earth lead-in conductors and down conductors^{a e f}

Material	Configuration	Cross-sectional area mm ²
Copper, Tin-plated copper	Solid tape	50
	Solid round ^b	50
	Stranded Rope lay conductor Smooth weave stranded conductor	50
	Solid round ^c	176
Aluminium	Solid tape	70
	Solid round	50
	Stranded Rope lay conductor Smooth weave stranded conductor	50
Aluminium alloy	Solid tape	50
	Solid round	50
	Stranded Rope lay conductor Smooth weave stranded conductor	50
	Solid round ^c	176
Copper-coated aluminium alloy	Solid round	50
Hot dipped galvanized steel	Solid tape	50
	Solid round	50
	Stranded	50
	Solid round ^c	176
Copper-coated steel Tin-plated copper-coated steel	Solid round	50
	Solid tape	50
Stainless steel ^g	Solid tape ^d	50
	Solid round	50
	Stranded Rope lay conductor Smooth weave stranded conductor	70
	Solid round ^c	176
Copper-clad steel	Solid round ^c	176

NOTE In France stranded conductors cannot be used as down conductors.

^a Mechanical and electrical characteristics, as well as corrosion resistance properties, shall meet the requirements of IEC 62561-2.

^b 50 mm² (8 mm diameter) can be reduced to 28 mm² (6 mm diameter) in certain applications where mechanical strength is not an essential requirement. Consideration should, in this case, be given to reducing the spacing between the fasteners.

^c Applicable for air-termination rods and earth lead-in conductor (except for aluminium and aluminium alloy in earth lead-in conductor). For air-termination rods where mechanical stress such as wind loading is not critical, a 9,5 mm diameter, 1 m long rod can be used.

^d If thermal and mechanical considerations are important then these values should be increased to 75 mm².

^e If the earth lead-in conductor is partially installed in soil it shall fulfill the requirements of Table 8.

^f If an insulating down conductor has been successfully tested according to IEC TS 62561-8:2018, 5.5.7 (electrical tests) the cross-sectional area can be reduced to the tested cross-sectional area.

^g Chromium ≥ 16 %; nickel ≥ 8 %; carbon ≤ 0,08 %.

Table 8 – Material, configuration and minimum dimensions of earth electrodes^a

Material	Configuration	Dimensions		
		Earth rod diameter mm	Earth conductor mm ²	Earth plate mm
Copper ^g Tin-plated copper	Stranded		50	
	Solid round	15	50	
	Solid tape		50	
	Tubular rod	20		
	Solid plate			500 × 500
	Lattice plate ^c			600 × 600
	Equipotential earth grid			Typical mesh size 250 mm to 500 mm, conductor 4 mm diameter ^h
Hot dipped galvanized steel	Solid round	14	78	
	Tubular rod	25		
	Solid tape		90	
	Solid plate			500 × 500
	Lattice plate ^c			600 × 600
	Profile ^d			
	Equipotential earth grid			Typical mesh size 250 mm to 500 mm, conductor 4 mm diameter ^h
Bare steel ^b	Stranded		70	
	Solid round		78	
	Solid tape		75	
Copper-coated steel ^g Tin-plated copper- coated steel	Solid round	14 ^e	50	
	Solid tape		90	
Stainless steel ^f	Solid round	15 ^e	78	
	Solid tape		100	
	Equipotential earth grid			Typical mesh size 250 mm to 500 mm, conductor 4 mm diameter ^h

NOTE In the United States, only copper, copper-coated steel and stainless steel are acceptable for direct burial.

^a Mechanical and electrical characteristics, as well as corrosion resistance properties, shall meet the requirements of IEC 62561-2.

^b Shall be embedded in concrete for a minimum depth of 50 mm.

^c Lattice plate constructed with a minimum total length of the conductor of 4,8 m (see cross-sections in IEC 62561-2).

^d Different profiles are permitted with a cross-section of 290 mm² and a minimum thickness of 3 mm, e.g. cross profile.

^e In some countries (e.g. United States), the diameter can be reduced to 12,7 mm.

^f Chromium ≥ 16 %, nickel ≥ 5 %, molybdenum ≥ 2 %, carbon ≤ 0,08 %.

