



BSI Standards Publication

Space Engineering — Thermal design handbook

Part 5: Structural Materials: Metallic and Composite

National foreword

This Published Document is the UK implementation of CEN/CLC/TR 17603-31-05:2021.

The UK participation in its preparation was entrusted to Technical Committee ACE/68, Space systems and operations.

A list of organizations represented on this committee can be obtained on request to its committee manager.

Contractual and legal considerations

This publication has been prepared in good faith, however no representation, warranty, assurance or undertaking (express or implied) is or will be made, and no responsibility or liability is or will be accepted by BSI in relation to the adequacy, accuracy, completeness or reasonableness of this publication. All and any such responsibility and liability is expressly disclaimed to the full extent permitted by the law.

This publication is provided as is, and is to be used at the recipient's own risk.

The recipient is advised to consider seeking professional guidance with respect to its use of this publication.

This publication is not intended to constitute a contract. Users are responsible for its correct application.

This publication is not to be regarded as a British Standard.

© The British Standards Institution 2021
Published by BSI Standards Limited 2021

ISBN 978 0 539 16979 9

ICS 49.140

Compliance with a Published Document cannot confer immunity from legal obligations.

This Published Document was published under the authority of the Standards Policy and Strategy Committee on 31 August 2021.

Amendments/corrigenda issued since publication

Date	Text affected
------	---------------

August 2021

ICS 49.140

English version

Space Engineering - Thermal design handbook - Part 5: Structural Materials: Metallic and Composite

Ingénierie spatiale - Manuel de conception thermique -
Partie 5 : Matériaux de structure : métalliques et
composites

Raumfahrttechnik - Handbuch für thermisches Design -
Teil 5: Strukturmaterialien: Metalle und Verbundstoffe

This Technical Report was approved by CEN on 14 June 2021. It has been drawn up by the Technical Committee CEN/CLC/JTC 5.

CEN and CENELEC members are the national standards bodies and national electrotechnical committees of Austria, Belgium, Bulgaria, Croatia, Cyprus, Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, Netherlands, Norway, Poland, Portugal, Republic of North Macedonia, Romania, Serbia, Slovakia, Slovenia, Spain, Sweden, Switzerland, Turkey and United Kingdom.



CEN-CENELEC Management Centre:
Rue de la Science 23, B-1040 Brussels

Table of contents

European Foreword	17
1 Scope	18
2 References	19
3 Terms, definitions and symbols	20
3.1 Terms and definitions	20
3.2 Symbols.....	20
4 Metallic materials	23
4.1 General.....	23
4.1.1 Modifiers of thermal radiative properties.....	26
4.1.2 Cladding definitions.....	27
4.1.3 Temper designation for heat treatable aluminium alloys.....	28
4.2 Aluminium alloys.....	28
4.3 Aluminium-Copper alloys	85
4.4 Aluminium-Magnesium alloys	104
4.5 Aluminium-Zinc alloys.....	114
4.6 Magnesium-Zinc-Thorium alloys	131
4.7 Titanium-Aluminium-Tin alloys	133
4.8 Titanium-Aluminium-Tin alloys	144
4.9 Titanium-Aluminium-Vanadium alloys	151
4.10 Nickel-Chrome-Cobalt-Molybdenum alloys	165
4.11 Iron-Nickel alloys	175
5 Composite materials	182
5.1 List of symbols.....	182
5.2 List of matrices, prepregs and laminates quoted in this clause	187
5.2.1 Matrices, adhesives, potting, moulding compounds	188
5.2.2 Prepregs, laminates and films	193
5.2.3 Code list of manufacturers (or developers).....	195
5.3 General introduction	197
5.3.2 Composition.....	198

5.3.3	Commercial fiber product names, descriptions and manufacturers	200
5.3.4	Geometry of fiber reinforcement. fabrics. abridged designation.....	205
5.4	Physical properties	210
5.4.1	Density.....	210
5.5	Thermal properties.....	216
5.5.1	Specific heat	216
5.5.2	Thermal conductivity	222
5.5.3	Thermal diffusivity	247
5.6	Thermo-elastic properties	256
5.6.1	Coefficient of linear thermal expansion.....	256
5.7	Thermal radiation properties of bare high strength fibers	319
5.7.1	Sample characterization.....	319
5.7.2	Emittance.....	319
5.7.3	Absorptance.....	321
5.8	Thermal radiation properties of bare composite materials.....	324
5.8.1	Tabulated data	324
5.9	Thermal radiation properties of coated composite materials	326
5.9.1	White painted composite materials.....	327
5.9.2	Sputtered Aluminium on graphite-epoxy composite material	331
5.10	Operating temperature range.....	334
5.10.1	Temperatures related to the maximum service temperature.....	335
5.11	Electrical properties	341
5.11.1	Electrical resistance and electrical resistivity	341
5.12	Prelaunch environmental effects.....	348
5.12.1	Moisture absorption and desorption	348
5.13	Postlaunch environmental effects	355
5.13.1	Ascent.....	355
5.13.2	Orbital effects.....	357
5.13.3	Re-entry effects.....	367
5.14	Thermal vacuum cycling	371
5.14.1	Test facilities	371
5.14.2	Measurement methods	372
5.14.3	Thermal vacuum cycling effects on the coefficient of linear thermal expansion	373
5.14.4	Trends in the variation of mechanical properties	378
5.15	Coating application	378
5.15.1	Pcbz conductive white paint	378
5.15.2	APA-2474 (TiO ₂ white paint)	378

5.15.3	Wiederhold's Z-12321	379
5.16	Past spatial uses	380
5.16.1	Intelsat v	380
5.16.2	Spelda (structure porteuse externe de lancement double ariane).....	381
5.16.3	CS-3A Japanese satellite	384
Bibliography metallic materials.....		387
References composite materials.....		391

Figures

Figure 4-1:	Specific heat, c , of Aluminium as a function of temperature, T	30
Figure 4-2:	Thermal conductivity, κ , of Aluminium as a function of temperature, T	31
Figure 4-3:	Thermal conductivity integrals of Aluminium as a function of temperature, T	32
Figure 4-4:	Thermal diffusivity, α , of Aluminium as a function of temperature, T	33
Figure 4-5:	Linear thermal expansion, $\Delta L / L$, of Aluminium as a function of temperature, T	34
Figure 4-6:	Normal spectral emittance, ε_{λ}' , of Aluminium as a function of wavelength, λ	37
Figure 4-7:	Normal spectral emittance, ε_{λ}' , of Aluminium conversion coatings as a function of wavelength, λ	38
Figure 4-8:	Angular spectral emittance, ε_{λ}' , of Aluminium as a function of wavelength, λ	39
Figure 4-9:	Normal total emittance, ε' , of Aluminium as a function of temperature, T	45
Figure 4-10:	Normal total emittance, ε' , of Aluminium anodized as a function of anodizing thickness, t_c	46
Figure 4-11:	Summary of data concerning the hemispherical total emittance, ε , of Aluminium as a function of temperature, T . From Touloukian & DeWitt (1970) [42].....	47
Figure 4-12:	Summary of data concerning the hemispherical total emittance, ε , of Aluminium conversion coatings vs. temperature, T . From Touloukian, DeWitt & HERNICZ (1972) [43].....	52
Figure 4-13:	Directional spectral absorptance, α_{λ}' , of Aluminium as a function of wavelength, λ . Data points ∇ correspond to $\beta = 25^\circ$	54
Figure 4-14:	Absorptance to emittance ratio, α_s/ε , of Aluminium conversion coatings as a function of the exposure time, t	60
Figure 4-15:	Normal - normal spectral reflectance, ρ_{λ}'' , of Aluminium as a function of wavelength, λ	62
Figure 4-16:	Normal - normal spectral reflectance, ρ_{λ}'' , of Aluminium contact coatings as a function of wavelength, λ	64
Figure 4-17:	Effect of coating thickness on normal - normal spectral reflectance, ρ_{λ}'' , of Aluminium conversion coatings as a function of wavelength, λ	65
Figure 4-18:	Bidirectional reflectance, ρ_{λ}'' , of Aluminium contact coatings as a function of wavelength, λ	66

Figure 4-19: Bidirectional spectral reflectance, ρ_{λ}'' , of Aluminium conversion coatings as a function of zenith angles, β and β' , of incident and reflected radiations.	68
Figure 4-20: Summary of data concerning normal - hemispherical spectral reflectance, ρ_{λ}' , of Aluminium vs. wavelength, λ . From Touloukian & DeWitt (1970) [42].	69
Figure 4-21: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Aluminium conversion coatings as a function of wavelength, λ	70
Figure 4-22: Effect of UV exposure on normal - hemispherical spectral reflectance, ρ_{λ}' , of Aluminium conversion coatings as a function of wavelength, λ	71
Figure 4-23: Effect of electron exposure on normal - hemispherical spectral reflectance of Aluminium conversion coatings as a function of wavelength, λ	72
Figure 4-24: Effect of simultaneous UV - electron exposure on normal - hemispherical spectral reflectance, ρ_{λ}' , of Aluminium conversion coatings as a function of wavelength, λ	73
Figure 4-25: Effect of proton exposure on normal - hemispherical spectral reflectance, ρ_{λ}' , of Aluminium conversion coatings as a function of wavelength, λ	74
Figure 4-26: Directional - hemispherical spectral reflectance, ρ_{λ}' , of Aluminium conversion coatings as a function of wavelength, λ	75
Figure 4-27: Hemispherical - normal spectral reflectance, ρ_{λ}' , of Aluminium contact coatings as a function of wavelength, λ	76
Figure 4-28: Bidirectional total reflectance, ρ'' , of Aluminium as a function of the viewing zenith angles, β'	77
Figure 4-29: Normal - normal spectral transmittance, τ_{λ}'' , of Aluminium as a function of wavelength, λ	80
Figure 4-30: Angular spectral transmittance, τ_{λ}'' , of Aluminium as a function of wavelength, λ	81
Figure 4-31: Electrical resistivity, σ^{-1} , of Aluminium as a function of temperature, T	83
Figure 4-32: Specific heat, c , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of temperature, T	86
Figure 4-33: Thermal conductivity, k , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of temperature, T	87
Figure 4-34: Thermal conductivity integrals of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of temperature, T	88
Figure 4-35: Thermal diffusivity, α , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of temperature, T	89
Figure 4-36: Linear thermal expansion, $\Delta L / L$, of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of temperature, T	90
Figure 4-37: Normal - spectral emittance, ε_{λ}' , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of wavelength, λ	91
Figure 4-38: Normal total emittance, ε' , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of temperature, T	93
Figure 4-39: Normal-normal spectral reflectance, ρ_{λ}'' , of Al-4,3 Cu-1,5 Mg-0,6 Mn, anodized, as a function of wavelength, λ	98

Figure 4-40: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn as a function of wavelength, λ .	99
Figure 4-41: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Al - 4,3 Cu - 1,5 Mg - 0,6 Mn, anodized, as a function of wavelength, λ .	100
Figure 4-42: Normal-hemispherical spectral reflectance, ρ_{λ}' , of Al-1 Mg-0,6 Si, as received, as a function of wavelength, λ .	108
Figure 4-43: Normal-hemispherical spectral reflectance, ρ_{λ}' , of Al-1 Mg-0,6 Si, grit blasted, as a function of wavelength, λ .	109
Figure 4-44: Normal-hemispherical spectral reflectance, ρ_{λ}' , of Al-1 Mg-0,6 Si, chemically polished, as a function of wavelength, λ .	111
Figure 4-45: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Al - 1 Mg - 0,6 Si, chemically milled, as a function of wavelength, λ .	112
Figure 4-46: Specific heat, c , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of temperature, T .	115
Figure 4-47: Thermal conductivity, k , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of temperature, T .	116
Figure 4-48: Thermal conductivity integral of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of temperature, T .	117
Figure 4-49: Thermal diffusivity, α , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of temperature, T .	118
Figure 4-50: Linear thermal expansion, $\Delta L / L$, of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of temperature, T .	119
Figure 4-51: Normal spectral emittance, ε_{λ}' , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of wavelength, λ .	120
Figure 4-52: Angular spectral emittance, ε_{λ}' , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of wavelength, λ .	121
Figure 4-53: Normal total emittance, ε' , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu as a function of temperature, T .	122
Figure 4-54: Normal-hemispherical spectral reflectance, ρ_{λ}' , of Al - 5,7 Zn - 2,5 Mg - 1,6 Cu conversion coatings, as a function of wavelength, λ .	126
Figure 4-55: Specific heat, c , of Ti - 5 Al - 2,5 Sn as a function of temperature, T .	134
Figure 4-56: Thermal conductivity, k , of Ti - 5 Al - 2,5 Sn as a function of temperature, T .	135
Figure 4-57: Thermal linear expansion, $\Delta L / L$, of Ti - 5 Al - 2,5 Sn as a function of temperature, T .	136
Figure 4-58: Normal spectral emittance, ε_{λ}' , of Ti - 5 Al - 2,5 Sn as a function of temperature, T , for $\lambda = 6,65 \times 10^{-7}$ m.	137
Figure 4-59: Normal total emittance, ε' , of Ti - 5 Al - 2,5 Sn as a function of temperature, T .	138
Figure 4-60: Normal-normal spectral reflectance, ρ_{λ}'' , of Ti - 5 Al - 2,5 Sn as a function of wavelength, λ .	140
Figure 4-61: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Ti - 5 Al - 2,5 Sn as a function of wavelength, λ .	141

