



International
Standard

ISO 22762-2

Elastomeric seismic-protection isolators —

Part 2: Applications for bridges — Specifications

*Appareils d'appuis structuraux en élastomère pour protection
sismique —*

Partie 2: Applications pour ponts — Spécifications

Fourth edition
2024-09

Reference number
ISO 22762-2:2024(en)

Full document details: [ISO 22762-2-2024](#)

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Published in Switzerland

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO document should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 45, *Rubber and rubber products*, Subcommittee SC 4, *Products (other than hoses)*.

This fourth edition cancels and replaces the third edition (ISO 22762-2:2018), of which it constitutes a minor revision.

The changes are as follows:

- the relation of this document to ISO 22762-5 and ISO 22762-6 have been added in Introduction;
- the use of the terms "elastomeric isolators" and "seismic isolators" have been made consistent throughout the document;
- the term "fracture" has been replaced by "break" throughout the document;
- modification of [Clause 3](#) to be kept consistent with ISO 22762-1 and ISO 22762-3.

A list of all parts in the ISO 22762 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Introduction

The ISO 22762 series includes two parts related to specifications for elastomeric isolators, i.e. ISO 22762-2 for bridges and ISO 22762-3 for buildings. This is because the elastomeric isolator requirements for bridges and buildings are quite different, although the basic concept of the two products is similar. Therefore, ISO 22762-2 and the relevant clauses in ISO 22762-1 are used when ISO 22762 (all parts) is applied to the design of bridge isolators whereas ISO 22762-3 and the relevant clauses of ISO 22762-1 are used when it is applied to building isolators.

The main differences to be noted between elastomeric isolators for bridges and elastomeric isolators for buildings are the following.

- a) Elastomeric isolators for bridges are mainly rectangular in shape and those for buildings are circular in shape.
- b) Elastomeric isolators for bridges are designed to be used for both rotation and horizontal displacement, while elastomeric isolators for buildings are designed for horizontal displacement only.
- c) Elastomeric isolators for bridges are designed to perform on a daily basis to accommodate length changes of bridges caused by temperature changes as well as during earthquakes, while elastomeric isolators for buildings are designed to perform only during earthquakes.
- d) Elastomeric isolators for bridges are designed to withstand dynamic loads caused by vehicles on a daily basis as well as earthquakes, while elastomeric isolators for buildings are mainly designed to withstand dynamic loads caused by earthquakes only.

For structures other than buildings and bridges (e.g. tanks), the structural engineer uses either ISO 22762-2 or ISO 22762-3, depending on the requirements of the structure.

ISO/TS 22762-4 is a guidance for the use of ISO 22762-3. ISO 22762-5 gives specifications and test methods for sliding seismic-protection isolators which are not specified as elastomeric isolators. ISO 22762-6 gives specifications and test methods for high-durability and high-performance elastomeric isolators. Three grades of requirements for each test item are introduced in ISO 22762-6.

Elastomeric seismic-protection isolators —

Part 2: Applications for bridges — Specifications

1 Scope

This document specifies minimum requirements and test methods for elastomeric seismic isolators used for bridges, as well as rubber material used in the manufacture of such isolators.

It is applicable to elastomeric seismic isolators used to provide bridges with protection from earthquake damage. The isolators covered consist of alternate elastomeric layers and reinforcing steel plates, which are placed between a superstructure and its substructure to provide both flexibility for decoupling structural systems from ground motion and damping capability to reduce displacement at the isolation interface and the transmission of energy from the ground into the structure at the isolation frequency.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 630 (all parts), *Structural steels*

ISO 22762-1:2024, *Elastomeric seismic-protection isolators — Part 1: Test methods*

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

3.1 breaking

rupture of *elastomeric isolator* (3.8) due to compression- (or tension-) shear loading

3.2 buckling

state when *elastomeric isolator* (3.8) lose their stability under compression-shear loading

3.3 compressive properties

K_v
compressive stiffness for all types of rubber bearings

3.4

cover rubber

rubber wrapped around the outside of inner rubber and reinforcing steel plates before or after curing of *elastomeric isolator* (3.8) for the purposes of protecting the inner rubber from deterioration due to oxygen, ozone and other natural elements and protecting the reinforcing plates from corrosion

3.5

design compressive stress

long-term compressive force on the *elastomeric isolator* (3.8) imposed by the structure

3.6

effective loaded area

area sustaining vertical load in *elastomeric isolator* (3.8), which corresponds to the area of reinforcing steel plates

3.7

effective width

<rectangular elastomeric isolator> the smaller of the two side lengths of inner rubber to which direction shear displacement is not restricted

3.8

elastomeric isolator

rubber bearing, for seismic isolation of buildings, bridges and other structures, which consists of multi-layered vulcanized rubber sheets and reinforcing steel plates

EXAMPLE High-damping rubber bearings, linear natural rubber bearings and lead rubber bearings.