^g An earth electrode of copper material buried in the soil shall not be used in contact with the steel members, steel pipes and steel piles related to the building structures because of corrosion considerations.

^h For equipotential earth grids, the dimensions vary depending on the intended area of equipotentialization.

6 Internal lightning protection system

6.1 General

The internal LPS shall prevent the occurrence of dangerous sparking within the structure to be protected due to lightning current flowing in the external LPS or in other conductive parts of the structure.

Dangerous sparking can occur between the external LPS and other components such as:

- metal installations;
- internal systems;
- external conductive parts and lines connected to the structure.

NOTE For protection against overvoltages of internal systems, refer to IEC 62305-4.

Dangerous sparking between different parts can be avoided by means of

- equipotential bonding in accordance with 6.2, or
- separation distance between the parts in accordance with 6.3.

6.2 Lightning equipotential bonding

6.2.1 General

Equipotentialization is achieved by interconnecting the LPS with

- metal installations,
- internal systems,
- external conductive parts and lines connected to the structure.

When lightning equipotential bonding is established to internal systems, part of the lightning current can flow into such systems and this effect shall be taken into account.

Interconnecting means can be

- bonding conductors, where the electrical continuity is not provided by natural bonding,
- surge protective devices (SPDs), where direct connections with bonding conductors are not feasible,
- isolating spark gaps (ISGs), where direct connections with bonding conductors are not allowed.

The manner in which lightning equipotential bonding is achieved is important and shall be discussed with the operator of the telecommunication network, the electric power, gas pipes operator, and other operators or authorities concerned, as there can be conflicting requirements.

SPDs shall be installed in such a way that they can be inspected.

When an LPS is installed, metalwork external to the structure to be protected can be affected. This should be considered when designing such systems. Lightning equipotential bonding for external metalwork can also be necessary.

Lightning equipotential bonding should be integrated and coordinated with other equipotential bonding in the structure.

6.2.2 Lightning equipotential bonding for metal installations

In the case of an isolated LPS, lightning equipotential bonding shall be established at ground level only.

For an attached LPS, lightning equipotential bonding shall be installed at the following locations:

- a) In the basement or approximately at ground level. Bonding conductors shall be connected to a bonding bar constructed and installed in such a way that it allows easy access for inspection. The bonding bar shall be connected to the earth-termination system. For large structures (typically more than 20 m in length), a ring bonding bar can be used or more than one bonding bar can be installed, provided that they are interconnected.
- b) Where the separation distance requirements are not fulfilled (see 6.3).

Lightning equipotential bonding connections shall be made as direct and straight as possible.

NOTE 1 When lightning equipotential bonding is established to conducting parts of the structure, part of the lightning current can flow into the structure.

The minimum values of the cross-section of the bonding conductors connecting different bonding bars and of the conductors connecting the bars to the earth-termination system are listed in Table 9.

Table 9 – Minimum dimensions of conductors connecting different bonding bars or connecting bonding bars to the earth-termination system

Class of LPS	Material	Cross-section mm ²
I to IV	Copper	16
	Aluminium	25
	Steel	50
NOTE In Japan, the minimum values of the cross-section are reduced from 16 mm ² to 14 mm ² for copper and 25 mm ² to 22 mm ² for aluminium.		

The minimum values of the cross-section of the bonding conductors connecting internal metal installations to the bonding bars are listed in Table 10.

Table 10 – Minimum dimensions of conductors connecting internal metal installations to the bonding bar

Class of LPS	Material	Cross-section mm ²
I to IV	Copper	6
	Aluminium	10
	Steel	16
NOTE In Japan, the minimum values of the cross-section are reduced from 6 mm ² to 5 mm ² for copper, 10 mm ² to 8 mm ² for aluminium and 16 mm ² to 14 mm ² for steel.		

If insulating pieces are inserted into gas lines or water pipes inside the structure to be protected, they shall, with the agreement of the water and gas supplier, be bridged by ISGs designed for such an operation.

NOTE 2 IEC 60079-14 would require that the ISG is rated for the hazardous areas which can be associated with the means of insulating sections in a gas line or other service carrying flammable liquids.