Figure 4-62: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Ti - 5 Al - 2,5 Sn, anodized, as a function of wavelength, λ	142
Figure 4-63: Electrical resistivity, σ^{-1} , of Ti - 5 Al - 2,5 Sn as a function of temperature, T	143
Figure 4-64: Specific heat, c , of Ti - 6 Al - 2 Sn - 4 Zr - 2 Mo as a function of temperature, T	145
Figure 4-65: Thermal conductivity, k , of Ti - 6 Al - 2 Sn - 4 Zr - 2 Mo as a function of temperature, T	146
Figure 4-66: Mean coefficient of linear thermal expansion, β , of Ti - 6 Al - 2 Sn - 4 Zr - 2 Mo from room temperature to temperature T	147
Figure 4-67: Electrical resistivity, σ^{-1} , of Ti - 6 Al - 2 Sn - 4 Zr - 2 Mo as a function of temperature, T	149
Figure 4-68: Specific heat, c , of Ti - 6 Al - 4 V as a function of temperature, T	152
Figure 4-69: Thermal conductivity, k , of Ti - 6 Al - 4 V as a function of temperature, T	153
Figure 4-70: Thermal conductivity integrals of Ti - 6 Al - 4 V as a function of temperature, T	154
Figure 4-71: Thermal diffusivity, α , of Ti - 6 Al - 4 V as a function of temperature, T	155
Figure 4-72: Thermal linear expansion, $\Delta L/L$, of Ti - 6 Al - 4 V as a function of temperature, T	156
Figure 4-73: Normal spectral emittance, ε_{λ}' , of Ti - 6 Al - 4 V as a function of temperature, T	157
Figure 4-74: Normal total emittance, ε' , of Ti - 6 Al - 4 V as a function of temperature, T	158
Figure 4-75: Hemispherical total emittance, ε , of Ti - 6 Al - 4 V as a function of temperature, T	160
Figure 4-76: Normal - hemispherical spectral reflectance, ρ_{λ}' , of Ti - 6 Al - 4 V as a function of wavelength, λ	162
Figure 4-77: Electrical resistivity, σ^{-1} , of Ti - 6 Al - 4 V as a function of temperature, T	163
Figure 4-78: Specific heat, c , of Ni - 19 Cr - 11 Co - 10 Mo - 3 Ti as a function of temperature, T	166
Figure 4-79: Thermal conductivity, k , of Ni - 19 Cr - 11 Co - 10 Mo - 3 Ti as a function of temperature, T	167
Figure 4-80: Thermal linear expansion, $\Delta L/L$, of Ni - 19 Cr - 11 Co - 10 Mo - 3 Ti as a function of temperature, T	168
Figure 4-81: Normal spectral emittance, ε_{λ}' , of Ni - 19 Cr - 11 Co - 10 Mo - 3 Ti as a function of wavelength, λ	169
Figure 4-82: Normal total emittance, ε' , of Ni - 19 Cr - 11 Co - 10 Mo - 3 Ti as a function of temperature, T	170
Figure 4-83: Normal-normal spectral reflectance, ρ_{λ}'' , of Ni - 19 Cr - 11 Co - 10 Mo - 3 Ti as a function of wavelength, λ . Data points $\triangleright$ correspond to normal-hemispherical reflectance while $\blacktriangleright$, $\blacktriangleleft$ correspond to hemispherical-normal reflectance.	172
Figure 4-84: Specific heat, c , of Fe - 36 Ni (Invar) as a function of temperature, T	176

Figure 4-85: Linear thermal expansion, $\Delta L/L$, of Fe - 36 Ni (Invar) as a function of temperature, T	177
Figure 4-86: Effect of the concentration of alloying elements, c , on the value of the coefficient of linear expansion, β . From MOND NICKEL Co.	178
Figure 4-87: Normal emittance, ε_{λ}' , of Fe - 36 Ni (Invar), for $\lambda = 6,7 \times 10^{-7}$ as a function of temperature, T	179
Figure 5-1: International ties between Carbon Fiber manufactures. From SENER (1984) [147].....	205
Figure 5-2: Schematic of an angle plied laminate. From Chamis (1987) [67].	206
Figure 5-3: Schematic of a tri-orthogonally fiber reinforced composite. a) Straight filaments. From Domínguez (1987) [82]. b) Tapes. From Aboudi (1984) [49].	206
Figure 5-4: Main types of woven fabrics. Lengthwise (warp) yarns and crosswise (fill) yarns can be interlaced to produce woven fabrics. A fabric construction of 16 x 14 means 16 warp ends per inch and 14 fill ends per inch. a) Plain weave. Very stable. Small yarn slippage. b) Leno weave. Minimizes distortion with few yarns. c) Twill. The fabric has a broken diagonal line and, consequently, greater pliability than a plain weave. d) Crowfoot satin. Pliable and comfortable to contoured surfaces. From Domínguez (1987) [82], Weeton, Peters & Thomas (1987) [164].	207
Figure 5-5: Longitudinal (to fibers) and transverse directions for the measurement of composite properties. From Chamis (1987) [67].	209
Figure 5-6: Cryostat assemblies for measuring the thermal conductivity, k . a) High- k samples. b) Low- k samples. From Pilling, Yates, Black & Tattersall (1979) [137]. For explanation see text.	222
Figure 5-7: Facility used to measure the thermal conductivity, k , of a sample as a function of temperature in the range 90 K to 410 K. Temperature changes continuously. From Ott (1981) [132].	224
Figure 5-8: Hypodermic probe to measure the thermal conductivity of polymer melts. All the dimensions are in mm. From Lobo & Cohen (1990) [120].	225
Figure 5-9: Thermal conductivity, k_m , of different matrices as a function of temperature, T . Numerical values are given in Table 5-10.	236
Figure 5-10: Longitudinal thermal conductivity, k_{f1} , of several advanced pitch graphite fibers vs. temperature, T . The fiber designation is from Amoco Performance Products; the number stands for the fiber elasticity modulus in millions of lbs.in ⁻² . All the data, unless otherwise stated, are from LMSC. Pitch precursor graphite fibers have a structure which approaches that of a single crystal of graphite and, thus, their thermal conductivity is very large. From McGuire & Vollerin (1990) [127].	237
Figure 5-11: Typical assembly for measuring the thermal diffusivity, α , of a long slender bar by use of the Angström method. From Landis (1964) [116].	247
Figure 5-12: Typical assembly for measuring the thermal diffusivity, α , of a disc shaped sample. From Lachi, Legrand & Degiovanni (1988) [115].	248
Figure 5-13: Thermal diffusivity, α_f , of different fiber cloths as a function of temperature, T . Numerical values are given in Table 5-33 From Touloukian (1967) [157].	251

- Figure 5-14: Experimental arrangement for the interferometric measurement of the thermal expansion. a) Specimen chamber assembly. b) Optical system. From James & Yates (1965) [108]. For explanation see text.256
- Figure 5-15: The ESTEC CTE 1000 facility for the measurement of the linear thermal expansion of structure up to 0,7 m long. All the dimensions are in mm. From Aalders (1989) [48].258
- Figure 5-16: Linear thermal expansion, β_m , as a function of temperature, T , for four different epoxy matrices. Numerical values are given in Table 5-41.269
- Figure 5-17: Linear thermal expansion coefficient measured parallel to fibers, β_1 , as a function of temperature, T , for some composite materials formed by the same matrix, DER 332/T403, and two different glass fiber reinforcements. Upper and lower limits of the shadowed regions are for 95% confidence.278
- Figure 5-18: Linear thermal expansion coefficient measured perpendicular to fibers, β_2 , as a function of temperature, T , for some composite materials formed by the same matrix, DER 332/T403, and two different glass fiber reinforcements.280
- Figure 5-19: Linear thermal expansion coefficient measured in different directions, β , as a function of temperature, T , for similar carbon fiber reinforced composite materials. The matrix is ERLA 4617/mPDA. From Rogers, Phillips, Kingston.Lee, Yates, Overy, Sargent & McCalla (1977) [144].281
- Figure 5-20: Linear thermal expansion coefficient measured parallel to fibers, β_1 , as a function of temperature, T , for different fiber volume ratios, φ_f . Fiber: Courtaulds HTS PT112/21Z; Matrix: DLS 351/BF₃400.290
- Figure 5-21: Linear thermal expansion coefficient measured perpendicular to fibers, β_2 , as a function of temperature, T , for different fiber volume ratios, φ_f . Fiber: Courtaulds HTS PT112/21Z; Matrix: DLS 351/BF₃400.291
- Figure 5-22: Linear thermal expansion coefficient measured either in plane of laminate, β_1 , or perpendicular to it, β_3 , as a function of temperature, T , for similar carbon fibers reinforced composite materials. The fiber is carbon HTS PT112/21Z. From Yates, McCalla, Sargent, Rogers, Phillips & Kingston-Lee (1978)b [169].292
- Figure 5-23: Linear thermal expansion coefficient, β , of a carbon fiber reinforced unidirectional composite material, measured in plane of laminate, as a function of the direction of the measurement, θ . Matrix is Epikote 828/BF₃MEA. Fibers are Torayca T300A. Temperature range is 290 K to 340 K. From Isikawa, Koyama & Kobayashi (1977, 1978) [106] & [107].299
- Figure 5-24: Linear thermal expansion coefficient measured parallel to fibers, β_1 , as a function of temperature, T , for two nominally identical carbon fiber reinforced composite materials produced on separate occasions and having slightly different fiber volume ratios, φ_f . Fiber: HTSCarbon; Matrix: Fibredux 914C.300
- Figure 5-25: Linear thermal expansion coefficient measured perpendicular to fibers, β_2 , as a function of temperature, T , for two nominally identical carbon fiber reinforced composite materials produced on separate occasions and having slightly different fiber volume ratios, φ_f . Fiber: HTSCarbon; Matrix: Fibredux 914C.301
- Figure 5-26: Linear thermal expansion coefficient measured in 0° direction, β_0 , as a function of temperature, T , for some carbon fiber reinforced composite

materials with various amounts of fibers in different directions. Fiber: Courtaulds HTS, Type II; Matrix: Fibredux 914C.	306
Figure 5-27: Linear thermal expansion coefficient, β_0 , of a two-ply ($\pm \theta$) carbon fiber reinforced composite material, measured in direction 0° of the plane of laminate, as a function of the angle ply, θ . Matrix is Hercules 3002, fibers are Hercules HT (Hercules 3002T prepreg). Temperature range is 80 K to 450 K. From Friend, Poesch & Leslie (1972) [90].	308
Figure 5-28: Linear thermal expansion coefficient, β , measured in several directions of the plane of laminate for an unidirectional and an angle plied carbon fiber reinforced composite material, as a function of temperature, T . Matrix is Narmco 5208, fibers are Narmco T300. From Karlsson (1983) [111].	309
Figure 5-29: Linear thermal expansion coefficient measured either parallel, β_1 , or perpendicular, β_2 , to fibers of two composites with similar epoxy matrices, but with carbon fiber or Kevlar 49 reinforcements.	316
Figure 5-30: Linear thermal expansion coefficient measured parallel to fibers, β_1 , as a function of temperature, T , for two graphite fiber-metal and one carbon fiber-epoxy composite materials.	317
Figure 5-31: Linear thermal expansion coefficient measured perpendicular to fibers, β_2 , as a function of temperature, T , for graphite fiber-metal and carbon fiber-epoxy composite materials.	318
Figure 5-32: Normal spectral absorptance, α'_λ , of SiO ₂ Fabric at 310 K vs. wavelength, λ . Sample is described in the text. From Eagles, Babjak & Weaver (1975) [85].	320
Figure 5-33: Normal-hemispherical spectral reflectance, ρ'_λ , of SiO ₂ Fabric vs. wavelength, λ . Sample is described in the text. From Eagles, Babjak & Weaver (1975) [85].	321
Figure 5-34: Solar absorptance, α_s , of SiO ₂ Fabric-Substrate composite as a function of the solar absorptance, α_{ss} , of the substrate. Sample: 16 Harness Satin Weave $0,38 \times 10^{-3}$ m thick, on different substrates. From Eagles, Babjak & Weaver (1975) [85].	322
Figure 5-35: Absorptance/Emitatnce ratio, α_s/ε , solar absorptance, α_s , and hemispherical total emittance, ε , of various mosaics of silica and carbon yarn as functions of the exposed black to total area fraction, A_B/A . From Eagles, Babjak & Weaver (1975) [85].	322
Figure 5-36: Normal spectral emittance, ε'_λ , of PV 100 coating on different substrates and with different thicknesses (see Table 5-67) vs. wavelength, λ , at 393 K. From Giommi, Marchetti, Salza & Testa (1985) [92].	327
Figure 5-37: Normal-hemispherical spectral reflectance factor, R'_λ , of PV 100 coating on different substrates and with different thicknesses vs. wavelength, λ . From Giommi, Marchetti, Salza & Testa (1985) [92].	329
Figure 5-38: Normal total emittance, $\varepsilon'(0)$, of sputtered aluminium on T300/5209 graphite-epoxy composite material as a function of sputtered coating thickness, t_c , and for two different textures of the supporting material. From Witte & Teichman (1989) [166].	332
Figure 5-39: Normal solar absorptance, α_s , of sputtered aluminium on T300/5209 graphite-epoxy composite material as a function of sputtered coating	

thickness, t_c , and for two different textures of the supporting material. From Witte & Teichman (1989) [166].	333
Figure 5-40: Solar absorptance to emittance ratio of sputtered aluminium on T300/5209 graphite-epoxy composite material as a function of sputtered coating thickness, t_c , and for two different textures of the supporting material. From Witte & Teichman (1989) [166].	334
Figure 5-41: Tensile strength, σ_t , vs. temperature, T , of structural materials. Inert atmospheres. From DeMario (1985) [81].	335
Figure 5-42: Electrical resistivity, ρ , as a function of frequency, f , for a carbon-epoxy composite material. Fiber: Super A, Matrix: Fibredux 914C. Layup ($0^\circ \pm 45^\circ$) 16 plies. Sample size: $\bigcirc$: $> 1,98 \times 10^{-3}$ m, 10×10^{-3} m, 25×10^{-3} m. $\square$: $> 1,98 \times 10^{-3}$ m, $5,5 \times 10^{-3}$ m, 25×10^{-3} m. From Thomson (1982) [156].	345
Figure 5-43: One-dimensional and radial models of laminar diffusion through homogeneous-isotropic media.	350
Figure 5-44: Moisture content, M , as a function of ambient temperature, T , after 100 h of exposure to distilled water at that temperature, for several carbon fiber reinforced composites. The specimens are infinitely large rods of 6×10^{-3} m diameter. $M_0 = 0,002$ assumed.	351
Figure 5-45: Effect of UV radiation on linear thermal expansion, β , of Graphite/epoxy T300/SP 288 laminates. a) $\theta = 90^\circ$, b) $\theta = (\pm 43^\circ)_s$, c) $\theta = 0^\circ$. Ambient pressure 10^{-4} Pa to 10^{-5} Pa. From Tennyson & Zimcik (1982) [107], Hansen & Tennyson (1983) [153].	361
Figure 5-46: Effect of UV radiation on linear thermal expansion, β , of Kevlar/epoxy 3M SP 306 laminates. a) $\theta = 90^\circ$, b) $\theta = (\pm 43^\circ)_s$, c) $\theta = 0^\circ$. Ambient pressure 10^{-4} Pa to 10^{-5} Pa. From Tennyson & Zimcik (1982) [154], Hansen & Tennyson (1983) [95].	361
Figure 5-47: Effect of electron radiation with (thick solid line) and without (thin solid line) UV exposure, on linear thermal expansion, β_0 , of graphite/epoxy and Kevlar/epoxy, $\theta = (\pm 43^\circ)_s$. Ambient pressure 10^{-4} Pa to 10^{-5} Pa. Exposure > 1 year and 300 ESD of UV. From Hansen & Tennyson (1983) [95].	362
Figure 5-48: Linear thermal expansion, β_0 , as a function of temperature, T , of T50(PAN)/F263 (0/90) _{2s} HM graphite/epoxy laminates exposed to electron radiation. Calculated by the compiler by numerical derivation ($\beta = d(\Delta L/L)/dT$) of data from Mauri & Crossman (1983) [125].	362
Figure 5-49: Graphs for estimating the depletion by atomic oxygen of a material of known Reaction Efficiency, R_e . From Leger & Visentine (1986) [118].	367
Figure 5-50: Effect of the number of thermal cycles, N , on the linear thermal expansion, β_0 , of $(\pm 22^\circ)_s$ T300/3M SP288 Graphite/Epoxy laminates. $300 \text{ K} \leq T \leq 370 \text{ K}$, $p = 1,33 \times 10^{-4} \text{ Pa}$ to $1,33 \times 10^{-5} \text{ Pa}$. From Tennyson & Zimcik (1982) [154], Hansen & Tennyson (1983) [95].	375
Figure 5-51: Effect of the number of thermal cycles, N , on the linear thermal expansion, β_0 , of $(\pm 43^\circ)_s$ T300/3M SP288 Graphite/Epoxy laminates. $300 \text{ K} \leq T \leq 370 \text{ K}$, $p = 1,33 \times 10^{-4} \text{ Pa}$ to $1,33 \times 10^{-5} \text{ Pa}$. From Tennyson (1980) [153], Tennyson & Zimcik (1982) [154], Hansen & Tennyson (1983) [95].	375
Figure 5-52: Effect of the number of thermal vacuum cycles, N , on the linear thermal expansion, β_0 , of $(\pm \theta^\circ)_s$ T300/3M SP288 Graphite/Epoxy laminates. $300 \text{ K} \leq T \leq 370 \text{ K}$, $p = 1,33 \times 10^{-4} \text{ Pa}$ to $1,33 \times 10^{-5} \text{ Pa}$. 50 cycles ≈ 220 days in	