3.9

first shape factor

ratio of effectively loaded area to free deformation area of one inner rubber layer between steel plates

3.10

high-damping rubber bearing

HDR

elastomeric isolator (3.8) with relatively high damping properties obtained by special compounding of the rubber and the use of additives

3.11

inner rubber

rubber between multi-layered steel plates inside an *elastomeric isolator* (3.8)

3.12

lead rubber bearing

LRB

elastomeric isolator (3.8) whose *inner rubber* (3.11) with a lead plug or lead plugs press fitted into a hole or holes of the elastomeric isolator body to achieve damping properties

3.13

linear natural rubber bearing

LNR

elastomeric isolator (3.8) with linear shear force-displacement characteristics and relatively low damping properties, fabricated using natural rubber

Note 1 to entry: Any bearing with relatively low damping can be treated as an LNR bearing for the purposes of elastomeric isolator testing.

3.14

maximum compressive stress

peak stress acting briefly on *elastomeric isolator* (3.8) in compressive direction during an earthquake

3.15**nominal compressive stress**

long-term stress acting on *elastomeric isolator* (3.8) in compressive direction as recommended by the manufacturer for the elastomeric isolator, including the safety margin

3.16**roll-out**

instability of an elastomeric isolator with either dowelled or recessed connection under shear displacement

3.17**routine test**

test for quality control of the production elastomeric isolators during and after manufacturing

3.18**second shape factor**

<circular elastomeric isolator> ratio of the diameter of the inner rubber to the total thickness of the inner rubber

3.19**second shape factor**

<rectangular or square elastomeric isolator> ratio of the effective width of the inner rubber to the total thickness of the inner rubber

3.20**shear properties**

comprehensive term that covers characteristics determined from elastomeric isolator tests:

- shear stiffness, K_h , for LNR;
- shear stiffness, K_h , and equivalent damping ratio, h_{eq} , for HDR and LRB;
- post-yield stiffness, K_d , and characteristic strength, Q_d , for LRB

3.21**structural engineer**

engineer who is in charge of designing the structure for seismically isolated bridges or buildings and is responsible for specifying the requirements for *elastomeric isolators* (3.8)

3.22**type test**

test for verification either of material properties and elastomeric isolator performances during development of the product or that project design parameters are achieved

3.23**ultimate properties**

properties at either buckling, breaking, or roll-out of an elastomeric isolator under compression-shear loading (see [Annex D](#)).

4 Symbols

For the purposes of this document, the symbols given in [Table 1](#) apply.

Table 1 — Symbols and descriptions

Symbol	Description
A	effective plan area; plan area of elastomeric isolator, excluding cover rubber portion
A_b	effective area of bolt
A_e	overlap area between the top and bottom elastomer area of elastomeric isolator
A_{free}	load-free area of elastomeric isolator
A_{load}	Loaded area of elastomeric isolator

Table 1 (continued)