Lightning equipotential bonding for metal installations shall conform to 5.5.

ISGs shall be tested according to IEC 62561-3 and shall have the following characteristics:

- $I_{\text{imp}} \geq I_F$ where I_F is the lightning current flowing along the relevant part of the external LPS (see IEC 62305-1:2024, Annex B and Annex E),
- rated impulse sparkover voltage U_{imp} (see IEC 62561-3) lower than the impulse withstand level of insulation between parts.

6.2.3 Lightning equipotential bonding for external conductive parts

For external conductive parts, lightning equipotential bonding shall be established as near as possible to the point of entry into the structure to be protected.

Bonding conductors shall be capable of withstanding the part I_F of the lightning current flowing through them evaluated in accordance with IEC 62305-1:2024, Annex E.

If direct bonding is not acceptable, ISGs, tested according to IEC 62561-3, with the following characteristics shall be used:

- $I_{\text{imp}} \geq I_F$ where I_F is the lightning current flowing along the considered external conductive part (see IEC 62305-1:2024, Annex E);
- the rated impulse sparkover voltage U_{imp} (see IEC 62561-3) lower than the impulse withstand level of insulation between parts.

NOTE When equipotential bonding is required, but an LPS is not required according to the risk assessment, the earth termination of the low-voltage electrical installation can be used for this purpose.

6.2.4 Lightning equipotential bonding for internal systems

It is imperative that lightning equipotential bonding is installed in accordance with 6.2.2 a) and 6.2.2 b).

If cables of internal systems are screened or located in metal conduits, it can be sufficient to bond only these screens and conduits (see Annex A).

NOTE 1 It is possible that bonding of screens and conduits does not avoid failure of equipment due to overvoltages in the connected cables. For protection of such equipment refer to IEC 62305-4.

If cables of internal systems are neither screened nor located in metal conduits, they shall be bonded via SPDs.

NOTE 2 For installation of SPDs tested to the requirements of Class I for power lines see also IEC 60364-5-53 and national installation codes.

Bonding conductors shall have the same current withstand as indicated in 6.2.2 for ISGs.

SPDs tested to class I for power lines and SPDs tested to class D1 for telecommunication or signal lines shall be installed. The necessary discharge current requirements of SPDs are assessed according to the methods given in IEC 62305-1 and IEC 62305-4.

SPDs shall comply with IEC 61643-11 and IEC 61643-21 and shall be

- tested with:

$$I_{\text{imp}} \geq (k_c \times I) / 2n' \quad (4)$$

where

$(k_c \times I)$ is the lightning current flowing along the relevant part of the external LPS (see IEC 62305-1:2024, Annex B and Annex E) and

n' is the number of conductors of the cable of an internal system;

- installed and selected with regard to protection level U_p according to IEC 62305-4:2024, Annex C in conjunction with IEC 60364-5-53, IEC 61643-11 and IEC 61643-21.

6.2.5 Lightning equipotential bonding for lines connected to the structure to be protected

Lightning equipotential bonding for electrical and telecommunication lines shall be installed in accordance with 6.2.3.

All the conductors of each line should be bonded directly or with an SPD. Live conductors shall be bonded to the bonding bar via an SPD.

If lines are screened or routed in metal conduits, these screens and conduits shall be bonded. Lightning equipotential bonding for conductors in these screens or conduits is not necessary, provided that the cross-section S_C of these screens or conduits is not lower than the minimum value S_{CMIN} evaluated in accordance with Annex A.

Lightning equipotential bonding of the cable screens or of the conduits shall be performed near the point where they enter the structure.

Bonding conductors shall have the same current withstand as indicated in 6.2.3 for ISGs.

SPDs shall comply with IEC 61643-11 and IEC 61643-21 and shall be:

- tested with $I_{\text{imp}} \geq I_F$ where I_F is the lightning current flowing along the lines (see IEC 62305-1:2024, Annex E);
- installed and selected with regard to the protection level U_p according to IEC 62305-4:2024, Annex C.

NOTE When equipotential bonding is required, but an LPS is not required according to the risk assessment, the earth termination of the low-voltage electrical installation can be used for this purpose.