vacuum. From Tennyson & Zimcik (1982) [154], Hansen & Tennyson (1983) [95].	376
Figure 5-53: Effect of the number of thermal vacuum cycles, N , on the linear thermal expansion, β_0 , of $(\pm \theta^\circ)_s$ 3M SP306 Kevlar/Epoxy laminates. $300\text{ K} \leq T \leq 370\text{ K}$, $p = 1,33 \times 10^{-4}\text{ Pa}$ to $1,33 \times 10^{-5}\text{ Pa}$. 50 cycles $\approx$ 220 days in vacuum. From Tennyson & Zimcik (1982) [154], Hansen & Tennyson (1983) [95].	376
Figure 5-54: Comparison of predicted (-) and experimental (o) values of the linear thermal expansion, β_0 , vs. fiber angle, θ , for $(\pm \theta^\circ)_s$ 3M SP306 Kevlar/Epoxy laminates. 48 cycles $\approx$ 220 days in vacuum. $300\text{ K} \leq T \leq 370\text{ K}$, $p = 1,33 \times 10^{-4}\text{ Pa}$ to $1,33 \times 10^{-5}\text{ Pa}$. From Tennyson & Zimcik (1982) [171], Hansen & Tennyson (1983) [95]. Results for Graphite/Epoxy are given in Tennyson (1980) [153]. Compare also with Figure 5-27.	377
Figure 5-55: Effect of the number of thermal vacuum cycles, N , on the linear thermal expansion, β_0 , of $(\pm \theta^\circ)_s$ 3M SP290 Boron/Epoxy laminates. $300\text{ K} \leq T \leq 370\text{ K}$, $p = 1,33 \times 10^{-4}\text{ Pa}$ to $1,33 \times 10^{-5}\text{ Pa}$. 50 cycles $\approx$ 220 days in vacuum. From Tennyson & Zimcik (1982) [154], Hansen & Tennyson (1983) [95].	377
Figure 5-56: Coefficient of the linear thermal expansion, β_0 , as a function of temperature, T , for Graphite/Epoxy circular hybrid tubes, identified as Spec. No. 12 in Table 5-84 and Table 5-85, before (solid line) and after (dashed line) thermal vacuum cycling. 3000 cycles. $98\text{ K} \leq T \leq 370\text{ K}$, $p = 1,33 \times 10^{-3}\text{ Pa}$. From Reibaldi (1985) [141].	378
Figure 5-57: Outline of INTELSAT V communication satellite.	380
Figure 5-58: Sketch of the ARIANE 4 upper part. From Thomas & Oliver (1985) [155].	382
Figure 5-59: Exploded view of SPELDA. From Thomas & Oliver (1985) [155].	383
Figure 5-60: Sketch of the CS-3a structure. From Kawashima, Inoue & Seko (1985) [112].	384
Figure 5-61: Exploded view of CS-3a Central Thrust Tube. Prepared by the compiler after Kawashima, Inoue & Seko (1985) [112].	385

Tables

Table 4-1: Normal Total Emittance of Aluminium.	40
Table 4-2: Normal Total Emittance and Normal Solar Absorptance of Aluminium Contact Coatings.	42
Table 4-3: Normal Total Emittance and Normal Solar Absorptance of Aluminium Conversion Coatings.	44
Table 4-4: Hemispherical Total Emittance of Aluminium Contact Coatings.	47
Table 4-5: Hemispherical total Absorptance of Aluminium.	55
Table 4-6: Normal Solar Absorptance of Aluminium.	57
Table 4-7: Normal Solar Absorptance of Aluminium Conversion Coatings.	58
Table 4-8: Angular Solar absorptance of Aluminium.	60
Table 4-9: Normal-Normal Solar Reflectance of Aluminium Conversion Coatings.	78
Table 4-10: Normal-Hemispherical Solar Reflectance of Both Bulk Aluminium and Contact Coatings.	79
Table 4-11: Normal Total Emittance of Al – 4,3 Cu – 1,5 Mg – 0,6 Mn, Anodized.	95

Table 4-12: Hemispherical Total Emittance of Al – 4,3 Cu – 1,5 Mg – 0,6 Mn	95
Table 4-13: Normal Solar Absorptance of Al – 4,3 Cu – 1,5 Mg – 0,6 Mn	96
Table 4-14: Normal Solar Absorptance of Al – 4,3 Cu – 1,5 Mg – 0,6 Mn, Anodized	97
Table 4-15: Normal Hemispherical Solar Reflectance of Al – 4,3 Cu – 1,5 Mg – 0,6 Mn, Anodized	102
Table 4-16: Normal Total Emittance of Al – 1 Mg – 0,6 Si	105
Table 4-17: Hemispherical Total Emittance of Al – 1 Mg – 0,6 Si	106
Table 4-18: Normal Solar Absorptance of Al – 1 Mg – 0,6 Si	107
Table 4-19: Hemispherical Total Emittance of Al – 5,7 Zn – 2,5 Mg – 1,6 Cu Conversion Coatings.	124
Table 4-20: Normal Solar Absorptance and Normal-Hemispherical Solar Reflectance of Al – 5,6 Zn – 2,5 Mg 1,6 Cu	125
Table 4-21: Normal Solar Absorptance of Ti – 5 Al – 2,5 Sn	139
Table 4-22: Normal Solar Absorptance of Ti – Al – 4 V	161
Table 4-23: Cost of Ti – 6 Al – 4 – V compared with those of other structural metallic materials.	164
Table 4-24: Electrical Resistivity of Ni – 19Cr – 11Co – 10Mo – 3Ti ^a	173
Table 4-25: Linear thermal expansion coefficient of Fe – 36 Ni under different temper conditions.	178
Table 4-26: Magnetic Properties of Fe – 36 Ni under different temper conditions.	180
Table 4-27: Relative Permeability of Fe – 36 Ni, measured at 400 A.m ⁻¹	180
Table 5-1: Abridged Designation of Single Reinforcement Laminates	208
Table 5-2: Density, ρ_f [kg.m ⁻³], of High-Strength Fibers	210
Table 5-3: Density, ρ_m [kg.m ⁻³], of Matrices	215
Table 5-4: Specific Heat, c_f [J.kg ⁻¹ .K ⁻¹], of High-Strength Fibers	217
Table 5-5: Fussed Silicia	218
Table 5-6: Kevlar ^d	219
Table 5-7: Specific Heat, c_m [J.kg ⁻¹ .K ⁻¹], of Matrices	220
Table 5-8: Specific Heat, c [J.kg ⁻¹ .K ⁻¹], of Composite Materials	221
Table 5-9: Longitudinal (1) and Transverse (2) Thermal Conductivity, of High-Strength Fibers. Tabulated Data are k_{f1} [W.m ⁻¹ .K ⁻¹]/ k_{f2} [W.m ⁻¹ .K ⁻¹], of Fibers	226
Table 5-10: Thermal Conductivity, k_m [W.m ⁻¹ .K ⁻¹], of Matrices	228
Table 5-11: Araldite LY556	229
Table 5-12: DER 332/T403 (100:36) ^c	229
Table 5-13: Epitoke 210/BF ₃ 400 ^b	230
Table 5-14: Epoxin 162 ^a	230
Table 5-15: Palatal P51 ^a	231
Table 5-16: Nylon 6 ^a	232
Table 5-17: Comco, Nylon 6/6 ^{g,h}	233

Table 5-18: Polypenco 101, Nylon 6/6 ^{g,h}	234
Table 5-19: Polypropylene ^a	235
Table 5-20: Characteristics of Composite Materials (Thermal Conductivity can be found following the links).....	237
Table 5-21: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	241
Table 5-22: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	241
Table 5-23: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	242
Table 5-24: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	242
Table 5-25: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	242
Table 5-26: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	243
Table 5-27: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	243
Table 5-28: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	244
Table 5-29: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	245
Table 5-30: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	245
Table 5-31: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	246
Table 5-32: Smoothed values of the Thermal conductivity, k [W.m ⁻¹ .K ⁻¹], of the Composite Specimens Characterized in Table 5-9.	246
Table 5-33: Thermal diffusivity, $\alpha_f \times 10^6$ [m ² .s ⁻¹], of High-Strength Fibers.....	249
Table 5-34: Thermal diffusivity, $\alpha_f \times 10^6$ [m ² .s ⁻¹], of High-Strength Fibers.....	250
Table 5-35: Thermal diffusivity, α_m [m ² .s ⁻¹], of Matrices	252
Table 5-36: Thermal diffusivity, $\alpha \times 10^6$ [m ² .s ⁻¹], of Composite Materials	253
Table 5-37: Thermal diffusivity, $\alpha \times 10^6$ [m ² .s ⁻¹], of Composite Materials	254
Table 5-38: Thermal diffusivity, $\square \times 10^6$ [m ² .s ⁻¹], of Composite Materials.....	255
Table 5-39: Linear thermal expansion, β_f [K ⁻¹], and elasticity modulus, E_f [Pa], of high-strength fibers	260
Table 5-40: Linear thermal expansion, β_m [K ⁻¹], elasticity modulus, E_m [Pa] and Poisson's ratio, ν_m , of matrices.....	264
Table 5-41: Arrangements of the Data on Linear Thermal Expansion, β , of Composite Materials Compiled in Table 5-42 to Table 5-60	270
Table 5-42: Characterization of Composite Materials (Linear Thermal Expansion is given following the links).	271

Table 5-43: Smoothed values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens characterized in Table 5-85.....	274
Table 5-44: Smoothed values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens characterized in Table 5-85.....	274
Table 5-45: Smoothed values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens characterized in Table 5-85.....	275
Table 5-46: Smoothed values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens characterized in Table 5-85.....	275
Table 5-47: Smoothed values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens characterized in Table 5-85.....	276
Table 5-48: Smoothed values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens characterized in Table 5-85.....	277
Table 5-49: Characterization of Composite Materials (Linear Thermal Expansion is given following the links).	282
Table 5-50: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-49.....	285
Table 5-51: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-49.....	286
Table 5-52: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-49.....	288
Table 5-53: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-49.....	289
Table 5-54: Characterization of Composite Materials (Linear Thermal Expansion is given following the links).	293
Table 5-55: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-54.....	295
Table 5-56: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-54.....	296
Table 5-57: Characterization of Composite Materials (Linear Thermal Expansion is given following the links).	302
Table 5-58: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-57.....	304
Table 5-59: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-57.....	305
Table 5-60: Characterization of Composite Materials (Linear Thermal Expansion is given following the links).	310
Table 5-61: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-60.....	312
Table 5-62: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-60.....	313
Table 5-63: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-60.....	314
Table 5-64: Smoothed Values of the Linear Thermal Expansion Coefficient, $\beta \times 10^6$ [K ⁻¹], of the Specimens Characterized in Table 5-60.....	315

Table 5-65: Effect of the Space Environment on Solar Absorptance, α_s , of Silica Fabrics	323
Table 5-66: Normal Total Emittance, ε' ($\beta=0$), and Solar Absorptance, α_s , of Uncoated Plastic Materials	324
Table 5-67: Coated Composite Materials the Thermal Radiation Properties of Which Are Given in This Clause	326
Table 5-68: Normal Total Emittance, ε' ($\beta=0$), of PV 100 Coating on Different Substrates and with Different Thicknesses	328
Table 5-69: Normal Solar Reflectance, ρ_s ($\beta=0$), of PV 100 Coating on Different Substrates and with Different Thicknesses	330
Table 5-70: Characteristic Temperatures of Neat and Reinforced Resins	336
Table 5-71: Electrical Resistivity, ρ_r [$\Omega.m$], of High-Strength Fibers	342
Table 5-72: Electrical Resistivity, ρ [$\Omega.m$], of Carbon-Epoxy Composite Materials	344
Table 5-73: Drill Bit Costs and Standard Drilling Hourse	346
Table 5-74: Characterization of Composite Materials, the Maximum Moisture Content and Diffusion Constants of which are given in Table 5-75 and Table 5-76 respectively	352
Table 5-75: Maximum Moisture Content, M_m , of the Specimens Characterized in Table 5-74	353
Table 5-76: Constants D_0 and C for the Arrhenius Expression, of the Transverse Diffusion Coefficient, D_2 , of the Specimens Characterized in Table 5-74	353
Table 5-77: Outgassing Data for Typical Composite Materials	355
Table 5-78: Characterization of Materials Tested under a Vacuum Radiation Environment	357
Table 5-79: Summary of the Data Regarding Radiation Effects on the Coefficient of Linear Thermal Expansion for the Specimens Characterized in Table 5-78	360
Table 5-80: Average Values of Linear Thermal Expansion, β , for 75S(Pitch)/948A1(0/90) _{2S} Graphite/Epoxy Laminates in the Temperature Range 280 K - 370 K	363
Table 5-81: Atomic Oxygen Reaction Efficiency Data from Reported LEO Flights and Ground Testing	365
Table 5-82: Weight Loss, WL (%), of Carbon Fibers After Isothermal Aging in Flowing Air	368
Table 5-83: Chemical Composition, Atom (%), of both T40R and Hercules AS4 Carbon Fibers, as received and oxidized, ESCA	370
Table 5-84: Characterization of Materials Tested under or after Thermal Vacuum Cycling	371
Table 5-85: Thermal Vacuum Cycling Effects on the Coefficient of Linear Thermal Expansion of the Specimens Characterized in Table 5-84	373
Table 5-86: Effect of Storage on the Linear Thermal Expansion, β_o , of the Hybrid Tubes Identified as Spec. No. 1, in Table 5-84 and Table 5-85	374
Table 5-87: Effect of Thermal Cycling (either Ambient or Vacuum) on the Linear Thermal Expansion, β_o , of the Hybrid Tubes Identified as Spec. No. 1 in Table 5-84 and Table 5-85 ^a	374

European Foreword

This document (CEN/CLC/TR 17603-31-05:2021) has been prepared by Technical Committee CEN/CLC/JTC 5 "Space", the secretariat of which is held by DIN.