Symbol	Description
A_p	area of the lead plug for a lead rubber bearing
a	Side length of square elastomeric isolator, excluding cover rubber thickness, or length in longitudinal direction of rectangular elastomeric isolator, excluding cover rubber thickness
a_e	length of the shorter side of the rectangular elastomeric isolator, including cover rubber thickness
a'	length in longitudinal direction of the rectangular elastomeric isolator, including cover rubber thickness
B	effective width for bending of flange
b	length in transverse direction of the rectangular elastomeric isolator, excluding cover rubber thickness
b'	length in transverse direction of the rectangular elastomeric isolator, including cover rubber thickness
c	distance from centre of bolt hole to effective flange section
D'	outer diameter of circular elastomeric isolator, including cover rubber
D_f	diameter of flange
d_i	inner diameter of reinforcing steel plate
d_k	diameter of bolt hole
d_0	outer diameter of reinforcing steel plate
E_{ap}	apparent Young's modulus of bonded rubber layer
E_c	apparent Young's modulus corrected, if necessary, by allowing for compressibility
E_c^s	apparent Young's modulus corrected for bulk compressibility depending on its shape factor (S_1)
E_∞	bulk modulus of rubber
E_0	Young's modulus of rubber
F_u	tensile force on elastomeric isolator by uplift
G	shear modulus
$G_{eq}(\gamma)$	equivalent linear shear modulus as a function of shear strain
H	height of elastomeric isolator, including mounting flange
H_n	height of elastomeric isolator, excluding mounting flange
h_{eq}	equivalent damping ratio
$h_{eq}(\gamma)$	equivalent damping ratio as a function of shear strain
K_d	post-yield stiffness (tangential stiffness after yielding of lead plug) of lead rubber bearing
K_h	shear stiffness
K_i	initial shear stiffness
K_p	shear stiffness of lead plug inserted in lead rubber bearing
K_r	shear stiffness of lead rubber bearing before inserting lead plug
K_t	tangential shear stiffness
K_v	compressive stiffness
L_f	length of one side of a rectangular flange
M	resistance to rotation
M_f	moment acting on bolt
M_r	moment acting on elastomeric isolator
n	number of rubber layers
n_b	number of fixing bolts
P	compressive force
P_0	design compressive force in absence of seismic action effects
P_{max}	maximum compressive force including seismic action effects
P_{min}	minimum compressive force including seismic actions effects (the minimum may be negative; ie the minimum force may be tensile)
Q	shear force

Table 1 (continued)

Symbol	Description
Q_b	shear force at breaking
Q_{buk}	shear force at buckling
Q_d	characteristic strength
S_1	first shape factor
S_2	second shape factor
T	temperature
T_0	standard temperature, 23 °C or 27 °C; where specified tolerance is ± 2 °C, T_0 is standard laboratory temperature
T_r	total rubber thickness, given by $T_r = n \times t_r$
t_r	thickness of one rubber layer
t_{r1}, t_{r2}	thickness of rubber layer laminated on each side of plate
t_s	thickness of one reinforcing steel plate
t_0	thickness of outside cover rubber
$U(\gamma)$	function giving ratio of characteristic strength to maximum shear force of a loop
v	loading velocity
W_d	energy dissipated per cycle
X	shear displacement
X_0	design shear displacement
X_b	shear displacement at breaking
X_{buk}	shear displacement at buckling
X_s	shear displacement due to quasi-static shear movement
X_{max}	maximum shear displacement
X_d	shear displacement due to dynamic shear movement
Y	compressive displacement
Z	section modulus of flange
α	coefficient of linear thermal expansion
γ	shear strain
γ_0	design shear strain
γ_a	upper limit of the total of design strains on elastomeric isolators
γ_b	shear strain at breaking
γ_c	local shear strain due to compressive force
γ_d	shear strain due to dynamic shear movement
γ_{max}	maximum design shear strain during earthquake
γ_r	local shear strain due to rotation
γ_s	shear strain due to quasi-static shear movement
γ_u	ultimate shear strain
δ_H	horizontal offset of elastomeric isolator
δ_v	difference in elastomeric isolator height measured between two points at opposite extremes of the elastomeric isolator
ε	compressive strain of rubber
ε_{cr}	compressive creep strain
ε_T	tensile strain of elastomeric isolator
ε_{Tb}	tensile-breaking strain of elastomeric isolator
ε_{Ty}	tensile-yield strain of elastomeric isolator
ζ	ratio of total height of rubber and steel layers to total rubber height

Table 1 (continued)