6.3 Separation distance

6.3.1 General approach

Dangerous sparking between the air termination or the down conductor and the structural metal parts, as well as between the metal installations and the internal systems can be prevented by providing a distance d between the parts greater than the separation distance, s . The general equation for the calculation of s is given by:

$$s = \frac{k_i}{k_m} \times (k_{c1} \times l_1 + k_{c2} \times l_2 + \dots + k_{cn} \times l_n) \quad (5)$$

where

k_i depends on the selected class of LPS (see Table 11);

k_m depends on the electrical insulation material (see Table 12);

$k_{c1, 2, n}$ depends on the (partial) lightning current flowing on the air termination and the down conductor (see Figure B.3 and Figure B.4);

$l_{1, 2, n}$ is the length, in metres, along the air termination and the down conductor from the point where the separation distance shall be considered, to the nearest equipotential bonding point or the earth termination (see Figure B.3 and Figure B.4).

NOTE 1 The length, l , along the air termination can be disregarded in structures with continuous metal roof acting as a natural air-termination system.

When the separation distance, s , by physical distance is not satisfied, an electrically insulated LPS can be used. The equivalent separation distance values for the insulating down conductors shall be taken from the cable manufacturer (see 5.5.4).

The calculated values for the separation distance are valid for a typical air gap. Any other arrangement (including insulating components) shall fulfil the same requirements (i.e. shall show the same protection efficiency) as the air gap.

Table 11 – Separation distance – Values of coefficient k_i

Class of LPS	k_i
I	0,08
II	0,06
III and IV	0,04

Table 12 – Separation distance – Values of coefficient k_m

Material	k_m
Air	1
Concrete, bricks, wood	0,5
NOTE 1 In using other insulating materials, construction guidance and the value of k_m is provided by the manufacturer. For an insulating stand-off consisting of FRP (fibreglass reinforced plastic), PE or PVC, with a minimum length of 0,5 m, $k_m = 0,7$ can be used. For additional information see IEC TS 62561-8. NOTE 2 When there are several insulating materials in series, it is a good practice to use the lower value for k_m.	

In the case of the lines or external conductive parts entering the structure, it is always necessary to ensure lightning equipotential bonding (by direct connection or connection by an SPD) at their point of entry into the structure.

In structures with metallic framework or reinforced concrete framework that is electrically continuous, the following two basic cases shall be considered:

- 1) Each concrete column or steel column, vertically electrically continuously connected, is used as natural down conductor, but no horizontal bonding. In this case the full separation distance s according to 6.3 shall be considered.
- 2) A bonding network according to IEC 62305-4:2024, 5.3 is installed. In this case a separation distance is not required.

The coefficient k_c of the lightning current amongst the air terminations and down conductors depends on the overall number n and the position of the down conductors, on the interconnecting ring conductors and on the type of earth-termination system. The necessary separation distance depends on the voltage drop along the shortest path from the point where the separation distance shall be considered, to the ground electrode or the nearest equipotential bonding point.

NOTE 2 For the calculation of k_c on the individual conductors, detailed calculation or numerical programmes can be used.

6.3.2 Simplified approach

As a simplification of the above approach in 6.3.1 the following formula can be used where only one value of k_c is used:

$$s = \frac{k_i}{k_m} \times k_c \times l \quad (\text{m}) \quad (6)$$

where

- k_i depends on the selected class of LPS (see Table 11);
- k_m depends on the electrical isolation material (see Table 12);
- k_c depends on the (partial) lightning current flowing on the air termination and the down conductor (see Table 13 or Figure B.1 and Figure B.2);
- l is the length, in metres, along the air termination and the down conductor from the point, where the separation distance shall be considered, to the nearest equipotential bonding point or the earth termination (see D.6.3).

For installation of an LPS in higher elevations an altitude correction shall be considered. The correction can be made according to IEC 60071-2 [12].

NOTE 1 If the smaller horizontal dimension of the structure (length or width) does not exceed three times the height, the vertical height of the structure can be used in the determination of the value of l .