It is highlighted that this technical report does not contain any requirement but only collection of data or descriptions and guidelines about how to organize and perform the work in support of EN 16603-31.

This Technical report (TR 17603-31-05:2021) originates from ECSS-E-HB-31-01 Part 5A.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN [and/or CENELEC] shall not be held responsible for identifying any or all such patent rights.

This document has been prepared under a mandate given to CEN by the European Commission and the European Free Trade Association.

This document has been developed to cover specifically space systems and has therefore precedence over any TR covering the same scope but with a wider domain of applicability (e.g.: aerospace).

1

Scope

In this Part 5 of the spacecraft thermal control and design data handbooks, clause 4 contains technical data on the metallic alloys used in spacecrafts is given: composition, application areas, properties and behaviour from a thermal and thermo-optics point of view, degeneration and aging. All other properties of the metallic alloys are outside the scope of this document.

Properties of composite materials combined to form heterogeneous structures are given in clause 5.

The Thermal design handbook is published in 16 Parts

TR 17603-31-01	Thermal design handbook – Part 1: View factors
TR 17603-31-02	Thermal design handbook – Part 2: Holes, Grooves and Cavities
TR 17603-31-03	Thermal design handbook – Part 3: Spacecraft Surface Temperature
TR 17603-31-04	Thermal design handbook – Part 4: Conductive Heat Transfer
TR 17603-31-05	Thermal design handbook – Part 5: Structural Materials: Metallic and Composite
TR 17603-31-06	Thermal design handbook – Part 6: Thermal Control Surfaces
TR 17603-31-07	Thermal design handbook – Part 7: Insulations
TR 17603-31-08	Thermal design handbook – Part 8: Heat Pipes
TR 17603-31-09	Thermal design handbook – Part 9: Radiators
TR 17603-31-10	Thermal design handbook – Part 10: Phase – Change Capacitors
TR 17603-31-11	Thermal design handbook – Part 11: Electrical Heating
TR 17603-31-12	Thermal design handbook – Part 12: Louvers
TR 17603-31-13	Thermal design handbook – Part 13: Fluid Loops
TR 17603-31-14	Thermal design handbook – Part 14: Cryogenic Cooling
TR 17603-31-15	Thermal design handbook – Part 15: Existing Satellites
TR 17603-31-16	Thermal design handbook – Part 16: Thermal Protection System

2 References

EN Reference	Reference in text	Title
EN 16601-00-01	ECSS-S-ST-00-01	ECSS System - Glossary of terms
TR 17603-31-04	ECSS-E-HB-31-01 Part 4	Thermal design handbook – Part 4: Conductive Heat Transfer
TR 17603-31-12	ECSS-E-HB-31-01 Part 12	Thermal design handbook – Part 12: Louvers
TR 17603-31-13	ECSS-E-HB-31-01 Part 14	Thermal design handbook – Part 14: Cryogenic Cooling

All other references made to publications in this Part are listed, alphabetically, in the **Bibliography**.

Terms, definitions and symbols

3.1 Terms and definitions

For the purpose of this Standard, the terms and definitions given in ECSS-S-ST-00-01 apply.

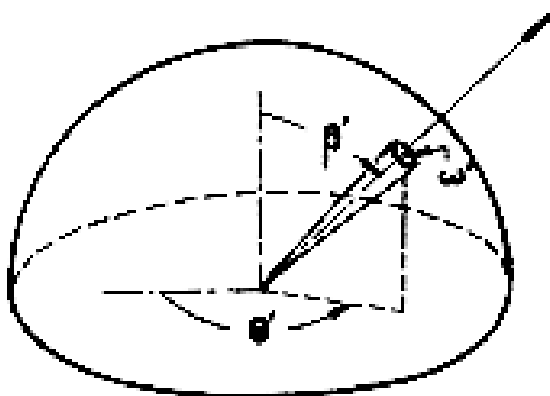
3.2 Symbols

B	magnetic induction, [T]
E	modulus of elasticity, [Pa]
H	magnetic field strength, [A.m ⁻¹]
R	reflectance factor
c	specific heat, [J.kg ⁻¹ .K ⁻¹]
k	thermal conductivity, [W.m ⁻¹ .K ⁻¹]
$\Delta L/L$	thermal expansion
α	thermal diffusivity, [m ² .s ⁻¹] $\alpha = k/\rho c$
α	temperature coefficient of electrical resistivity, [K ⁻¹]
α	hemispherical total absorptance
$\alpha'(\beta, \theta)$	directional total absorptance
α_s	normal solar absorptance
$\alpha_\lambda(\lambda)$	hemispherical spectral absorptance
$\alpha'_\lambda(\lambda, \beta, \theta)$	directional spectral absorptance
β	mean coefficient of linear thermal expansion, [K ⁻¹] angle between surface normal and direction of incident flux, [angular degrees]
β'	angle between surface normal and direction of emitted, reflected or transmitted flux, [angular

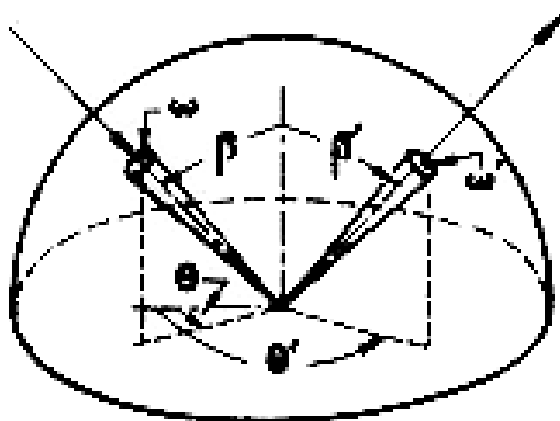
	degrees]
ε	hemispherical total emittance
$\varepsilon'(\beta', \theta')$	directional total emittance
$\varepsilon_\lambda(\lambda)$	hemispherical spectral emittance
$\varepsilon'_\lambda(\lambda, \beta', \theta')$	directional spectral emittance
θ	azimuthal angle of incident flux, [angular degrees]
θ'	azimuthal angle of emitted, reflected or transmitted flux, [angular degrees]
λ	wavelength, [m]
μ/μ_0	relative magnetic permeability
ρ	density, [kg.m ⁻³]
	hemispherical total reflectance
$\rho_\lambda(\lambda)$	hemispherical spectral reflectance
$\rho'(\beta, \theta)$	directional-hemispherical total reflectance
$\rho'(\beta', \theta')$	hemispherical-directional total reflectance
ρ'_s	normal-hemispherical solar reflectance
$\rho'_\lambda(\lambda, \beta, \theta)$	directional-hemispherical spectral reflectance
$\rho'_\lambda(\lambda, \beta', \theta')$	hemispherical-directional spectral reflectance
$\rho''(\beta, \theta, \beta', \theta')$	bidirectional total reflectance.
$\rho''_\lambda(\lambda, \beta, \theta, \beta', \theta')$	bidirectional spectral reflectance
$\rho''_s(\beta, \theta, \beta', \theta')$	bidirectional solar reflectance
σ	electrical conductivity, [$\Omega^{-1} \cdot m$] σ^{-1} , electrical resistivity [$\Omega \cdot m$]
σ_{ult}	ultimate tensile strength, [Pa]
$\tau'_\lambda(\lambda, \beta, \theta, \beta', \theta')$	bidirectional spectral transmittance
ω	solid angle of incident radiation beam [steradians]
ω'	solid angle of emitted, reflected or transmitted radiation beam, [steradians]

The sketches below show the angles used to characterize the radiative fluxes arriving at or leaving a surface element.

Angles used to define directional emittance



Angles used to define bidirectional reflectance



Metallic materials

4.1 General

Data for each alloy are arranged as indicated below. When no data on some property are available the heading is omitted.

1. TYPICAL COMPOSITION, PERCENT

2. OFFICIAL DESIGNATIONS

3. PHYSICAL PROPERTIES

3.1. Density

3.2. Thermal properties

3.2.1. Specific heat

3.2.2. Thermal conductivity

3.2.3. Thermal diffusivity

3.2.4. Thermal expansion

3.2.5. Melting range

3.3. Thermal radiation properties

3.3.1. Emittance

3.3.1.1. Directional spectral emittance

3.3.1.1.1. Normal spectral emittance

3.3.1.1.2. Angular spectral emittance

3.3.1.2. Directional total emittance

3.3.1.2.1. Normal total emittance

3.3.1.3. Hemispherical spectral emittance

3.3.1.4. Hemispherical total emittance

3.3.2. Absorptance

3.3.2.1. Directional spectral absorptance

3.3.2.1.1. Normal spectral absorptance

3.3.2.2. Directional total absorptance

3.3.2.2.1. Normal total absorptance

3.3.2.3. Hemispherical spectral absorptance

3.3.2.4. Hemispherical total absorptance

3.3.2.5. Solar absorptance

3.3.2.5.1. Normal solar absorptance

3.3.2.5.2. Angular solar absorptance

3.3.2.6. Absorptance to emittance ratio

3.3.3. Reflectance

3.3.3.1. Bidirectional spectral reflectance

3.3.3.1.1. Normal-normal spectral reflectance

3.3.3.1.2. Angular (non-normal) spectral reflectance

3.3.3.2. Directional-hemispherical spectral reflectance

3.3.3.2.1. Normal-hemispherical spectral reflectance

3.3.3.2.2. Angular-hemispherical spectral reflectance

3.3.3.3. Hemispherical-directional spectral reflectance

3.3.3.3.1. Hemispherical-normal spectral reflectance

3.3.3.4. Hemispherical spectral reflectance

3.3.3.5. Bidirectional total reflectance

3.3.3.5.1. Normal-normal total reflectance

3.3.3.5.2. Angular (non-normal) total reflectance

3.3.3.6. Directional-hemispherical total reflectance

3.3.3.6.1. Normal-hemispherical total reflectance

3.3.3.7. Hemispherical-directional total reflectance

3.3.3.7.1. Hemispherical-normal total reflectance

3.3.3.8. Bidirectional solar reflectance

3.3.3.8.1. Normal-normal solar reflectance

3.3.3.9. Directional-hemispherical solar reflectance

3.3.3.9.1. Normal-hemispherical solar reflectance

3.3.4. Transmittance

3.3.4.1. Bidirectional spectral transmittance

3.3.4.1.1. Normal-normal spectral transmittance

3.3.4.1.2. Angular (non-normal) spectral transmittance

3.4. Other physical properties

3.4.1. Electrical resistivity

3.4.2. Magnetic properties

4. ENVIRONMENTAL BEHAVIOR

4.1. Prelaunch

4.2. Postlaunch

5. CHEMICAL PROPERTIES

5.1. Solution potential

5.2. Corrosion resistance

6. FABRICATION

6.1. Casting

6.2. Forming

6.3. Welding

6.4. Machining

6.5. Heat treatment

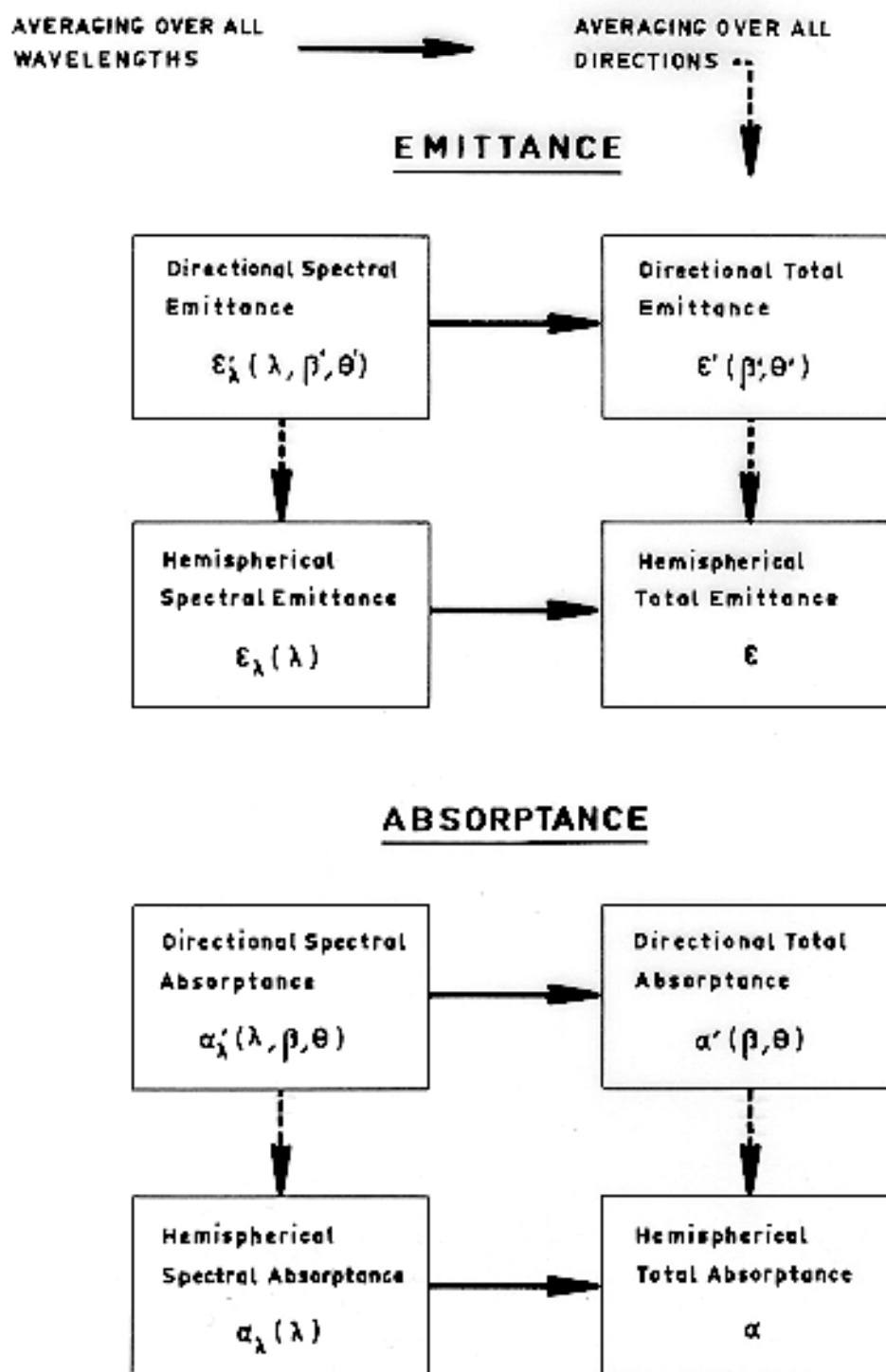
6.6. Anodizing

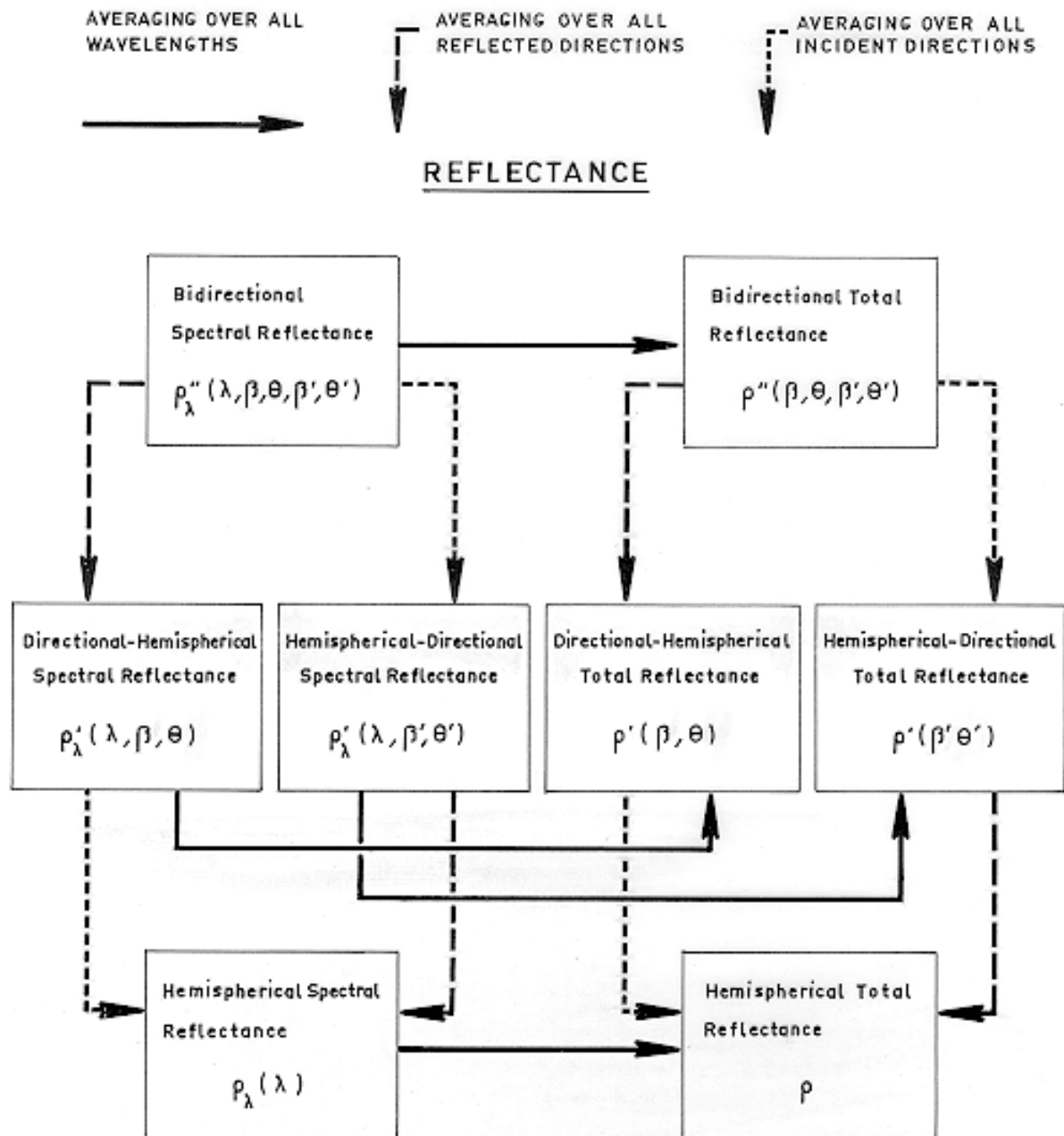
7. AVAILABLE FORMS AND CONDITIONS

8. USEFUL TEMPERATURE RANGE

9. APPLICATIONS

4.1.1 Modifiers of thermal radiative properties





4.1.2 Cladding definitions

Clad. A composite metallic material containing two or three layers that have been bonded together. Bonding may be achieved by co-rolling, welding, casting, heavy chemical deposition or heavy electroplating.

Alclad. Clad produced by bonding either a corrosion-resistant aluminium alloy or high purity aluminium to a base of a structurally stronger aluminium alloy.

Nonclad. Metallic material to which no other alloy has been bonded by cladding.

4.1.3 Temper designation for heat treatable aluminium alloys

F Condition: As fabricated.

O Condition: Annealed (wrought products only).

W Condition: Solution heat treated.

T1 Condition: Naturally aged to a stable condition.

T2 Condition: Annealed (cast products only).

T3 Condition: Solution heat treated, cold worked, and naturally aged to a substantially stable condition.

T4 Condition: Solution heat treated and naturally aged to a substantially stable condition.

T5 Condition: Artificially aged only.

T6 Condition: Solution heat treated and artificially aged.

T7 Condition: Solution heat treated and over aged.

T8 Condition: Solution heat treated, cold worked, and artificially aged. Different amounts of cold working are denoted by a second digit.

T9 Condition: Solution heat treated, artificially aged and cold worked.

T10 Condition: Artificially aged and cold worked.

4.2 Aluminium alloys

ALLOYS Al - 99,99. Al - 99,9. Al - 99,8. Al - 99,7. Al - 99,5. Al - 99,3. Al - 99.

This data item concerns all aluminium alloys whose aluminium content is above 99%.

1. TYPICAL COMPOSITION, PERCENT. Maximum values are given except for Aluminium.

	Al	Cu	Fe	Mn	Si	Zn	Others	
							Each	Total
Al - 99,99	>99,99	-	-	-	-	-	-	0,01
Al - 99,9	>99,9	0,02	0,07	0,01	0,07	0,03	0,01	-
Al - 99,8	>99,8	0,03	0,15	0,03	0,15	0,06	0,02	-
Al - 99,7	>99,7	0,03	0,25	0,03	0,20	0,07	0,03	-
Al - 99,5	>99,5	0,05	0,40	0,05	0,30	0,10	0,03	-
Al - 99,3	>99,3	0,10	0,60	0,05	0,30	0,10	0,05	-
Al - 99,0	>99,0	0,20	0,80	0,05	0,50	0,10	0,05	-

2. OFFICIAL DESIGNATIONS

	AECMA	ISO	AFNOR	AMS	BS	DIN
Al - 99,99					1	Al 99,98R S - Al 99,98R 3,0385
Al - 99,9						Al 99,9 3,0305
Al - 99,8		Al 99,8	A8		1A	Al 99,8 S - Al 99,8 3,0285
Al - 99,7		Al 99,7	A7	~4000		Al 99,7 3,0275
Al - 99,5	Al P 99,5	Al 99,5	A5	~4000	1B ~1E	Al 99,5 S - Al 99,5 3,0255 ~E - Al ~3,0257
Al - 99,3			~A45	4040 4041 4042		~S - Al 99,5Ti ~3,0805
Al - 99,0		Al 99,0 ~Al 99,0Cu	A4	~1100 4001 4003 4062 4102 4180 7220	1C	Al 99 3,0205

NOTE ~ Can be approximately included with those alloys having the indicated aluminium content.

3. PHYSICAL PROPERTIES

3.1. Density.

Al - 99,99, $\rho = 2699 \text{ kg.m}^{-3}$. (Pennington (1961) [29]).

Al - 99,5 $\rho = 2700 \text{ kg.m}^{-3}$. (Kappelt (1961) [23]).

Al - 99,0 $\rho = 2710 \text{ kg.m}^{-3}$. (Kappelt (1961) [23]).

3.2. Thermal properties

3.2.1. Specific heat

Effect of temperature on specific heat: Figure 4-1.

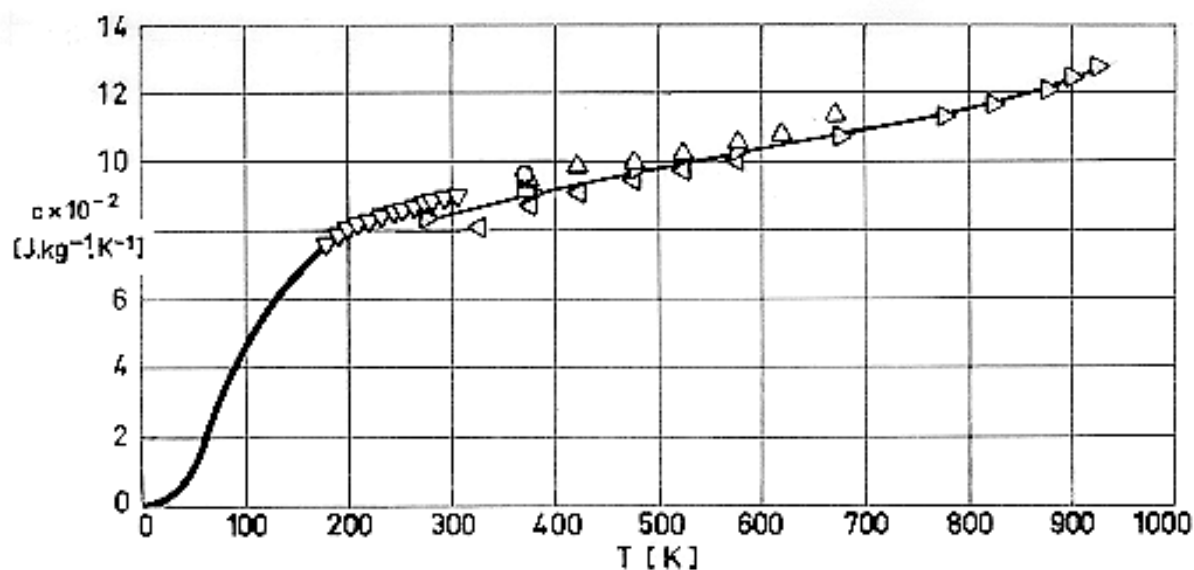


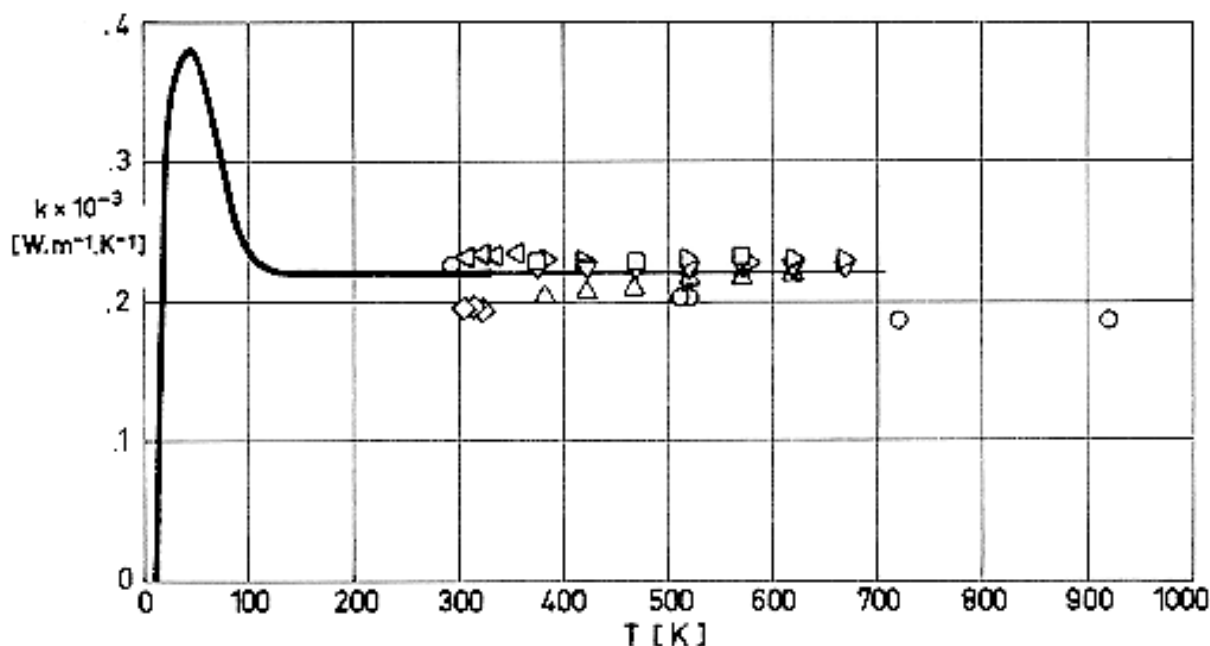
Figure 4-1: Specific heat, c , of Aluminium as a function of temperature, T .

Explanation

Key	Description	Comments	References
○	Al - 99,0		Kappelt (1961) [23].
□	Al - 99,99		Pennington (1961) [29].
△	Al - 99,99 Average of 2 samples 1) Water quenched from 873 K; annealed 100 h at 403 K. 2) Cooled from 873 K at 5 K.min ⁻¹	Reported error ≤ 1%	Touloukian (1967)a [38]
▽	Al 99,9 Single crystal. Melted and cooled 2 d in vacuum.		
▷	Al - 99,9	Reported error ± 5%	
◁		Reported error ± 5%	
—			Coston (1967) [18].

3.2.2. Thermal conductivity

Effect of temperature on thermal conductivity: Figure 4-2.



Note: non-si units are used in this figure

Figure 4-2: Thermal conductivity, κ , of Aluminium as a function of temperature, T .

Explanation

Key	Description	Comments	References
○	Al - 99,9	Losses evaluated by measuring unsteady state cooling of rod initially at uniform temperature.	Touloukian (1967)a [38]
□	0,04 Si - 0,03 Fe - 0,006 Cu - 0,005 Ti, and traces of Mn and Mg. Annealed 1 h at 723 K and cooled slowly.	Reported error ± 3%.	
△	Al - 99,5 Cast at 973 K into molds at 473 K; rolled and drawn, then turn into rods.		
▽	Al - 99,9 Same treatment as above.		
▷	Al - 99,9 Same treatment as above.		
◁	Al 99,99	Reported error ± 1%.	
◇	Commercially pure.	Reported error ± 3%.	

Key	Description	Comments	References
	Sample 2×10^{-2} m in diameter and $1,8 \times 10^{-2}$ m length.		
—			Coston (1967) [18].

Thermal conductivity integrals: Figure 4-3.

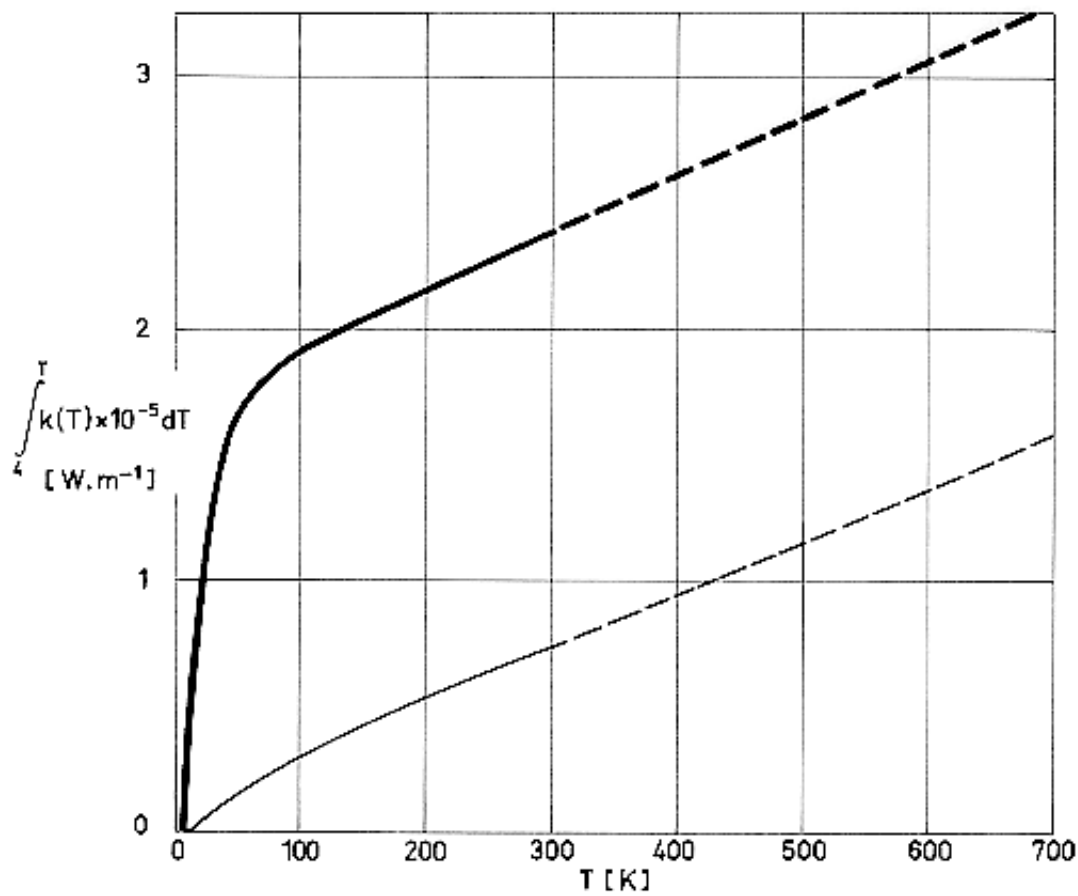


Figure 4-3: Thermal conductivity integrals of Aluminium as a function of temperature, T .

Explanation

- : Al - 99,99. From Coston (1967) [18].
- - -: Al - 99,0. From Coston (1967) [18].
- — —: Straight line whose slope has been calculated by the compiler by fitting the experimental data points $\triangleright$ and $\triangleleft$ of Figure 4-2 with the least-squares method.
- — —: Calculated by the compiler from data points $\diamond$ of Figure 4-2

3.2.3. Thermal diffusivity.

Effect of temperature on thermal diffusivity: Figure 4-4.

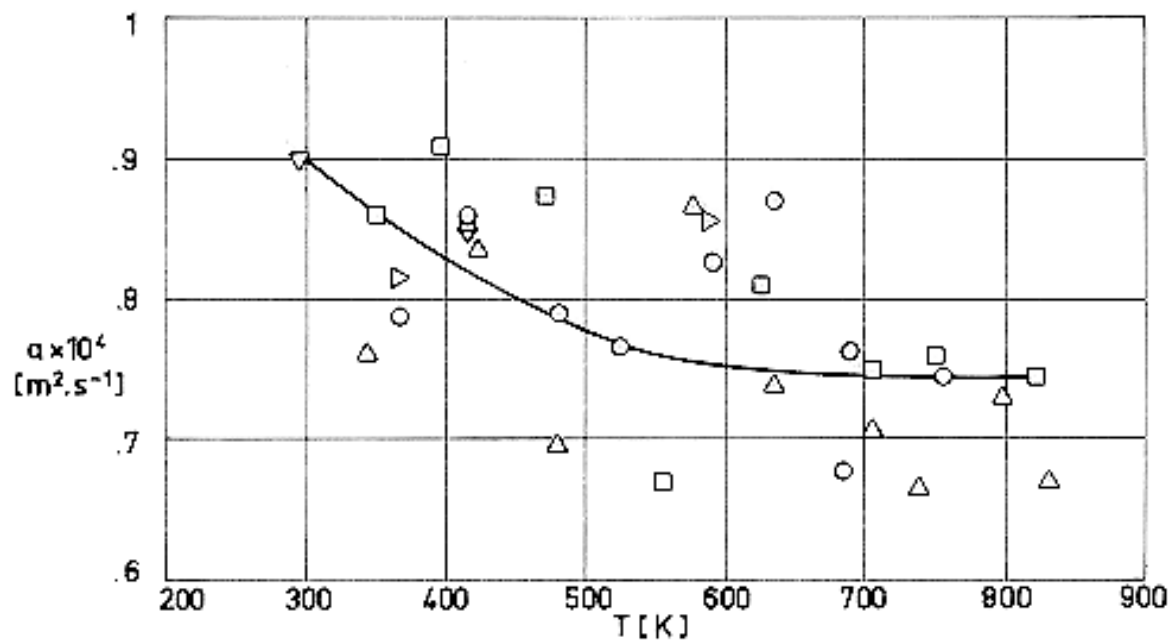


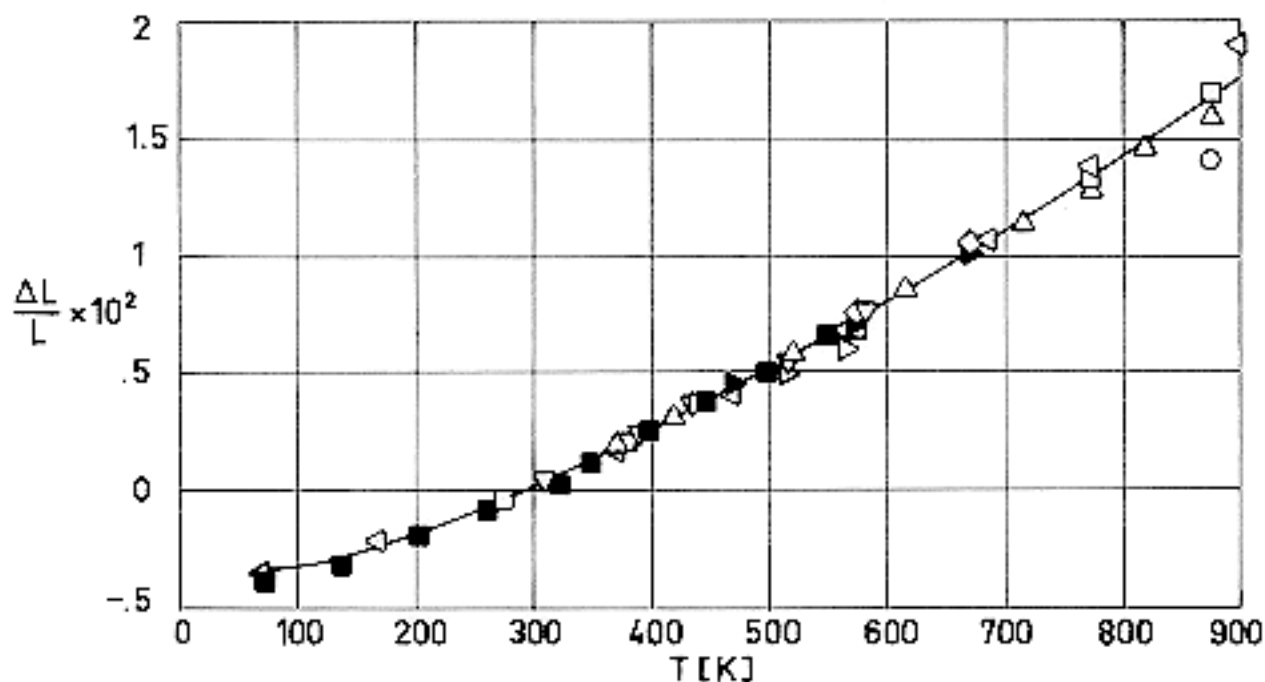
Figure 4-4: Thermal diffusivity, α , of Aluminium as a function of temperature, T .

Explanation

Key	Description	Comments	References
○	Al - 99,9	Reported error $\pm 11\%$.	Touloukian (1967)a [38].
□	Same as above.	Second run of the above specimen. Reported error $\pm 11\%$.	
△	Same as above.	Third run of the above specimen. Reported error $\pm 11\%$.	
▽	Pure. 1.9×10^{-3} m ² square cross-section and 3.52×10^{-3} m length.	Reported error $\pm 5\%$.	
▷	Pure.		

3.2.4. Thermal expansion.

Effect of temperature on thermal expansion: Figure 4-5.



Note: non-si units are used in this figure

Figure 4-5: Linear thermal expansion, $\Delta L / L$, of Aluminium as a function of temperature, T .

Explanation

Key	Description	Comments	References
○			Touloukian (1967)a [38].
□	Al - 99,99 Annealed above 873 K.		
■	Al - 99,99		
△	Al - 99,9 Annealed 2 h at 893 K and cooled slowly.		
▽	99,952 Al - 0,019 Cu - 0,015 Fe - 0,014 Si. Cast in graphite mold.		
▷	Chemically pure.	X-ray diffraction method.	

Key	Description	Comments	References
◁	99,989 Al - 0,004 each Si, Cu - 0,003 Fe.		
►	Pure. Pressed rod made of sintered aluminium powder.		
◇	Al - 99,5		

Mean coefficient of linear thermal expansion, β .

The available information concerning thermal expansion coefficients of these alloys seems to indicate that there is no noticeable influence of the aluminium content on β . Values given below correspond to Al - 99,99.

T [K]	73-293	123-293	173-293	223-293	293-373	293-473	293-573	293-673	293-773
$\beta \times 10^6$ [K ⁻¹]	18,0	19,9	21,0	21,8	23,6	24,5	25,5	26,4	27,4

From Pennington (1961) [29].

3.2.5. Melting range

Al - 99,99: 933 K. (Pennington (1961) [29]).

Al - 99,5: 919 K - 930 K. (Kappelt (1961) [23]).

Al - 99,0: 916 K - 930 K. (Kappelt (1961) [23]).

3.3. Thermal radiation properties

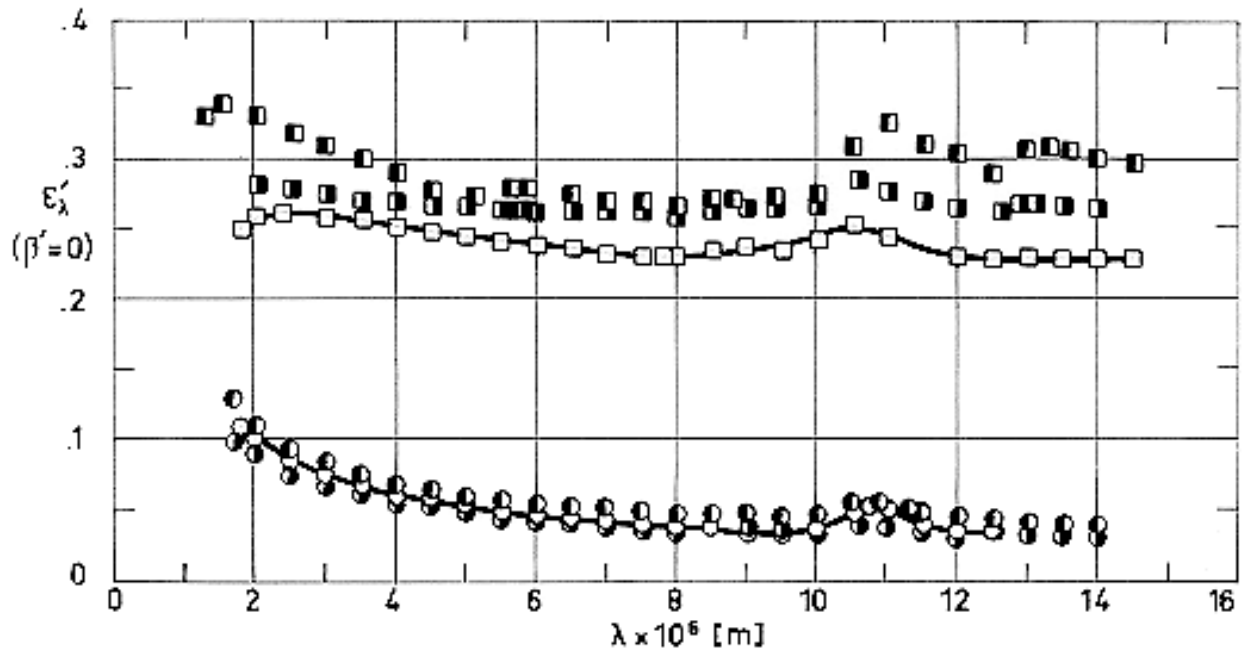
3.3.1. Emittance

Data concerning emittance have been arranged as indicated in the following Table.

3.3.1.1. Directional spectral emittance.				
Clause	Heading	Data presented	Fig.	Table
3.3.1.1.1.	Normal $\beta' = 0$	Al - 99,7	Figure 4-6	
		Aluminium conversion coatings.	Figure 4-7	
3.3.1.1.2.	Angular (non-normal) $\beta' \neq 0$	Al - 99,0	Figure 4-7	
3.3.1.2. Directional total emittance.				

3.3.1.2.1.	Normal $\beta' = 0$	Aluminium.		Table 4-1
		Aluminium. Effect of temperature.	Figure 4-9	
		Aluminium contact coatings.		Table 4-2 ^a
		Aluminium conversion coatings.		Table 4-3 ^a
		Aluminium conversion coatings. Effect of anodizing thickness.	Figure 4-10	
3.3.1.4. Hemispherical total emittance.				
	$\omega' = 2\pi$	Aluminium. Effect of temperature.	Figure 4-11	
		Aluminium contact coatings.		Table 4-4
		Aluminium conversion coatings. Effect of anodizing thickness.	Figure 4-12	

^a Solar absorptance, α_s , has been also included in this Table in order to save space.



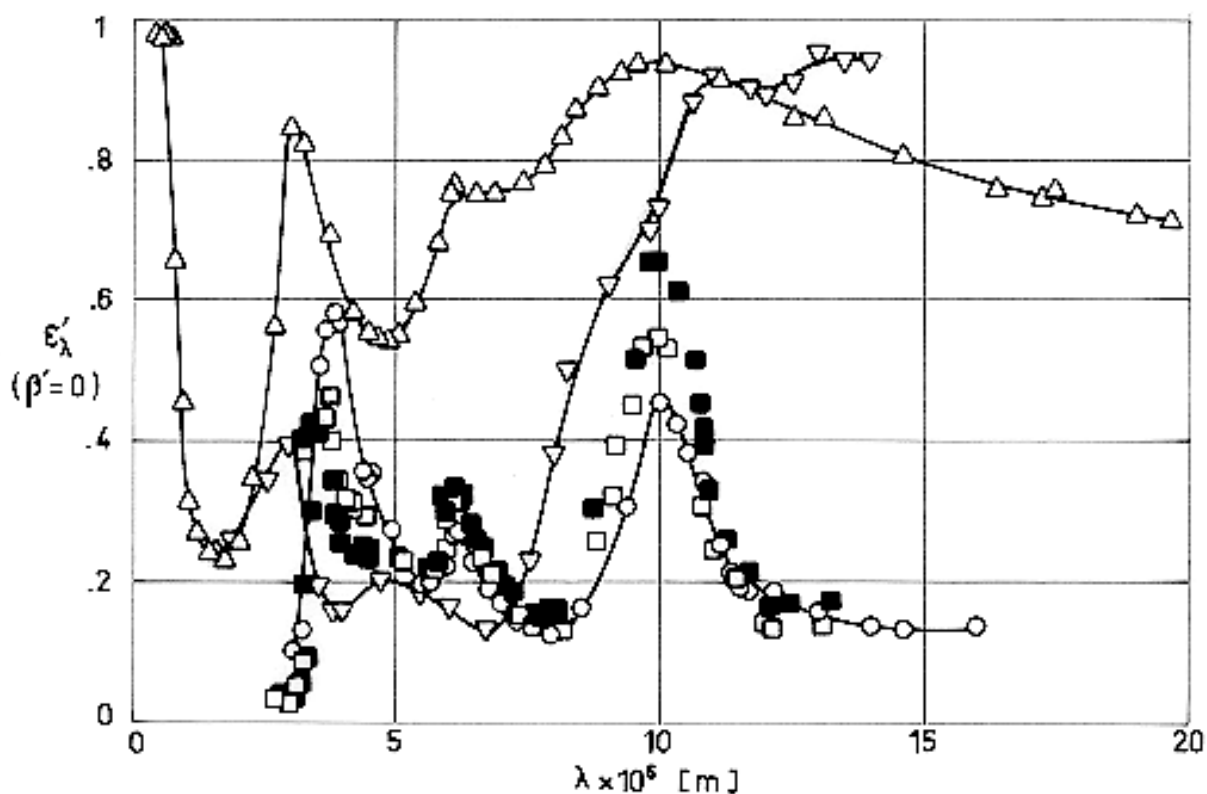
Note: non-si units are used in this figure

Figure 4-6: Normal spectral emittance, ϵ_{λ}' , of Aluminium as a function of wavelength, λ .

Explanation

Key	Description	Comments	References
○	99,7 Al - 0,11 Fe - 0,11 Si - 0,01 Cu - 0,01 Mg - <0,01 Mn, Ni, Zn. Cylindrical tube. Heated at 467 K for 15 h. Polished. Surface roughness: $7,62 \times 10^{-8}$ m (center line average).	Sample temperature: $T = 599$ K. Data from smooth curve. Reported error $\pm 20\%$ (in the wavelength range 2×10^{-6} to 10^{-5} m).	Touloukian & DeWitt (1970) [42].
●	Same as ○ except heated at 697 K for 20 h.	Same as ○ except $T = 697$ K.	
●	Same as ○ except heated at 805 K for 15 h.	Same as ○ except $T = 805$ K.	
□	Same specimen as ○ except heated at 462 K for 25 h. Roughness and knurled with grade 180 silicon carbide paper. Surface roughness: $2,92 \times 10^{-6}$ m (centre line average).	$T = 462$ K. Data from smooth curve. Reported error $\pm 10\%$ (in the wavelength range 2×10^{-6} to 10^{-5} m).	

Key	Description	Comments	References
■	Same as □ except heated at 598 K for 22 h.	Same as □ except $T = 599$ K.	
■	Same as □ except heated at 715 K for 27 h.	Same as □ except $T = 715$ K.	



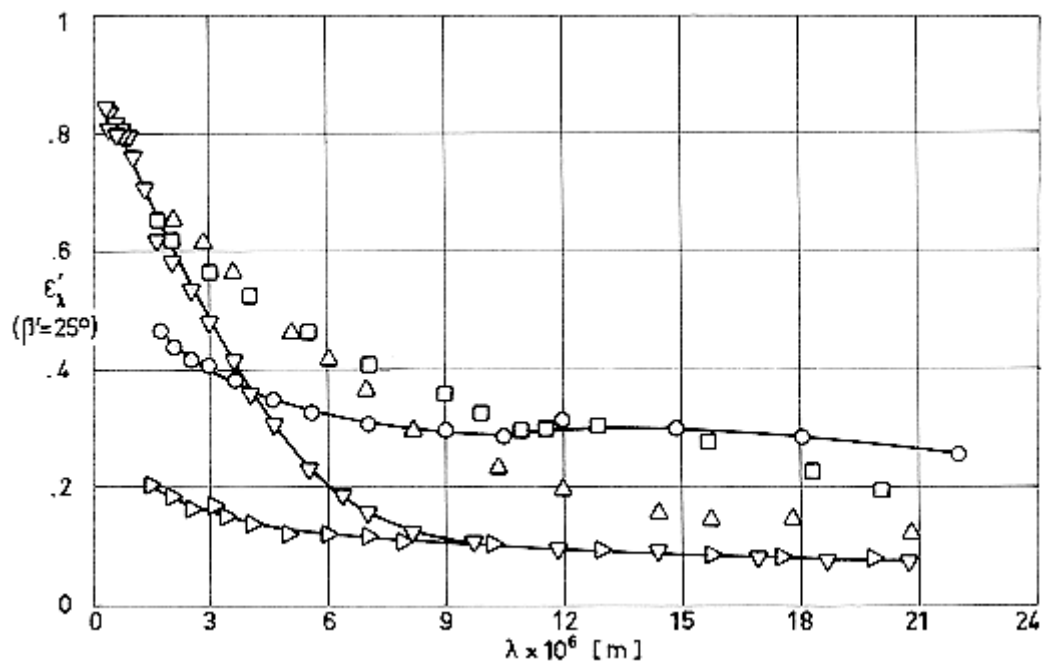
Note: non-si units are used in this figure

Figure 4-7: Normal spectral emittance, ε'_λ , of Aluminium conversion coatings as a function of wavelength, λ .

Explanation

Key	Description	Comments	References
○	Alodine 401.45. Reaction of an aluminium surface with an aqueous solution of chromic, phosphoric, and hydrofluoric acid. Substrate: Al - 99,8 (Echo II).	Sample temperature: $T = 295$ K. Data from smooth curve. Converted from $R(2\pi, 0)$.	Touloukian, DeWitt & Hernicz (1972) [43].
□	Same as ○ except reacted for 20 s in a 1 N		

Key	Description	Comments	References
	sodium hydroxide solution at 298 K, then washed in water and dried in air.		
■	Same as □. Reacted for 40 s.		
△	Black anodized.	$T = 323$ K. Data from smooth curve. Converted from $R(2\pi, 0)$.	
▽	Al - 99.7. Anodized 30 min at 10^{-2} A.m $^{-2}$ in 4 N analar sulphuric acid at 293 K, sealed for 30 min in boiling distilled water. Anodizing thickness $2,54 \times 10^{-6}$ m. Heated at 456 K for 15 h.	$T = 461$ K. Data from smooth curve. Reported error $\pm 10\%$.	



Note: non-si units are used in this figure

Figure 4-8: Angular spectral emittance, ε'_λ , of Aluminium as a function of wavelength, λ .

Explanation

Key	Description	Comments	References
○	Al - 99.0. Nominal composition. Sandblasted with 120 mesh alumina (mesh opening $1,25 \times 10^{-4}$ m).	Sample temperature:	Touloukian & DeWitt (1970) [42].

Key	Description	Comments	References
□	Same as ○ except sandblasted with 320 mesh alumina (mesh opening $4,6 \times 10^{-5}$ m).	$T = 306$ K. Authors assumed $\alpha = \varepsilon = 1 - \rho$. $\rho (25^\circ, 2\pi)$.	
△	Same as ○ except sandblasted with 600 mesh alumina (mesh opening $2,4 \times 10^{-5}$ m).		
▽	Same as ○ except sandblasted with 1000 mesh alumina (mesh opening $1,4 \times 10^{-5}$ m).		
▷	Same as ○ except sanded with 280 mesh silicon carbide paper.		

Table 4-1: Normal Total Emittance of Aluminium

Alloy	T [K]	ε' ($\beta' = 0$)	Comments	References
Al - 99,99	298	0,03		Pennington (1961) [29]
Al - 99,0		0,05	Polished	Zerlaut, Carrol & Gates (1966) [47].
Al -		0,21	Foil, vapor blasted, wet.	
Al - 99,0		0,33	Sandblasted.	
Al -	311	0,065	Bright foil roughened with abrasive cloth.	Touloukian (1967)a [38].
Al -	373	0,18	Sheet, rough polished.	
Al - 99,99		0,02	Foil ($1,27 \times 10^{-4}$ m thick) GMC Bright dip for 10 min at 350 K.	Bevans (1969) [14].
Al -	296	0,04	Polished.	TRW (1970) [44].
Al -	298	0,055 to 0,070	Rough plate.	
Al -		0,04	Bare metal.	Scollon & Carpitella (1970) [33].
Al - 99,0	370	0,022	Polished with MgO and water, measured in vacuum ($2,1 \times 10^{-2}$ Pa).	Touloukian & DeWitt (1970) [42].
Al - 99,99	425,4	0,037	Rolled, polished.	

Alloy	T [K]	ε' ($\beta' = 0$)	Comments	References
Al - 99,99	647	0,045	Same as above.	
Al - 99,99	780	0,0497	Same as above.	
Al - 99,99	414	0,0486	Highly polished.	
Al - 99,99	610	0,0576	Same as above.	
Al - 99,99	733	0,065	Same as above.	
Al -	366	0,028	Foil.	
Al -	311	0,045	Foil, embossed (Pattern No. 1).	
Al -	311	0,056	Foil, embossed (Pattern No. 2).	
Al -	311	0,047	Foil, embossed (Pattern No. 3).	
Al -	311	0,056	Foil, embossed (Pattern No. 4).	
Al -	311	0,061	Foil, embossed (Pattern No. 5).	
Al - 99,9	311	0,045	0,002 Si, 0,0001 Fe, 0,001 Cu, 0,0003 Na, 0,0003 Ca, 0,0003 Mg. Electrolytically brightened, density 2698 kg.m ⁻³ at 298 K. aluminium foil reference ($\varepsilon = 0,05$).	
Al -	311	0,035 to 0,050	Foil, bright; etched in hot sodium hydroxide solution 0,5 to 2 min, and dipped in nitric acid.	
Al -	311	0,044	Foil, bright; roughened with abrasive cloth (No. 120 Aloxite cloth).	
Al -	311	0,063	Foil, bright; roughened with abrasive cloth (No. 120 Aloxite cloth).	
Al -	311	0,066	Foil, bright; roughened with abrasive cloth (No. 120 Aloxite cloth).	
Al -	311	0,04	Foil, surface film formed by means of exposure to corrosive attack; foil-covered cardboard taken from foil-insulated dry-ice cabinet	

Alloy	T [K]	ε' ($\beta' = 0$)	Comments	References
			exposed to weather on beach during 8 months.	
Al -	311	0,05	Foil; suspended vertically in the laboratory for 3 years and measured with the accumulated dust and fume.	
Al -	311	0,09	Foil; chemically oxidized by treating with hot solution of sodium carbonate and chromate.	
Al -	311	0,10	Foil; lacquer coated; heated to partially decompose lacquer and color in brown.	
Al -	311	0,10	Foil after 2 years exposure to salt spray and moisture at seashore.	
Al -	373	0,09	Commercial sheet.	
Al -	373	0,095	Sheet, polished.	

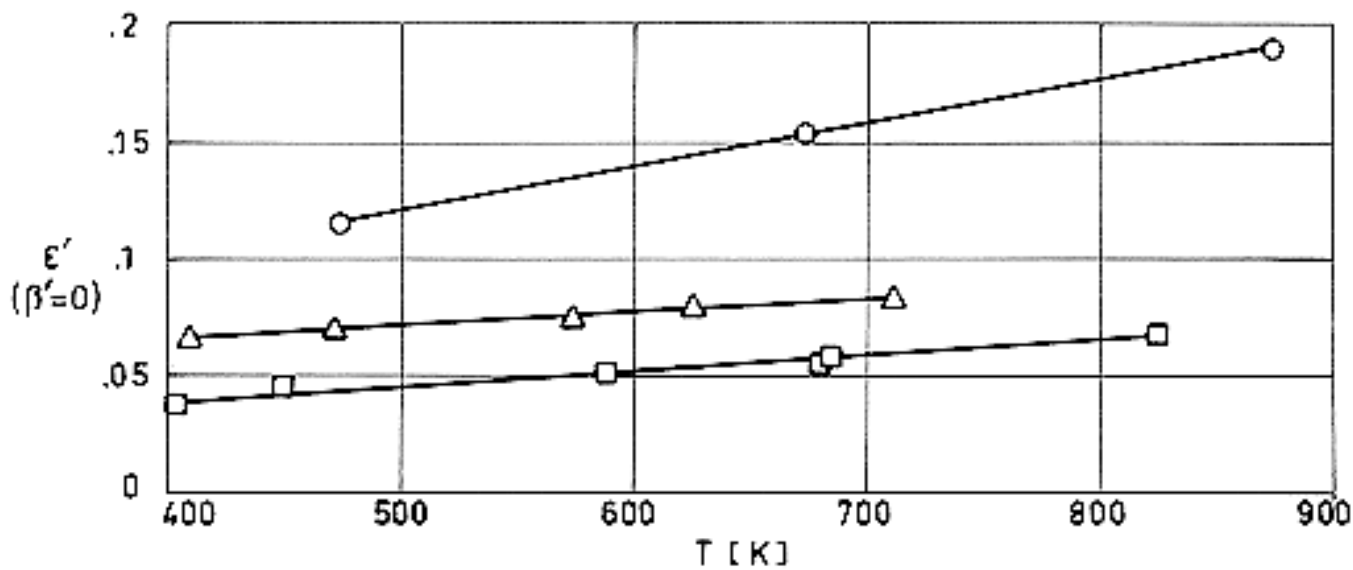
Table 4-2: Normal Total Emittance and Normal Solar Absorptance of Aluminium Contact Coatings

Alloy	T [K]	ε' ($\beta' = 0$)	α_s ($\beta = 0$)	Comments	References
Al -		0,03	0,10	Vacuum deposited (opaque thickness) on aluminium sheet with resin undercoat.	Bevans (1969) [14].
Al -		0,03	0,09	Vacuum deposited (opaque thickness) on aluminium foil, Reynolds Wrapp.	
Al -		0,04	0,21	Vacuum deposited (opaque thickness) on Beryllium foil.	
Al -		0,03	0,09	Vacuum deposited (opaque thickness) on Mylar film $2,5 \times 10^{-5}$ m thick.	
Al -		0,014	0,08	10^{-7} to 2×10^{-7} m thick aluminium	Scollon & Carpitella

Alloy	T [K]	ε' ($\beta' = 0$)	α_s ($\beta = 0$)	Comments	References
				vapor deposited on unspecified surface. Polished surface. Measured in vacuum.	(1970) [33].
Al -		0,051	0,15	Same as above. Measured in air.	
Al -		0,024	0,13	Vapor deposited aluminium on Mylar.	
Al -		$\leq 0,05$	$\leq 0,13$	Vapor deposited aluminium on $1,2 \times 10^{-5}$ m thick Kapton. Data for metallic side. Silicone pressure sensitive adhesive. Schjeldahl.	
Al -		$\leq 0,06$	0,10 to 0,14	Vapor deposited aluminium on Kapton . Data for metallic side. Silicone pressure sensitive tape. Schjeldahl G-103500 tape.	
Al -		0,13 to 0,17	0,12 to 0,16	Vapor deposited aluminium on $1,2 \times 10^{-5}$ m thick Kapton plus nylon tulle. Data for metallic surface. Acrylic pressure sensitive adhesive. Second surface reflector. Schjeldahl G-102000 tape.	
Al -		0,025	0,11	$1,5 \times 10^{-7}$ m thick evaporated aluminium on Quartz.	McCargo, Spradley, Greenberg & McDonald (1971) [26].

Table 4-3: Normal Total Emittance and Normal Solar Absorptance of Aluminium Conversion Coatings

Alloy	T [K]	ε' ($\beta' = 0$)	α_s ($\beta = 0$)	Comments	References
Al - 99,99		0,77	0,20	Hard anodized, 8×10^{-6} m thick, with sulphuric acid electrolyte 11% by weight, at 270 K.	Bevans (1969) [14].
Al - 99,99		0,79	0,14	Soft anodized, $1,3 \times 10^{-5}$ m thick, with sulphuric acid electrolyte 15% by weight, at 270 K.	
Al - 99,7		0,82	0,24	Soft anodized, $1,3 \times 10^{-5}$ m thick, with sulphuric acid electrolyte 16% by weight, at 294 K.	
Al - 99,7		0,74	0,40	Anodized, 8×10^{-6} m thick, with chromic acid electrolyte 5% by weight, at 308 K, anodizing voltage 40V DC, 120 min.	
Al - 99,99		0,08	0,27	Anodized, citric acid electrolyte 1 kg.m ⁻³ ammonium citrate, at 295 K, anodizing voltage: 300V DC, 60 min.	
Al - 99,7		0,86	0,31	Anodized, 2×10^{-5} m thick, oxalic acid solution 3% by weight, at 311 K, anodizing voltage: 30V DC, 60 min.	
Al - 99,99		0,39	0,33	Anodized, sulphamic acid electrolyte 100 kg.m ⁻³ , at 294 K, anodizing voltage: 45V DC, 30 min.	
Al - 99,99		0,77	0,64	Anodized, sulphamic acid electrolyte 100 kg.m ⁻³ , at 294 K, anodizing voltage: 15V DC, 30 min.	
Al - 99,99		0,03	0,27	Anodized, sulphamic acid electrolyte 100 kg.m ⁻³ , at 294 K, anodizing voltage: 5,5V DC, 15 min.	
Al -		0,73	0,70	Chromic acid anodized. Chemical surface finish. Degradation caused by deposition of outside contaminants (73 h in low earth orbit on board Apollo 9).	Scollon & Carpitella (1970) [33].
Al -		0,90		Carbon black impregnated anodized coating. Chemical surface finish.	

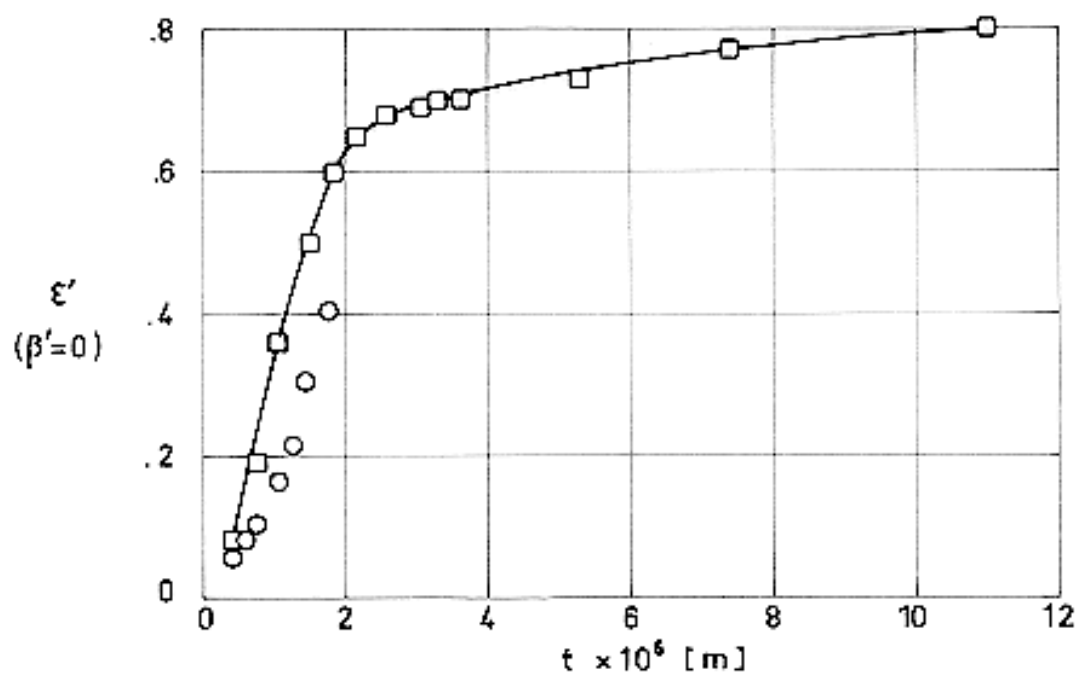


Note: non-si units are used in this figure

Figure 4-9: Normal total emittance, ε' , of Aluminium as a function of temperature, T .

Explanation

Key	Description	Comments	References
○	Cleaned, polished, and oxidized.		Touloukian & DeWitt (1972) [158].
□	Pure. Highly polished.	Reported error 2%.	
△	Pure. Rolled, as received.		

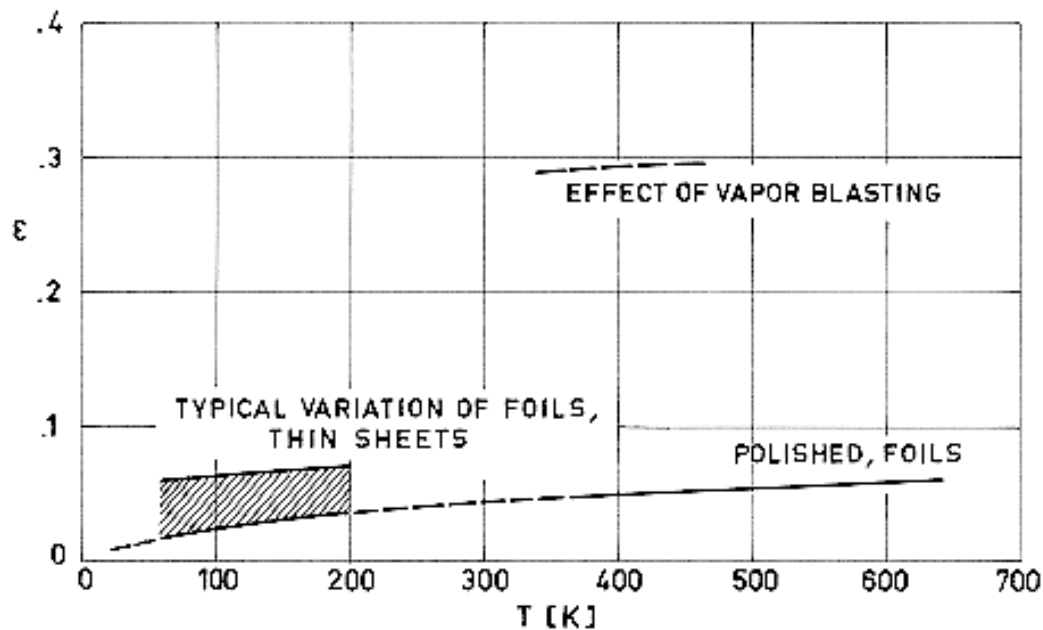


Note: non-si units are used in this figure

Figure 4-10: Normal total emittance, ϵ' , of Aluminium anodized as a function of anodizing thickness, t_c .

Explanation

Key	Description	Comments	References
○	Barrier-layer anodic coating on a high aluminium substrate. Substrate cleaned, electropolished in a flouboric acid solution, anodized in aqueous ammonium tartrate solution, then immersed in a phosphoric acid solution.	Sample temperature $T \sim 298 \text{ K}$. Measured in vacuum ($\sim 1,33 \times 10^{-4} \text{ Pa}$).	Touloukian, DeWitt & Hernicz (1972) [43].
□	Foil oxidized electrolytically in 15% sulphuric acid.	$T = 311 \text{ K}$. Measured relative to Aluminium.	



Note: non-si units are used in this figure

Figure 4-11: Summary of data concerning the hemispherical total emittance, ϵ , of Aluminium as a function of temperature, T . From Touloukian & DeWitt (1970) [42].

Table 4-4: Hemispherical Total Emittance of Aluminium Contact Coatings.

T [K]	ϵ	Comments
76	0,04	Aluminium; plastic Mylar ($1,27 \times 10^{-5}$ m thick) and aluminium substrates; produced by vaporizing aluminium on both sides of Mylar. Measured in vacuum ($1,3 \times 10^{-4}$ to $1,3 \times 10^{-5}$ Pa). Authors assumed $\alpha = \epsilon$ for 300 K blackbody incident radiation. Reported error 5%.
76	0,07	Aluminium; stainless steel substrate; Al sprayed on substrate. Measured in vacuum ($1,3 \times 10^{-4}$ to $1,3 \times 10^{-5}$ Pa). Authors assumed $\alpha = \epsilon$ for 300 K blackbody incident radiation. Reported error 5%.
76	0,06	Aluminium; stainless steel substrate; Al sprayed on substrate; wire brushed. Measured in vacuum ($1,3 \times 10^{-4}$ to $1,3 \times 10^{-5}$ Pa). Authors assumed $\alpha = \epsilon$ for 300 K blackbody incident radiation. Reported error 5%.
76	0,04	Aluminium plastic Mylar ($1,27 \times 10^{-5}$ m thick) and aluminium substrate; Al vapor deposited on both sides of Mylar. Measured in vacuum ($1,3 \times 10^{-4}$ Pa). Authors assumed $\alpha = \epsilon$ for 294 K blackbody radiation.

T [K]	ε	Comments
76	0,043	Similar to above specimen and conditions.
773-1273	0,69-0,78	Aluminium; iron substrate; substrate sandblasted and degreased; coated to a surface density of 75 kg.m^{-2} with aluminium powder suspension; sintered at 1223 K in vacuum. Measured in vacuum ($6,7 \times 10^{-4} \text{ Pa}$). Data extracted from smooth curve. Reported error 2,5%.
378-486	0,33-0,27	Aluminium ($1,27 \times 10^{-4}$ to $2,03 \times 10^{-4} \text{ m}$ thick); Al substrate; sprayed. Measured in vacuum ($0,13 \text{ Pa}$). Reported error 3%.
333	0,047	Aluminium; Mylar substrate. Measured in vacuum ($6,7 \times 10^{-4} \text{ Pa}$). Reported error <3,5%.
300-415	0,06	Aluminium (10^{-6} m thick); Mylar ($1,2 \times 10^{-5} \text{ m}$ thick) and stainless steel ($2,5 \times 10^{-4} \text{ m}$ thick) substrates; Mylar cemented to stainless steel; Al vapor deposited. Measured in vacuum ($1,3 \times 10^{-5} \text{ Pa}$). Reported error 5%.
258-348	0,0428-0,0454	Aluminium ($2 \times 10^{-7} \text{ m}$ thick); stainless steel substrate; Al vapor deposited on hand-polished substrate; property measured by steady-state calorimetric method. Mentioned below as specimen 1.
248-348	0,0293-0,0311	Same specimen and conditions as 1 except property measured by transient calorimetric method; property of second side of sample assumed.
303	0,024	Same specimen and conditions as 1 except property calculated from ρ (10° , 10°) measured by specular method relative to a front surface aluminized mirror.
300	0,0482	Same specimen and conditions as 1 except property calculated from ρ ($7,5^\circ$, 2π) measured by ellipsoid method.
200-400	0,0224-0,0237	Same specimen and conditions as 1 except property calculated from ρ (2π - 75° , 15°). Specimen placed at the center of a heated cavity, so that the angle of viewing can be varied from 15° to 75° . (Millard & Streed (1969) [27]).
295	0,0279	Same specimen and conditions as 1 except property measured by a portable Quick Emittance Device.
295	0,041	Same specimen and conditions as 1 except property measured by a portable emissometer.
~298	0,0334	Polyester film ($6,35 \times 10^{-6} \text{ m}$ thick) double aluminized. Coating thickness of emitting surface $t_{c1} = 4,55 \times 10^{-8} \text{ m}$. Coating thickness of second surface $t_{c2} = 3,78 \times 10^{-8} \text{ m}$.