Symbol	Description
θ	rotation angle of elastomeric isolator about the diameter of a circular bearing or about an axis through a rectangular bearing
θ_a	rotation angle of elastomeric isolator in the longitudinal direction (a)
θ_b	rotation angle of elastomeric isolator in the transverse direction (b)
λ	correction factor for calculation of stress in reinforcing steel plates
η	correction factor for calculation of critical stress
κ	correction factor for apparent Young's modulus according to hardness
$\Sigma\gamma$	total local shear strain
σ	compressive stress in elastomeric isolator
σ_0	design compressive stress
σ_B	tensile stress in bolt
σ_b	bending stress in flange
σ_{bf}	allowable bending stress in steel
σ_{cr}	critical compressive stress in elastomeric isolator
σ_f	allowable tensile stress in steel
σ_{max}	maximum design compressive stress
σ_{min}	minimum design compressive stress
σ_{nom}	for building: nominal compressive stress recommended by manufacturer
σ_s	tensile stress in reinforcing steel plate
σ_{sa}	allowable tensile stress in steel plate
σ_{sy}	yield stress of steel for flanges and reinforcing steel plates
σ_{su}	tensile strength of steel for flanges and reinforcing steel plates
σ_t	tensile stress
σ_{te}	allowable tensile stress in elastomeric isolator
τ_B	shear stress in bolt
τ_f	allowable shear stress in steel
ϕ	factor for computation of buckling stability
ξ	factor for computation of critical stress

5 Classification

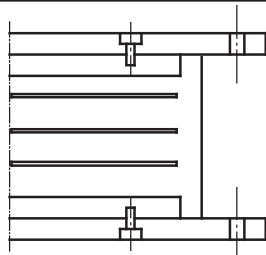
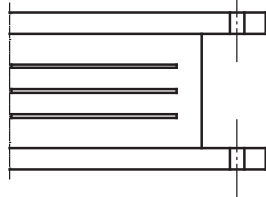
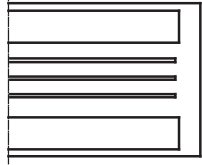
5.1 General

Elastomeric isolators are classified by construction, their ultimate properties and tolerances on their performance.

5.2 Classification by construction

Elastomeric isolators are classified by construction, as shown in [Table 2](#). The structural engineer shall specify which construction is to be used.

Table 2 — Classification by construction

Type	Construction	Illustration
Type I	Mounting flanges are bolted to connecting flange plates, which are bonded to the laminated rubber.	
Type II	Mounting flanges are directly bonded to the laminated rubber.	
Type III	Elastomeric isolators without mounting flanges	

5.3 Classification by tolerances on shear stiffness

Elastomeric isolators may be classified by their tolerance on shear stiffness, as shown in [Table 3](#). The structural engineer shall specify the tolerance required.

Table 3 — Classification by tolerance on shear stiffness

Class	Tolerance %
S-A	±10
S-B	±20

6 Requirements

6.1 General

Elastomeric isolators for bridges and the materials used in their manufacture shall meet the requirements specified in this clause. For test items (see [Table 4](#)) that have no specific required values, the manufacturer shall define the values and inform the purchaser prior to production.

The standard temperature for determining the properties of elastomeric isolators is 23 °C or 27 °C in accordance with prevailing International Standards. However, it is advisable to establish a range of working temperatures, taking into consideration actual environmental temperatures and possible changes in temperature at the work site where the elastomeric isolators are installed.

6.2 Type tests and routine tests

6.2.1 Testing to be carried out on elastomeric isolators is classified into type tests, and routine tests.

6.2.2 Type tests shall be conducted either to ensure that project design parameters have been achieved (in which case the test results shall be submitted to the structural engineer for review prior to production) or

to verify elastomeric isolator performance and material properties during development of the product. The test piece for each type test shall be full-scale or one of the options specified in [Table 4](#). The test piece shall not have been subjected to any previous test programme. The tests shall be performed on test pieces not subjected to any scragging, unless the production elastomeric isolators are to be supplied after scragging. In that case, the test pieces shall be subjected to the same scragging procedure as the production elastomeric isolators

6.2.3 Previous type test results may be substituted, provided the following conditions are met.

- a) Elastomeric isolators are fabricated in a similar manner and from the same compound and adhesive.
- b) All corresponding external and internal dimensions are within 10 % of each other.
- c) The second shape factors are within ± 10 %.
- d) The test conditions such as maximum and minimum vertical load applied in the ultimate property test, as described in [6.5.7](#), are more severe.

Table 4 — Tests on products

Properties	Test item	Test method	Routine test	Type test	Test piece ^a
Compressive properties Rotation performance	Compressive stiffness Compressive displacement	ISO 22762-1:2024, 6.2.1, method 1	X	X	Full-scale only
Shear properties	Shear stiffness Equivalent damping ratio Post-yield stiffness (for LRB) Characteristic strength (for LRB)	ISO 22762-1:2024, 6.2.2	X	X	Full-scale only
Tensile properties	Tensile breaking strength Shear strain	ISO 22762-1:2024, 6.5	N/A	Opt.	Scale B
Dependence of shear properties	Shear strain dependence	ISO 22762-1:2024, 6.3.1	N/A	X	Scale B
	Compressive stress dependence	ISO 22762-1:2024, 6.3.2	N/A	Opt.	Scale B
	Frequency dependence	ISO 22762-1:2024, 6.3.3 ISO 22762-1:2024, 5.8	N/A	X(m)	Scale A, STD, SBS
	Repeated loading dependence	ISO 22762-1:2024, 6.3.4	N/A	X	Scale B
X: Test to be conducted with elastomeric isolators. X(m): Test can be conducted either with elastomeric isolators or with shear-block test pieces. N/A: Not applicable. Opt.: Optional. Scale A: Scaling such that, for a circular bearing, diameter ≥ 150 mm, for a rectangular bearing, side length ≥ 100 mm and, for both types, rubber layer thickness $\geq 1,5$ mm and thickness of reinforcing steel plates $\geq 0,5$ mm. Scale B: Scaling such that, for a circular bearing, diameter ≥ 450 mm, for a rectangular bearing, side length ≥ 400 mm and, for both types, rubber layer thickness $\geq 1,5$ mm and thickness of reinforcing steel plates $\geq 0,5$ mm. STD: Standard test piece (see ISO 22762-1:2024, Tables 12 and 13). SBS: Shear-block test piece specified in ISO 22762-1:2024, 5.8.3. With LRB, SBS shall only be used for ageing tests. ^a Test piece may in all cases be a full-scale elastomeric isolator. This column indicates other options, where these exist.					

Table 4 (continued)

Properties	Test item	Test method	Routine test	Type test	Test piece ^a
	Temperature dependence	ISO 22762-1:2024, 6.3.5 ISO 22762-1:2024, 5.8	N/A	X(m)	Scale A, STD, SBS
Shear displacement capacity	Breaking strain Buckling strain Roll-out strain	ISO 22762-1:2024, 6.4	N/A	X	Scale B
Durability	Ageing	ISO 22762-1:2024, 6.6.1 ISO 22762-1:2024, 5.8	N/A	X(m)	Scale A, STD, SBS
	Creep	ISO 22762-1:2024, 6.6.2	N/A	X	Scale A
Cyclic compressive fatigue	Shear stiffness	ISO 22762-1:2024, 6.6.3	N/A	X	Scale B
Reaction force characteristics at low-rate deformation	Shear stiffness or shear force	ISO 22762-1:2024, 6.7	N/A	Opt.	Scale A
X: Test to be conducted with elastomeric isolators. X(m): Test can be conducted either with elastomeric isolators or with shear-block test pieces. N/A: Not applicable. Opt.: Optional. Scale A: Scaling such that, for a circular bearing, diameter ≥ 150 mm, for a rectangular bearing, side length ≥ 100 mm and, for both types, rubber layer thickness $\geq 1,5$ mm and thickness of reinforcing steel plates $\geq 0,5$ mm. Scale B: Scaling such that, for a circular bearing, diameter ≥ 450 mm, for a rectangular bearing, side length ≥ 400 mm and, for both types, rubber layer thickness $\geq 1,5$ mm and thickness of reinforcing steel plates $\geq 0,5$ mm. STD: Standard test piece (see ISO 22762-1:2024, Tables 12 and 13). SBS: Shear-block test piece specified in ISO 22762-1:2024, 5.8.3. With LRB, SBS shall only be used for ageing tests. ^a Test piece may in all cases be a full-scale elastomeric isolator. This column indicates other options, where these exist.					

6.2.4 Routine tests are carried out during production for quality control. Sampling is allowed for routine testing. Sampling shall be conducted randomly and cover not less than 20 % of the production of any elastomeric isolator design. For a given project, tests shall cover not less than four test pieces for each size and not less than 20 test pieces in total. If elastomeric isolators are supplied after scragging, the routine test shall be performed on scragged elastomeric isolators.

6.3 Functional requirements

6.3.1 Elastomeric isolators for bridges have the conventional basic functions of bridge rubber bearings, such as supporting the weight of the structure and live loads, absorbing the expansion, contraction, rotation and deflection of the superstructure. In addition, elastomeric isolators have more sophisticated functions in order to improve the deformation performance characteristics of superstructures, regulate the inherent period of superstructures, and effectively distribute inertial forces and reduce vibration energies using the spring and shock damping performance of rubber materials or a combination of rubber materials and lead plugs.

6.3.2 The elastomeric isolators shall function correctly when they are subjected to normal environmental conditions and maintenance, during an economically reasonable design service life. Where exceptional environmental and application conditions are encountered, additional precautions shall be taken. The conditions shall then be precisely defined.

6.3.3 Although seismic rubber bearings are designed to accommodate shear movements, they should not be used to provide permanent resistance to a constantly applied shear force.

6.3.4 Some caution is necessary if bearings are designed to accommodate tensile forces. The limiting values are given in [Annex C](#).

6.4 Design compressive force and design shear displacement

The design stress and strain of an elastomeric isolator are defined by the following relationships between the design force and the displacement:

$$\sigma_0 = \frac{P_0}{A}, \sigma_{\max} = \frac{P_{\max}}{A_e}, \sigma_{\min} = \frac{P_{\min}}{A}$$

and

$$\gamma_0 = \frac{X_0}{T_r}, \gamma_{\max} = \frac{X_{\max}}{T_r}$$

The design compressive forces P_0 , $P_{\max}$ and $P_{\min}$ and design shear displacements X_0 and $X_{\max}$ for an elastomeric isolator shall be provided by the structural engineer.

6.5 Performance requirements

6.5.1 General

The elastomeric isolators shall be tested and the results recorded using the specified test methods. They shall satisfy the requirements listed below. The design value for each elastomeric isolator shall be specified prior to the tests. The test items are summarized in [Table 4](#), which indicates the type tests that are optional, where a scaled elastomeric isolator or a material test piece may substitute an elastomeric isolator, and the tests to be performed as routine tests. Double-shear configuration testing, as described in ISO 22762-1:2024, 6.2.2 can be employed with the approval of the structural engineer.

Some of these properties may be determined using one of the standard test pieces detailed in ISO 22762-1:2024, Tables 10 and 11. The standard test pieces are used for non-specific product tests, such as testing in the development of new materials and products.

6.5.2 Compressive properties

6.5.2.1 General requirements

6.5.2.1.1 The maximum compressive displacement at the design load shall exceed the design requirement specified by the structural engineer.

6.5.2.1.2 When a compressive stiffness constant is required, the compressive stiffness, K_v , shall be within $\pm 30\%$ of the design requirement.

6.5.2.1.3 The values of P_1 and P_2 necessary to calculate K_v are obtained from [Formulae \(1\)](#) and [\(2\)](#):

$$P_1 = A_{\text{load}} \times \sigma_1 \quad (1)$$

$$P_2 = A_{\text{load}} \times \sigma_2 \quad (2)$$

whereby the recommended values of σ_1 and σ_2 should be:

- a) σ_1 : 1,5 N/mm²;
- b) σ_2 : 6,0 N/mm².

The values of σ_1 and σ_2 can also be given by the structural engineer.

6.5.2.2 Test piece

The test piece shall be a full-scale elastomeric isolator for the type test and a production elastomeric isolator for the routine test.

6.5.2.3 Test conditions

The standard test temperature, T_0 , is 23 °C or 27 °C. If the test is carried out at a different temperature, the result shall be corrected to the value of the property at T_0 by an appropriate method.

6.5.3 Rotation properties

6.5.3.1 General requirements

The displacement measured during compressive tests at the design load shall exceed the rotation displacement specified by the structural engineer. Static rotation tests can be carried out as an option using a test piece and test method agreed with the structural engineer.

6.5.3.2 Test piece

The test piece shall be a full-scale elastomeric isolator for the type test and a production elastomeric isolator for the routine test.

6.5.4 Shear properties

6.5.4.1 General requirements

6.5.4.1.1 The shear strain shall be 100 %, 175 % or a shear strain as selected by the structural engineer.

6.5.4.1.2 The shear stiffness shall be within the tolerance selected from [Table 3](#) for the design requirement.

6.5.4.1.3 The equivalent damping ratio shall satisfy the requirement specified by the structural engineer.

6.5.4.1.4 The test items required for determination of shear properties are given in [Table 5](#).

Table 5 — Shear property test items

Isolator type	Test item	No. of loading cycles	Data loop
LNR	Shear stiffness, K_h	3	Third cycle
HDR	Shear stiffness, K_h Equivalent damping ratio, h_{eq}	3 or 11	Third cycle or average of the second to the eleventh. The data may be determined from a single loop (preferably the third) or from the average response over the second to eleventh loops, depending on the decision of the structural engineer.
LRB	Shear stiffness, K_h , and equivalent damping ratio h_{eq} or post-yield stiffness K_d , and characteristic strength, Q_d	3 or 11	Third cycle or average of the second to the eleventh. The data may be evaluated from a single loop (preferably the third) or from the average response over the second to eleventh loops, depending on the decision of the structural engineer.

6.5.4.2 Test piece

The test piece shall be a full-scale elastomeric isolator for the type test and a production elastomeric isolator for the routine test.

6.5.4.3 Test conditions

The standard temperature, T_0 , is 23 °C or 27 °C. If the test is carried out at a different temperature, the result shall be corrected to the value of the property at T_0 by an appropriate method.

6.5.5 Tensile properties

6.5.5.1 General requirements

The test piece shall not break at the force specified by the structural engineer.

6.5.5.2 Test piece

The test piece shall be a full-scale or a scale B elastomeric isolator.

6.5.5.3 Test conditions

The test piece shall be subjected to the shear strain specified by the structural engineer, and the force specified by the structural engineer to pull the elastomeric isolator shall then be applied.

6.5.6 Dependencies of shear properties

6.5.6.1 Shear-strain dependence

6.5.6.1.1 General requirements

The shear-strain dependence shall be within a specified range agreed by both the structural engineer and the manufacturer.

6.5.6.1.2 Test piece

The test piece shall be a full-scale or a scale B elastomeric isolator.

6.5.6.1.3 Test conditions

The shear properties at $0,5\gamma_0$, $1,0\gamma_0$, $1,5\gamma_0$ or the maximum shear strain shall be determined. Tests can also be performed at shear strains of $0,1\gamma_0$ and $0,2\gamma_0$.

6.5.6.2 Compressive stress dependence

6.5.6.2.1 General requirements

The compressive stress dependence shall be within a specified range agreed on by both the structural engineer and the manufacturer.

6.5.6.2.2 Test piece

The test piece shall be a full-scale or a scale B elastomeric isolator.

6.5.6.2.3 Test conditions

The shear properties at 0 , $0,5\sigma_0$, $1,0\sigma_0$, $1,5\sigma_0$ and the maximum tensile stress, if applicable, shall be determined, and the results normalized using the value corresponding to the design stress.

6.5.6.3 Frequency dependence

6.5.6.3.1 General requirements

The frequency dependence shall be within a specified range agreed by both the structural engineer and the manufacturer.

6.5.6.3.2 Test piece

The test piece shall be a full-scale or a scale A elastomeric isolator, a standard test piece or a shear-block test piece.

6.5.6.4 Repeated loading dependence

6.5.6.4.1 General requirements

The repeated loading dependence shall be within a specified range agreed by both the structural engineer and the manufacturer.

6.5.6.4.2 Test piece

The test piece shall be a full-scale or a scale B elastomeric isolator.

6.5.6.4.3 Test conditions

The shear strain amplitude shall be γ_0 .

6.5.6.5 Temperature dependence

6.5.6.5.1 General requirements

The temperature dependence shall be within a specified range agreed by both the structural engineer and the manufacturer.

6.5.6.5.2 Test piece

The test piece shall be a full-scale or a scale A elastomeric isolator, a standard test piece or a shear-block test piece.

6.5.6.5.3 Test conditions

The shear strain amplitude shall be γ_0 .

6.5.7 Shear displacement capacity

6.5.7.1 General requirements

6.5.7.1.1 The test piece shall be subjected to shear deformation under the constant compressive force given in the design requirements until breaking, buckling or roll-out occurs in one direction. The shear deformation and shear force at occurrence of breaking or buckling shall be recorded.