Table 13 – Separation distance – Approximated values of coefficient k_c

Number of down conductors n	k_c
1 (only in the case of an isolated LPS)	1
2	0,66
3 and more	0,44
The values of this Table 13 apply for all Type B earthing arrangements and for Type A earthing arrangements, provided that the earth resistances of neighbouring earth electrodes do not differ by more than a factor of 2. If the earth resistances of single earth electrodes differ by more than a factor of 2, $k_c = 1$ shall be assumed.	

7 Maintenance and inspection of an LPS

7.1 General

The LPS should be maintained regularly, to ensure that it does not deteriorate and continues to fulfil the requirements to which it was originally designed.

The effectiveness of any LPS depends on its installation, maintenance, and the testing methods used. Inspections, testing and maintenance shall not be conducted during the threat of thunderstorms.

NOTE Additional information on the inspection and maintenance of LPSs is provided in Clause D.7.

7.2 Maintenance

Regular inspections are among the fundamental conditions for reliable maintenance of an LPS.

The property owners or their designated representative shall be informed by the inspection team of all observed deviations to the standard and they shall be repaired as soon as reasonably practicable.

All maintenance work will be fully recorded and reported to the property owners or their designated representative, to be kept with other information on the LPS.

Any repairs or upgrades to the lightning protection system resulting from change of the structure, its use or its equipment should be carried out in a timely manner.

7.3 Objective of inspections

An LPS tends to lose its effectiveness over the years because of corrosion, weather-related damage, theft, mechanical damage and damage from direct lightning strikes.

The mechanical and electrical characteristics of the LPS should be fully maintained throughout the entire lifetime of the LPS in order to conform to the design requirements of this document.

The objective of the inspections is to ascertain that:

- the LPS (internal and external) conforms to the design based on this document;
- all components of the LPS are in good condition and capable of performing their designed functions, and that there is no corrosion or other damage;
- any recently added or modified services, equipment or constructions, or any modifications on the building or its equipment or its purpose, are addressed into the LPS design.

Inspections of lightning protection systems include visual inspections or electrical testing, or both.

7.4 Need for inspection

Inspections should be made as follows:

- during the construction of the structure, to check the embedded electrodes or other components which will be concealed in the structure and will become inaccessible;
- after the installation of the LPS;
- periodically at such intervals as determined with regard to the nature of the structure to be protected, for example corrosion problems;
- after alterations or repairs;
- when it is known that the structure has been struck by lightning.

NOTE If no alternative exists, pictures of installations that are not accessible upon completion of the installation can be accepted in lieu of inspection after installation. Examples include earthing connections and connections in concealed locations.

During the periodic inspection, it is particularly important to check the following:

- deterioration and corrosion of air-termination elements, conductors and connections;
- earthing resistance (or impedance) value for the earth-termination system;
- condition of connections, equipotential bonding and fixing components.

All inspection and testing work and results shall be fully recorded and reported to the property manager or his designated representative, to be kept with other information on the LPS.

8 Protection measures against injury to human beings due to touch and step voltages

8.1 Protection measures against touch voltages

When, under normal conditions, people are present in the vicinity of the down conductors of an LPS, there can be a hazard to life, even if the LPS has been designed and constructed according to the requirements of this document.

The hazard is reduced to a tolerable level if one of the following conditions is fulfilled:

- a) under normal conditions there are no persons within 3 m of the down conductors;
- b) the "natural" down-conductor system consists of at least 10 columns of the extensive metal framework of the structure or of at least 10 pillars of interconnected steel of the structure, with the electrical continuity ensured;

NOTE 1 In such cases where the minimization of step and touch potential is essential, detailed calculations, for instance by using computer programs, can be performed.

- c) the contact resistance with the soil, within 3 m of the down conductor, is not less than 100 k Ω over an area of a typical footprint (0,02 m²).

NOTE 2 A layer of insulating material, e.g. asphalt, of 5 cm thickness generally reduces the hazard to a tolerable level.

NOTE 3 Contact resistance is as per definition IEC 581-23-08 [13]. Values are measured between a 400 cm² electrode compressed with a uniform force of 750 N and a point where voltage is not modified by current injection.

If none of the conditions are fulfilled, protection measures shall be adopted against injury to human beings due to touch voltages such as one of the following: